Numerické experimenty

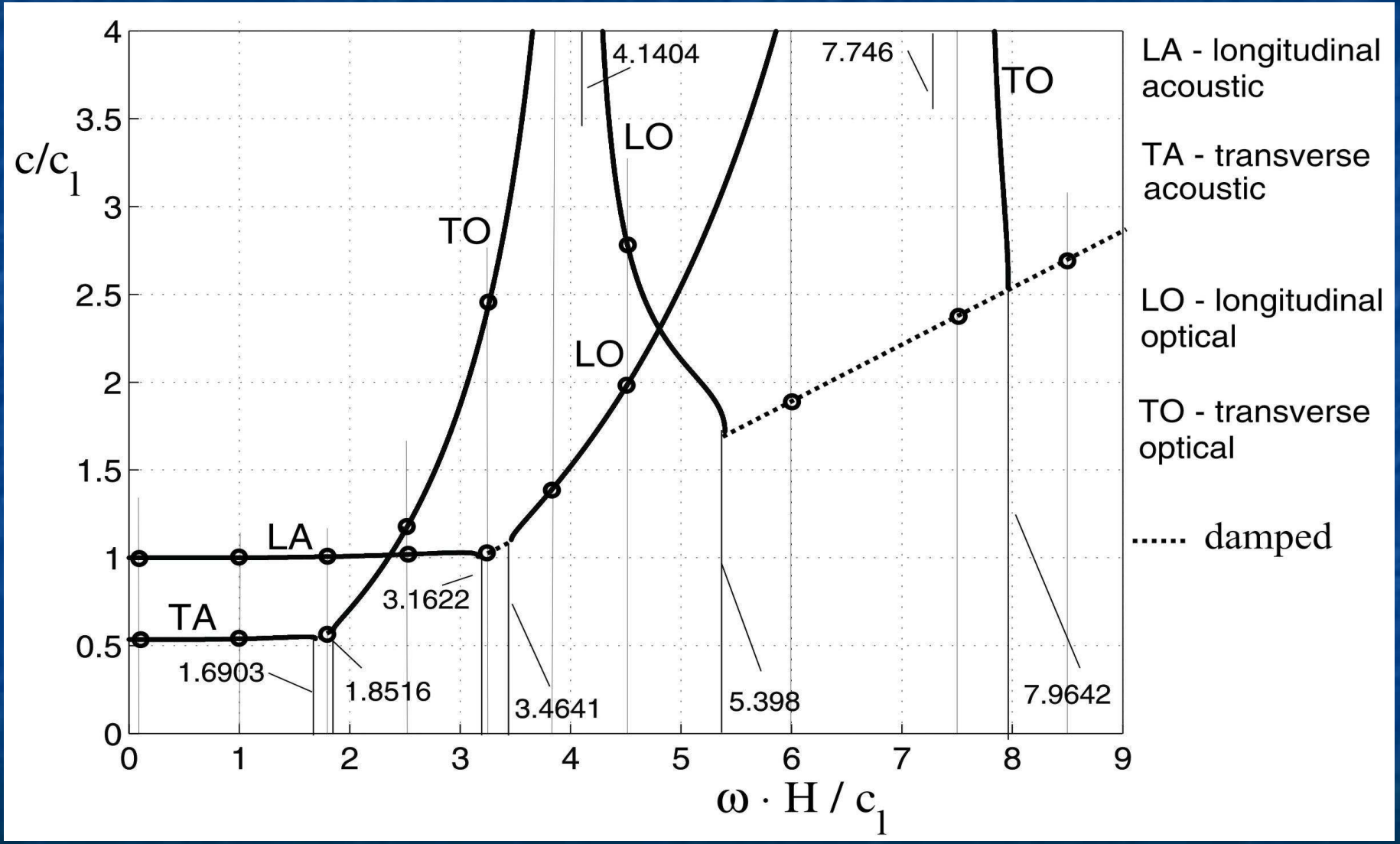
1. Rozlehlá stěna ve stavu rovinné deformace,
   síť 100x100 kvadratických prvků,
   velikost hrany prvku H=1mm

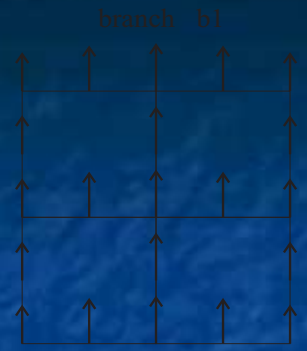
2. Bodové kinematické buzení ve středu desky
   ve vodorovném směru,
   pro jednotlivé testy se bezrozměrná frekvence $\omega H/c_1$
   mění v rozmezí 0.1-8.3 s krokem 0.1

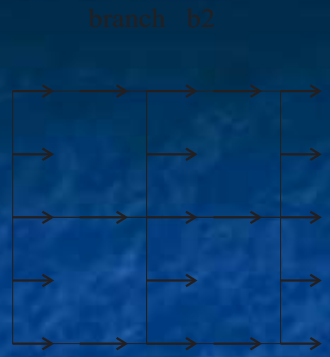
3. Numerická integrace Newmarkovou metodou
   s časovým krokem Δt=1e-5 s,
   Courantovo číslo $Co=c_1\Delta t/H=0.011602$

4. Materiálové vlastnosti: modul pružnosti E=1 Pa
   Poissonovo číslo μ= 0.3
   hustota ρ=1 kg/m^3

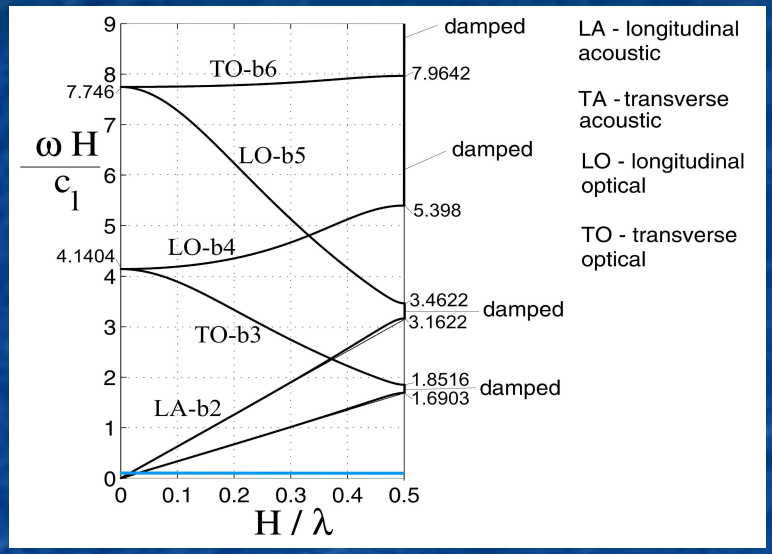
Frekvence buzení

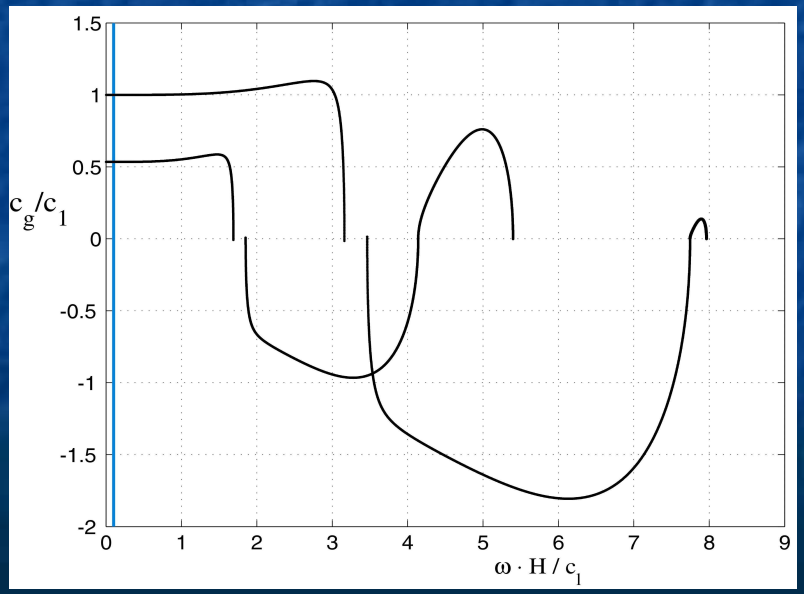


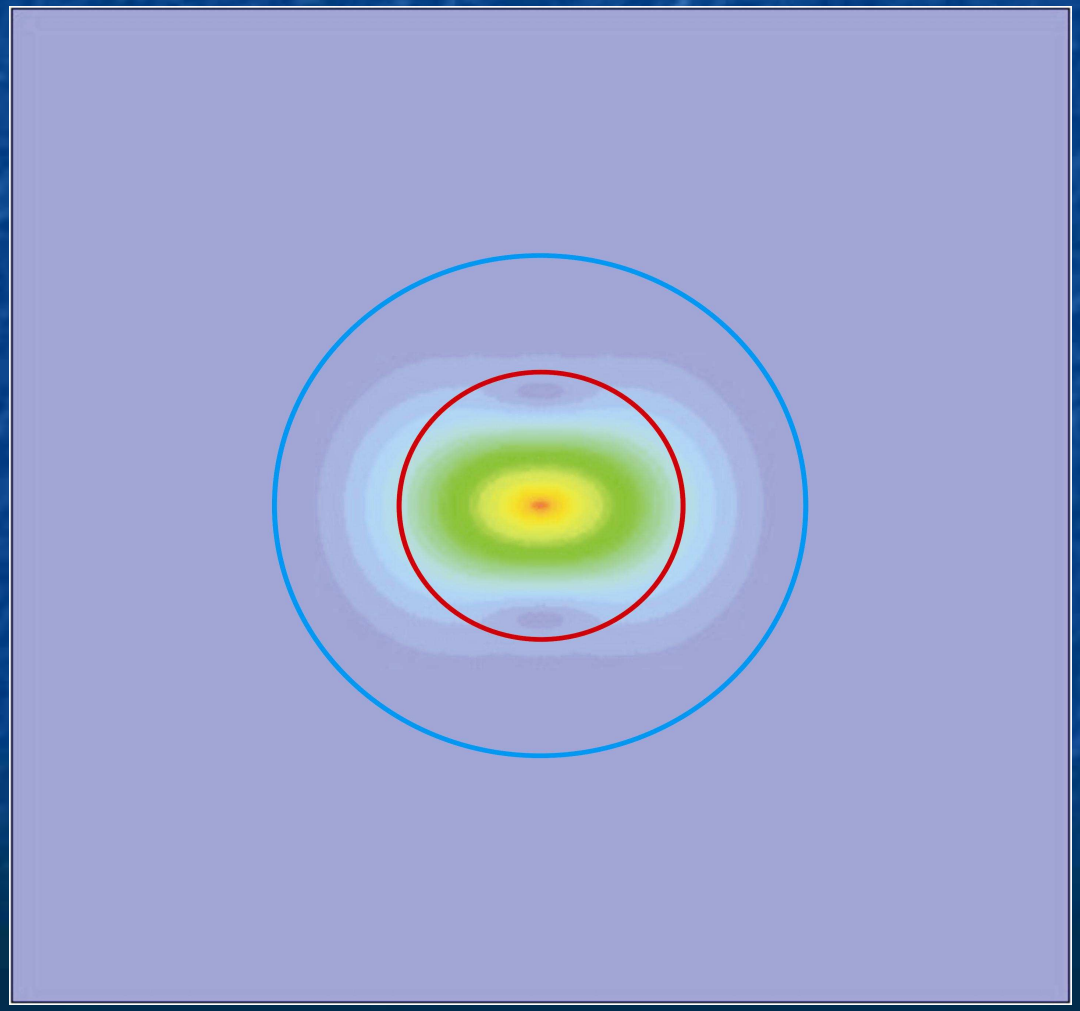

branch b1

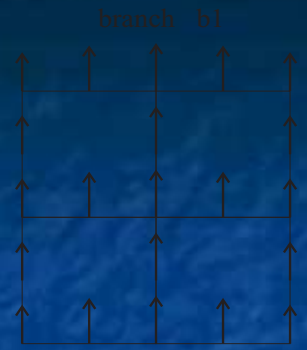

branch b2

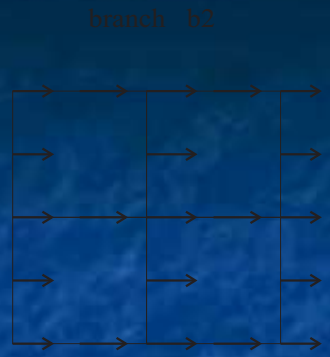
$$\omega H / c_1 = 0.1$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

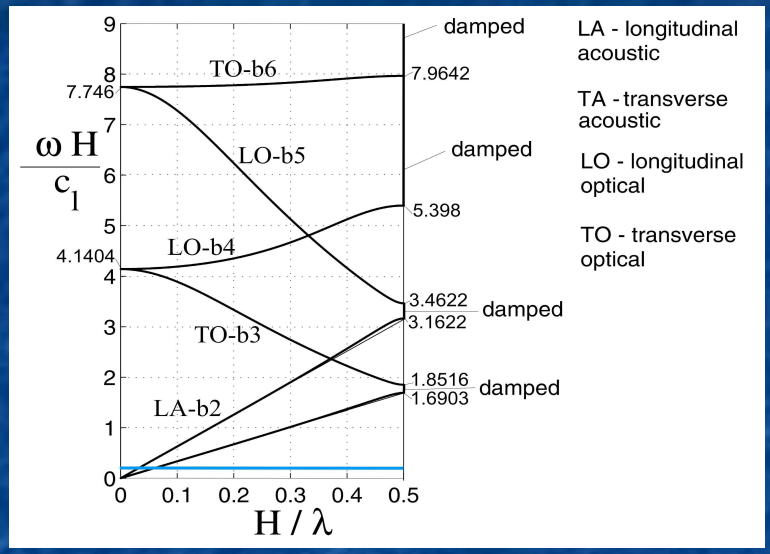

cg /c1
ω · H / c1

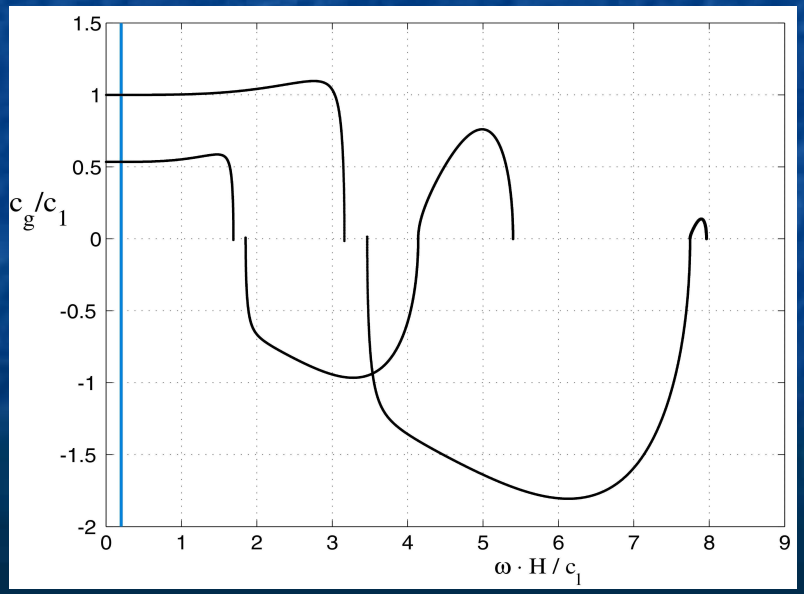


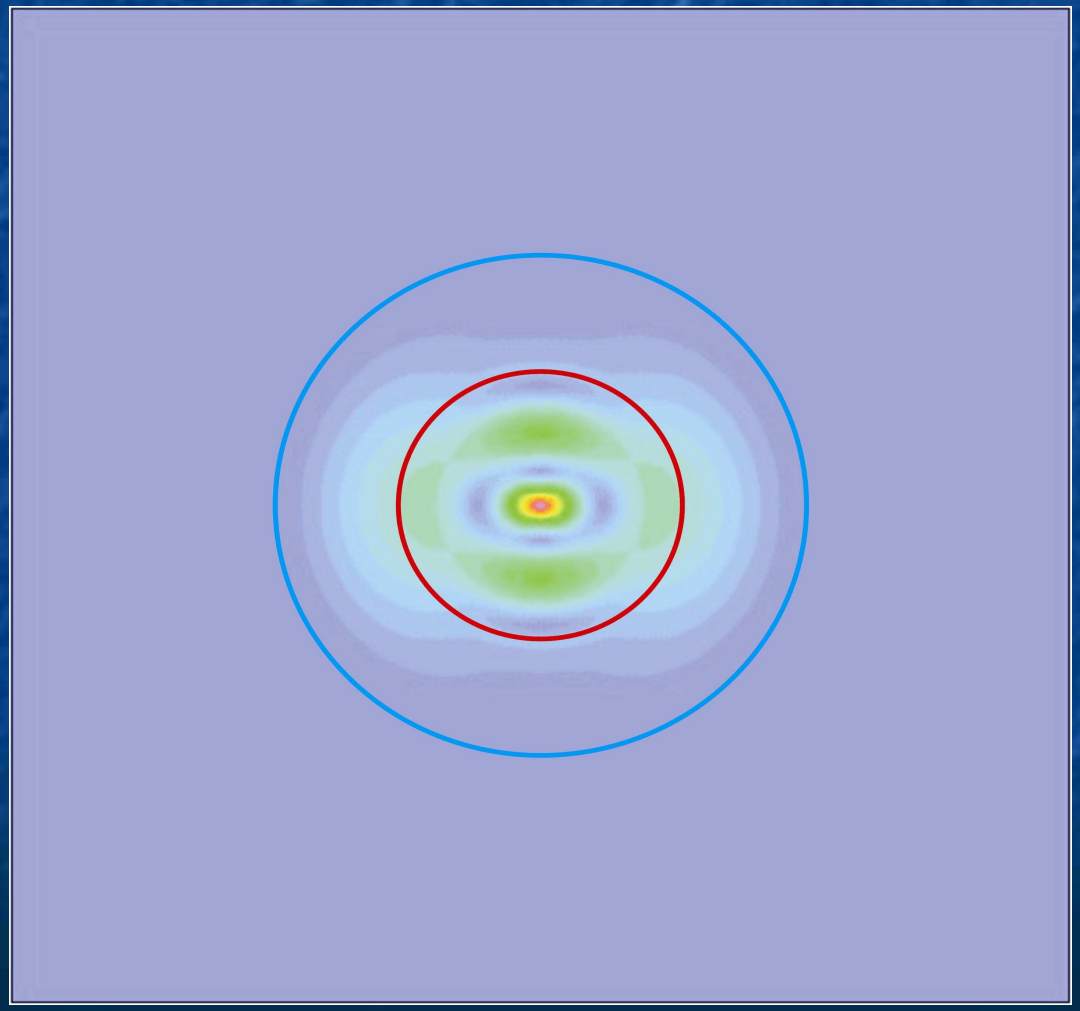

branch b1

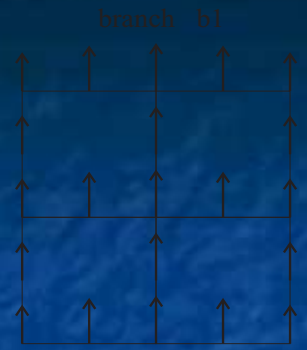

branch b2

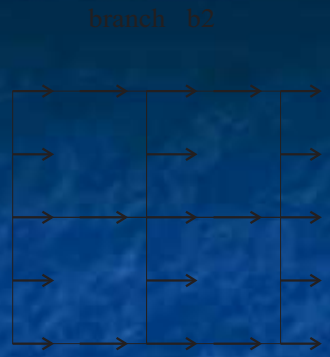
$$\omega H / c_1 = 0.2$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

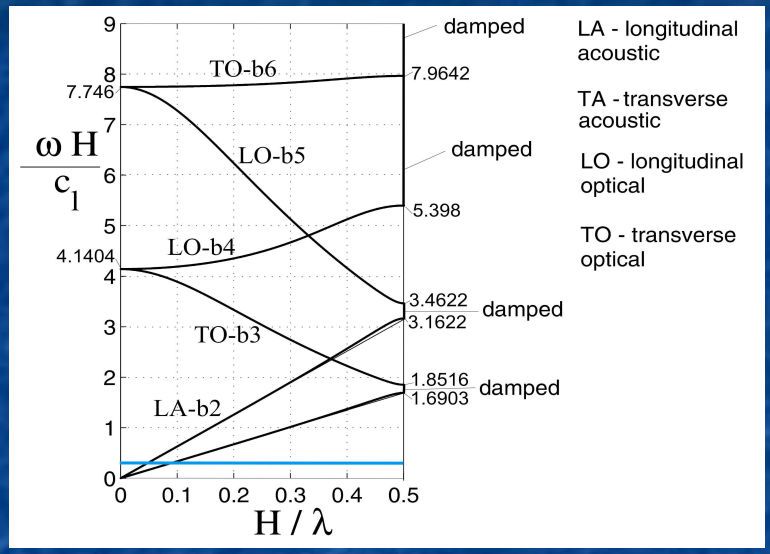

cg /c1
ω · H / c1

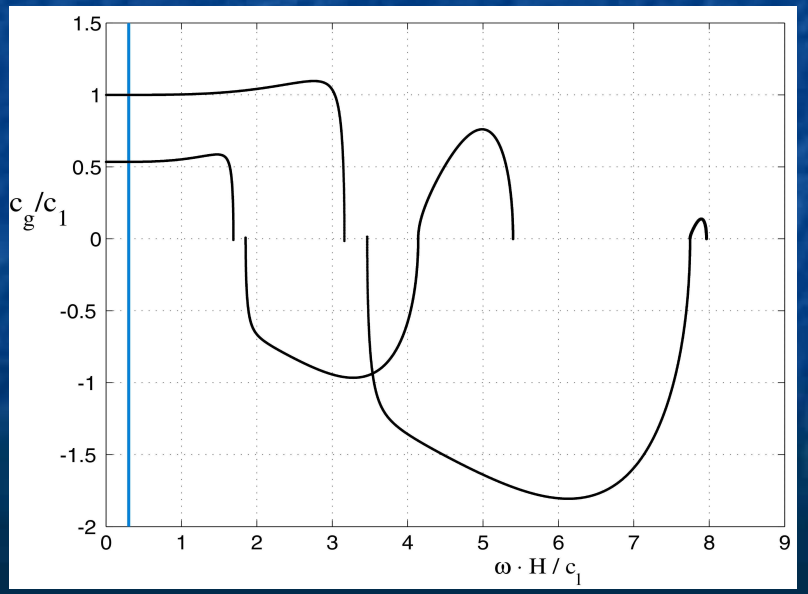


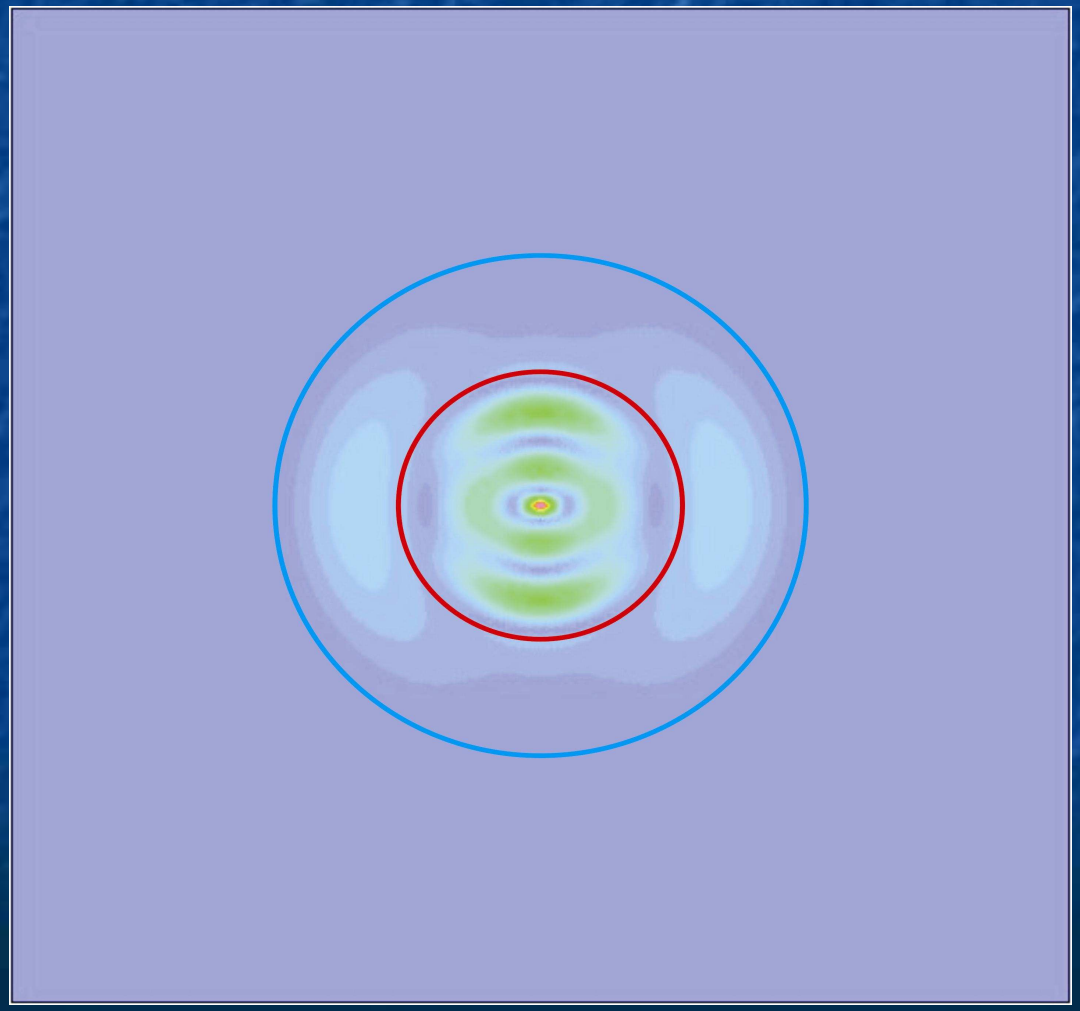

branch b1

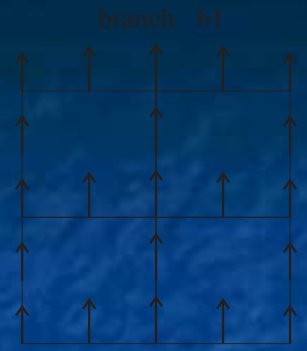

branch b2

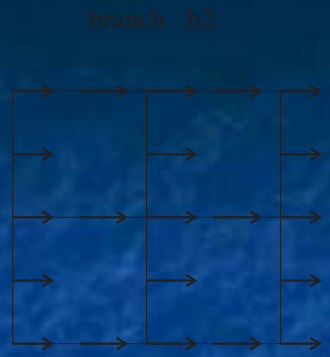
$$\omega H / c_1 = 0.3$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

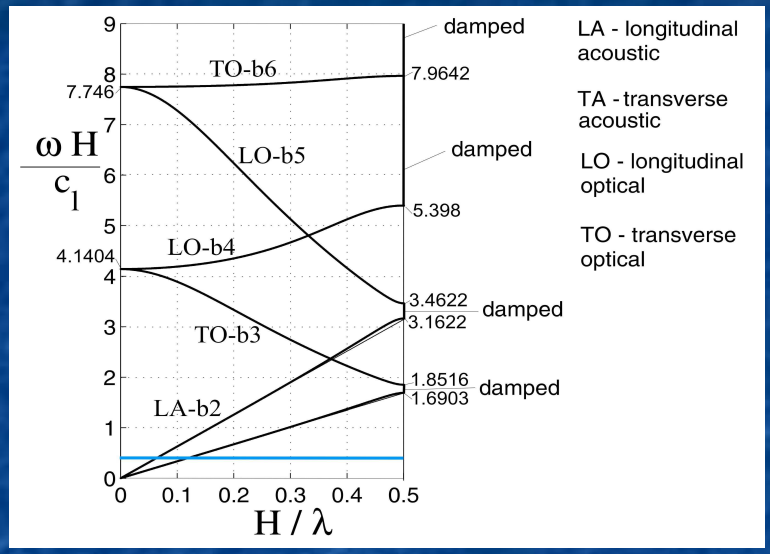

cg /c1
ω · H / c1

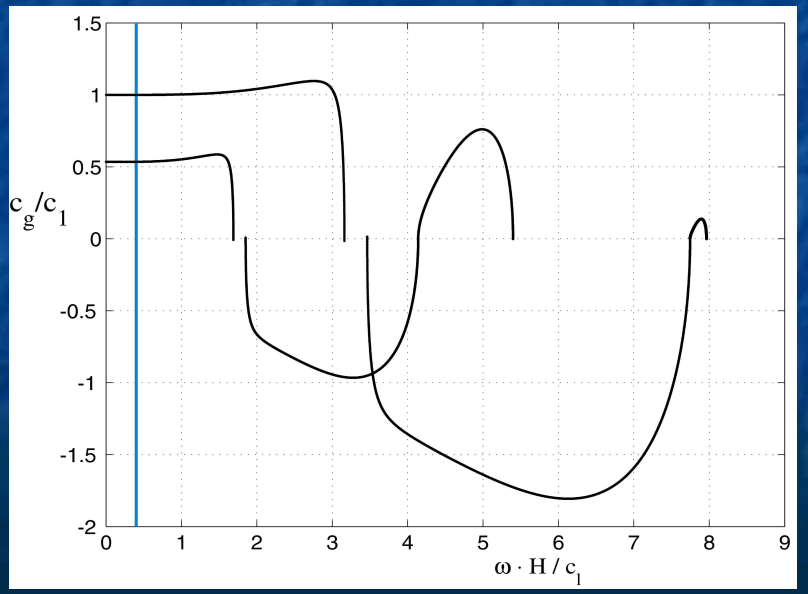


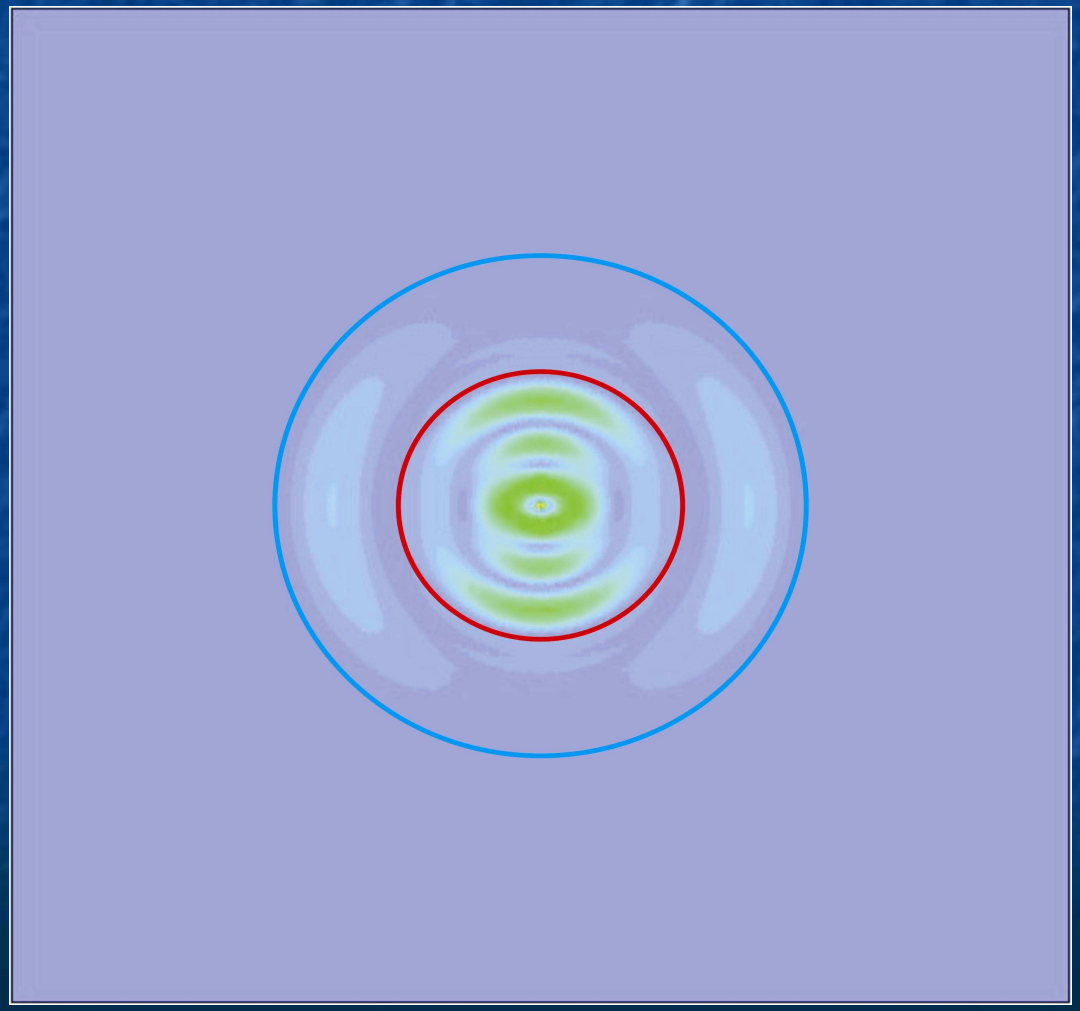

branch b1

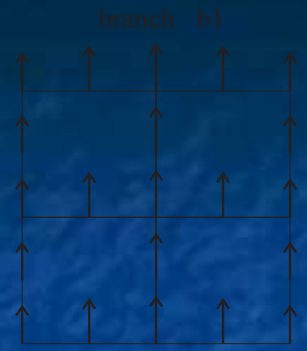

branch b2

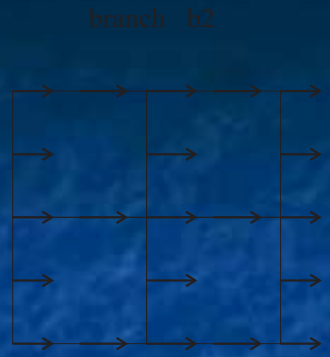
$$\omega H / c_1 = 0.4$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

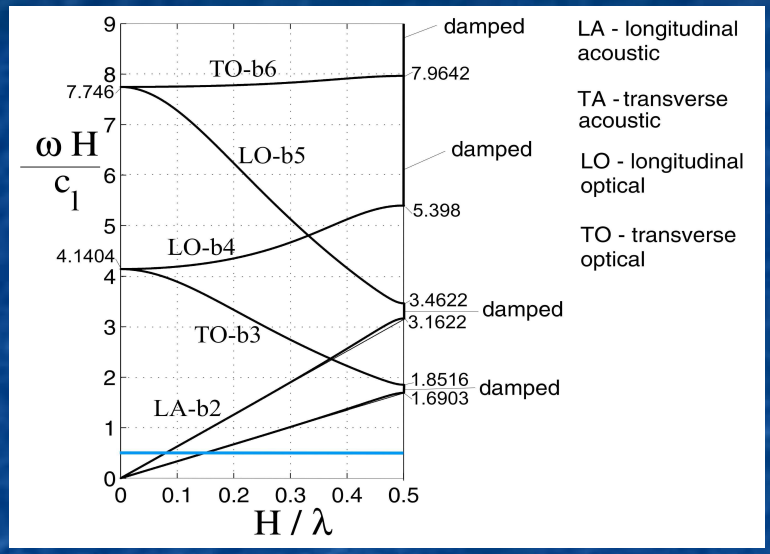

cg /c1
ω · H / c1

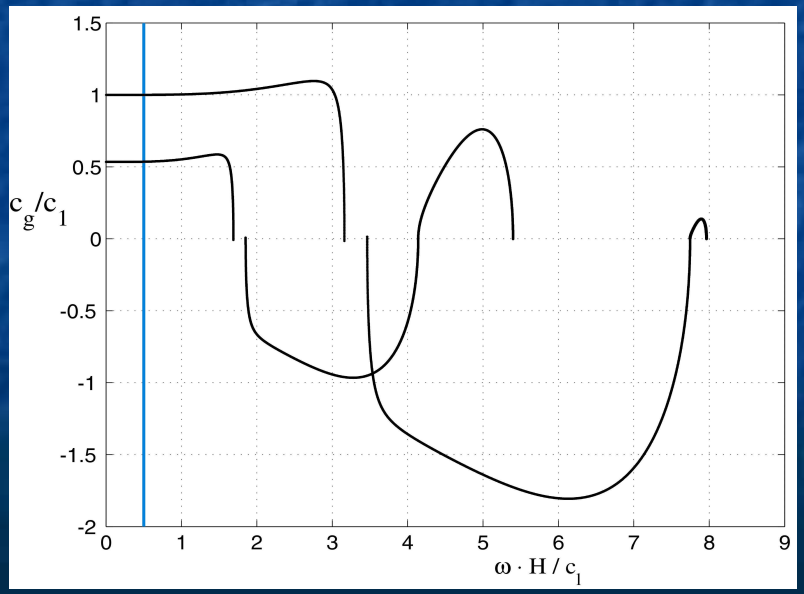


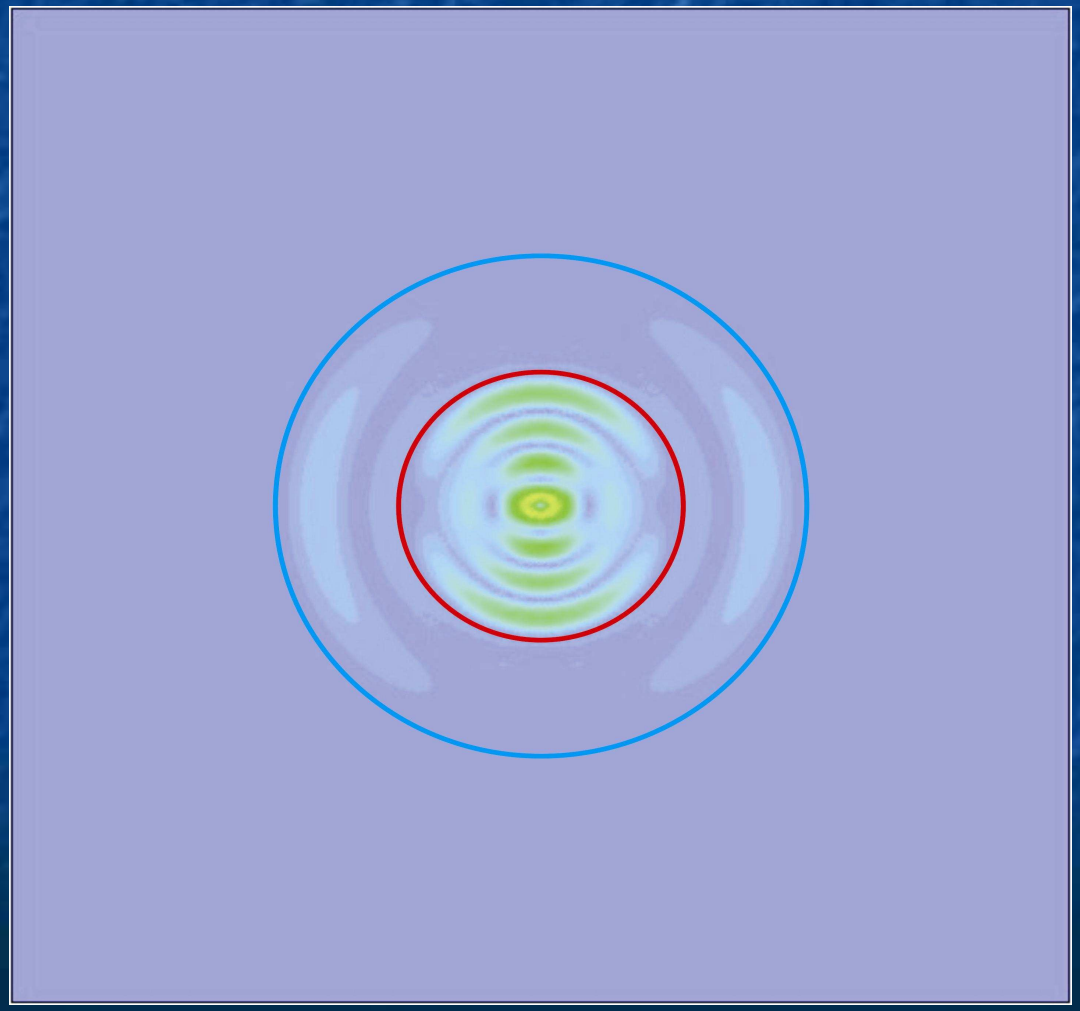

branch b1

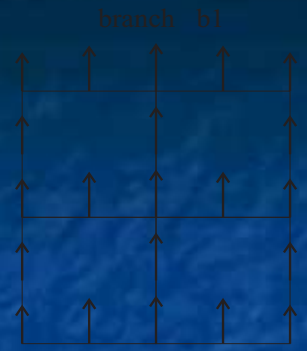

branch b2

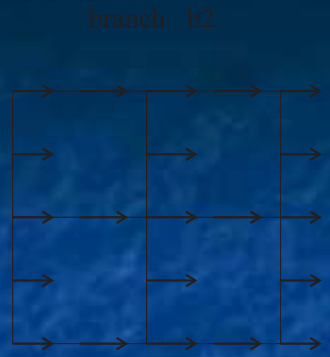
$$\omega H / c_1 = 0.5$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

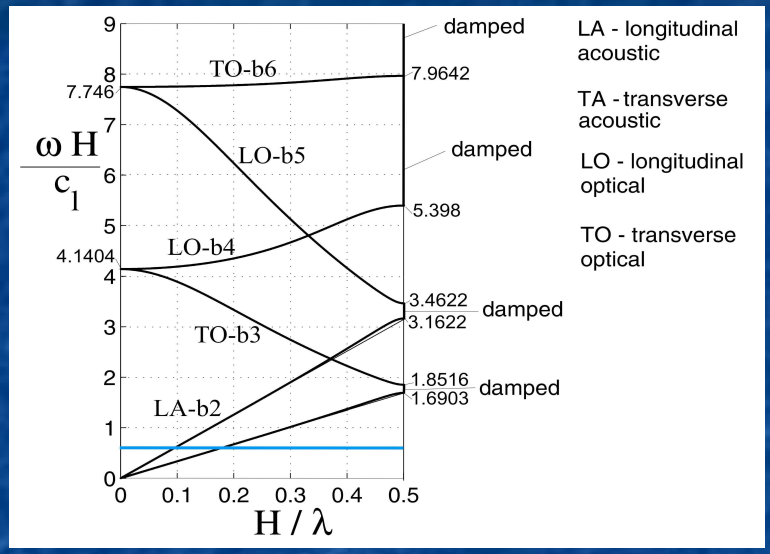

cg /c1
ω · H / c1

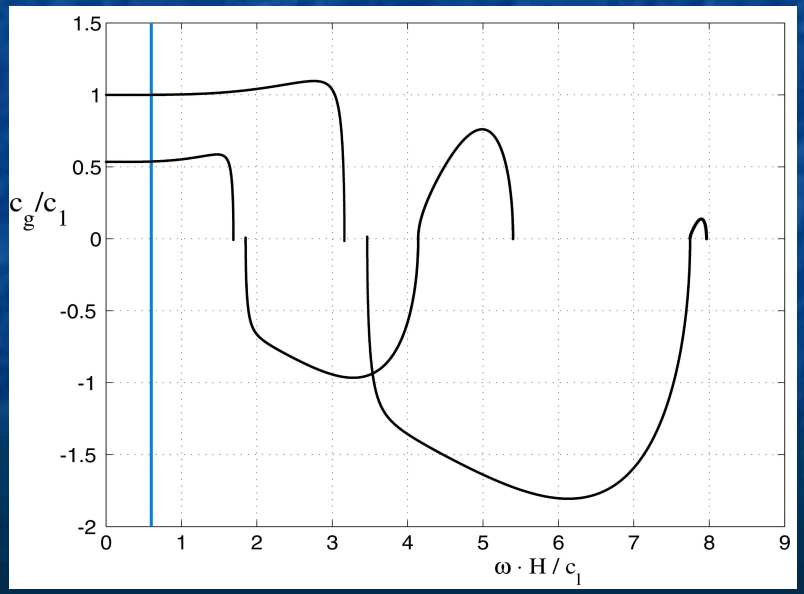


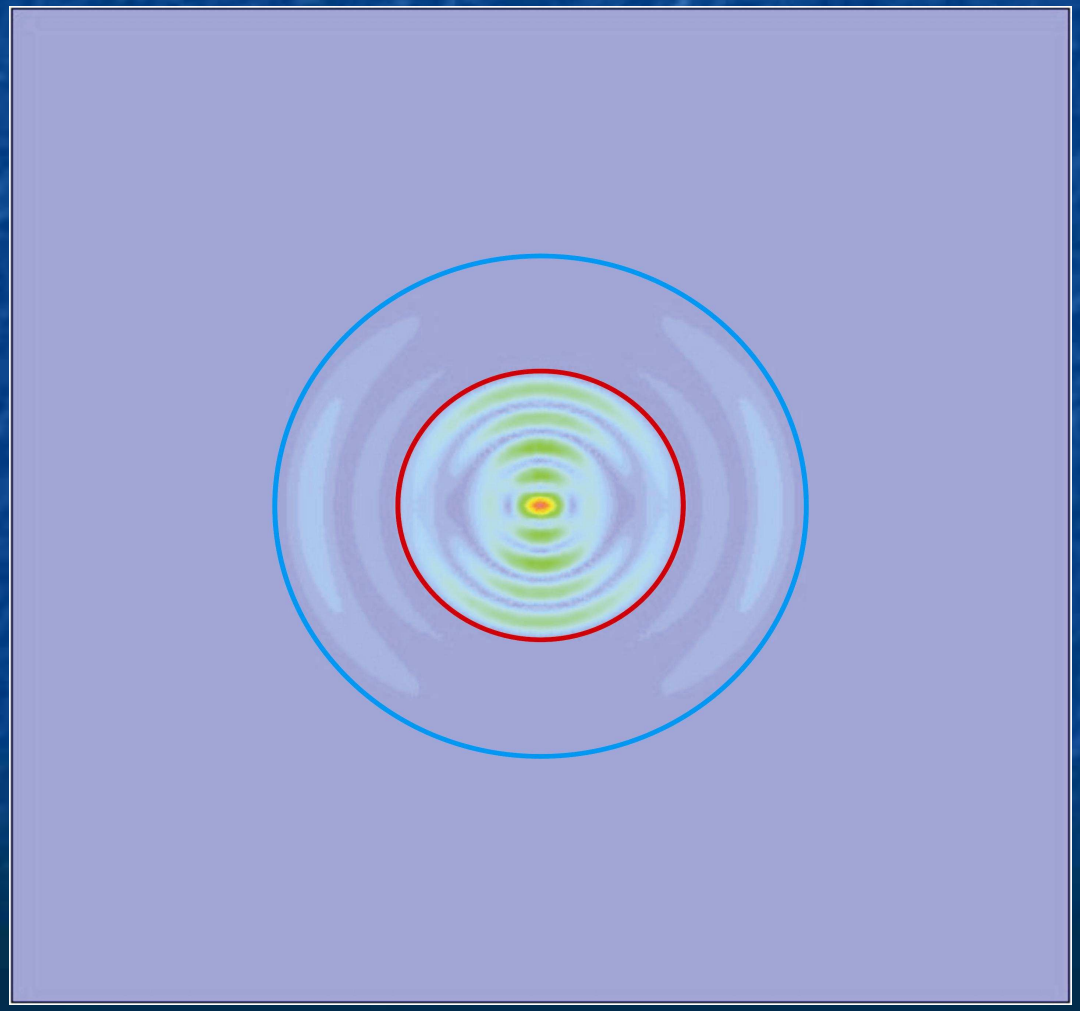

branch b1

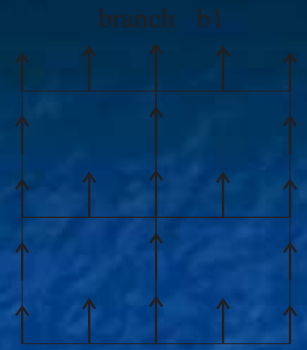

branch b2

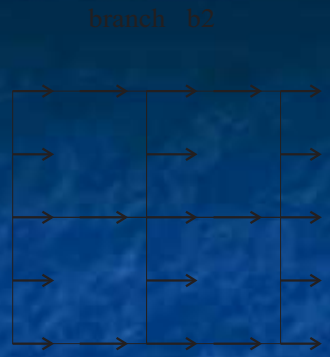
$$\omega H / c_1 = 0.6$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

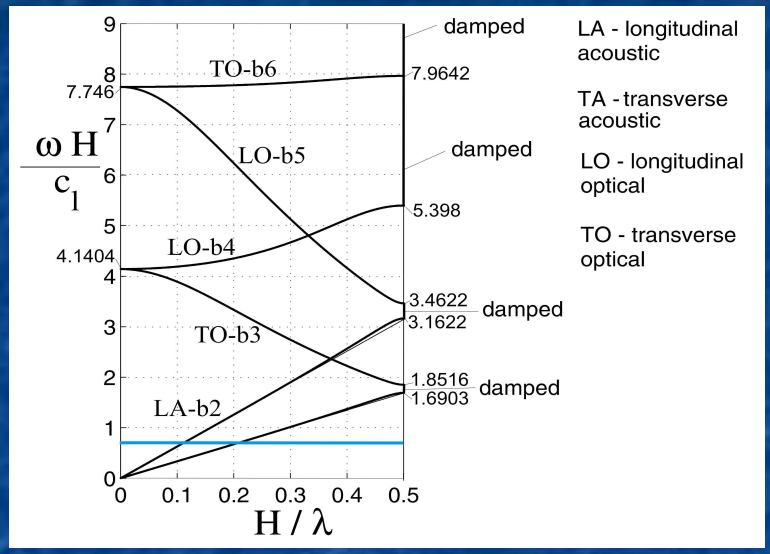

cg /c1
ω · H / c1




branch b1


branch b2

$$\omega H / c_1 = 0.7$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
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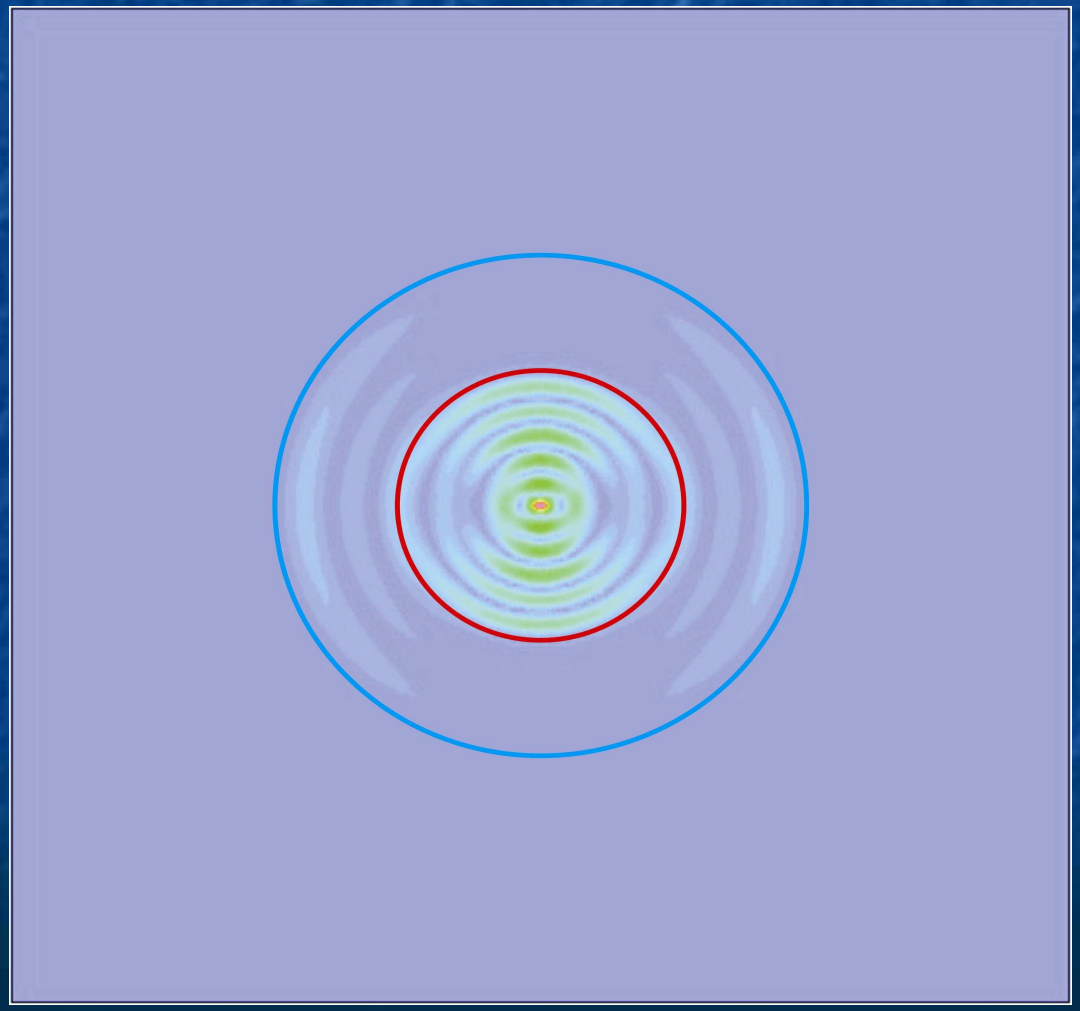
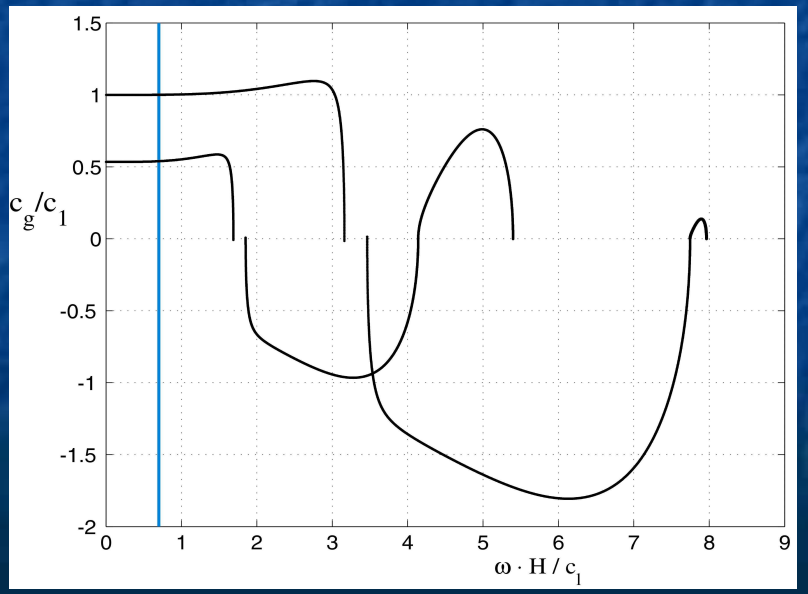
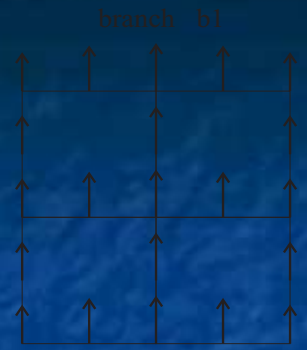
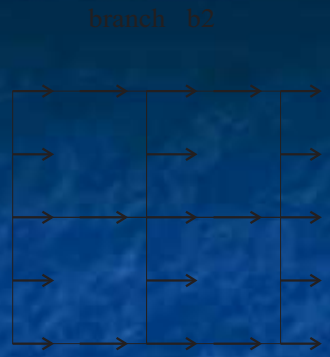
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

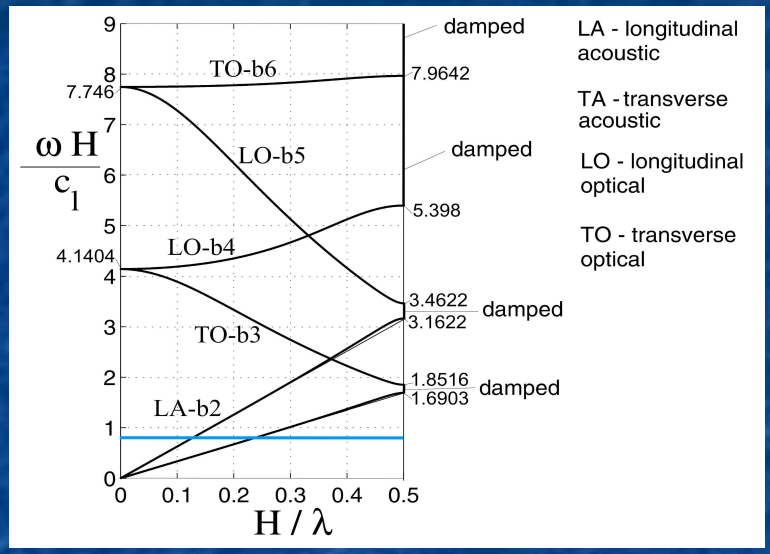


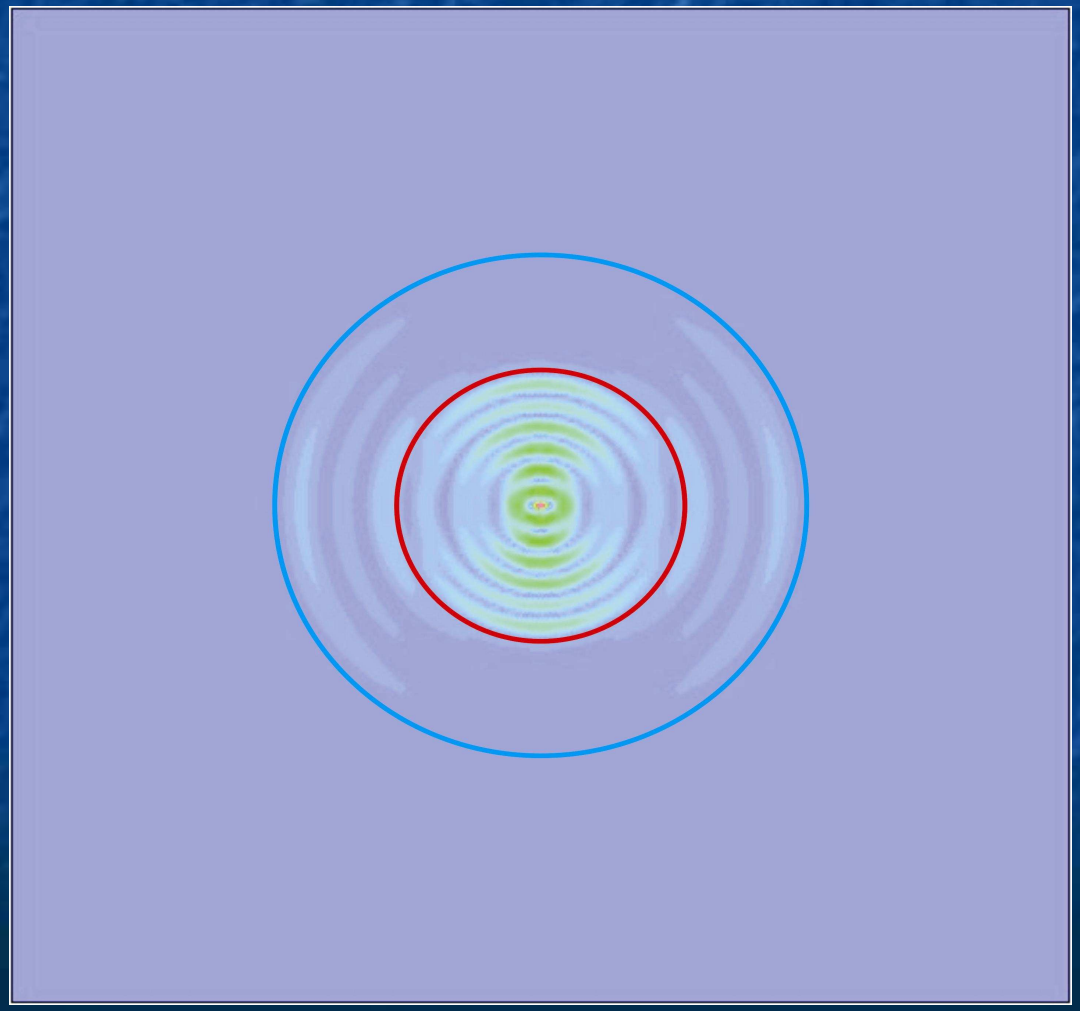

cg/c1
ω · H / c1

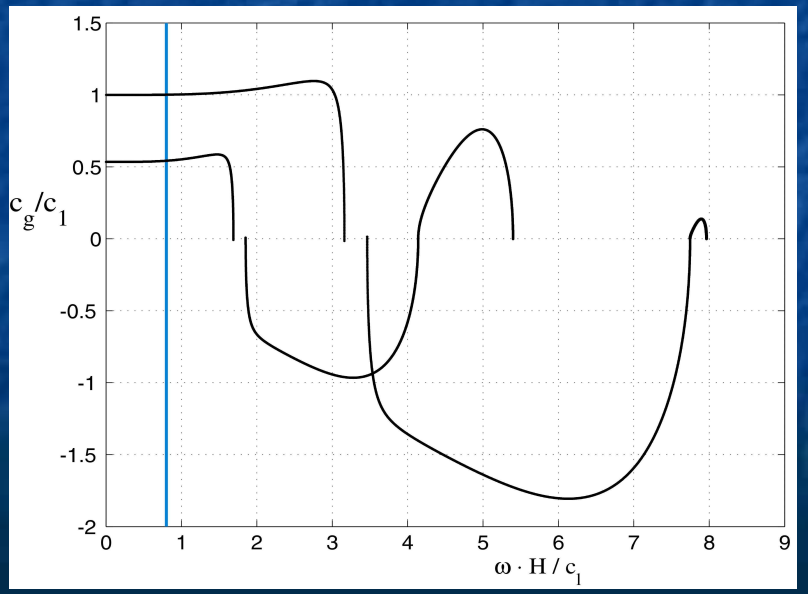

branch b1

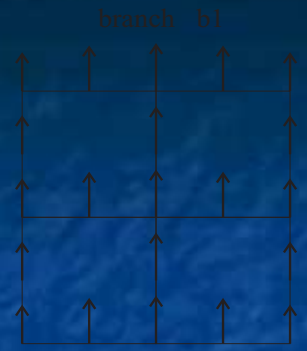

branch b2

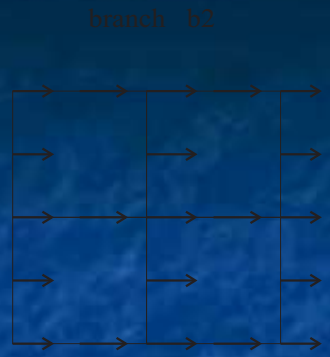
$$\omega H / c_1 = 0.8$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

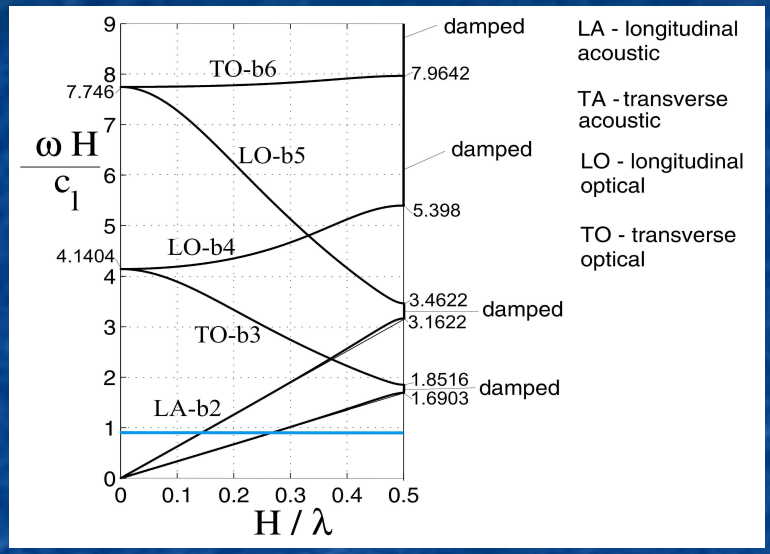



cg /c1
ω · H / c1


branch b1


branch b2

$$\omega H / c_1 = 0.9$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
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1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
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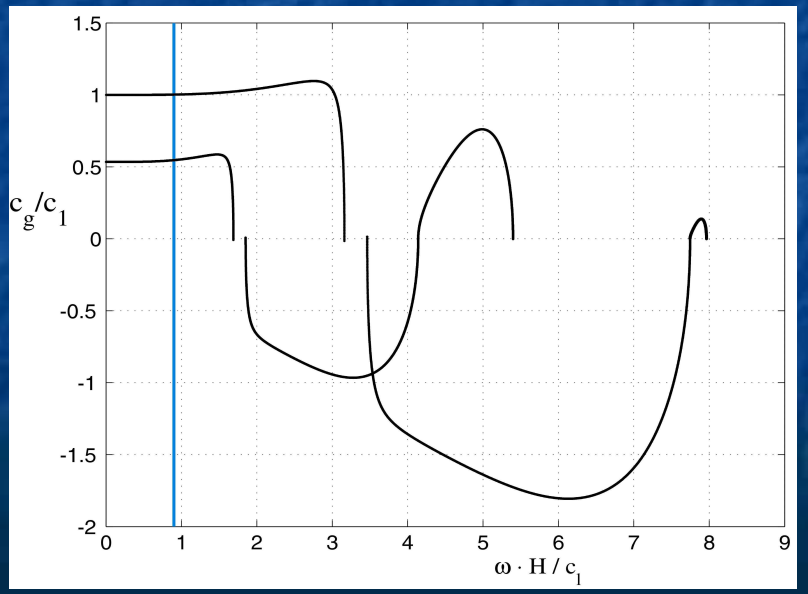
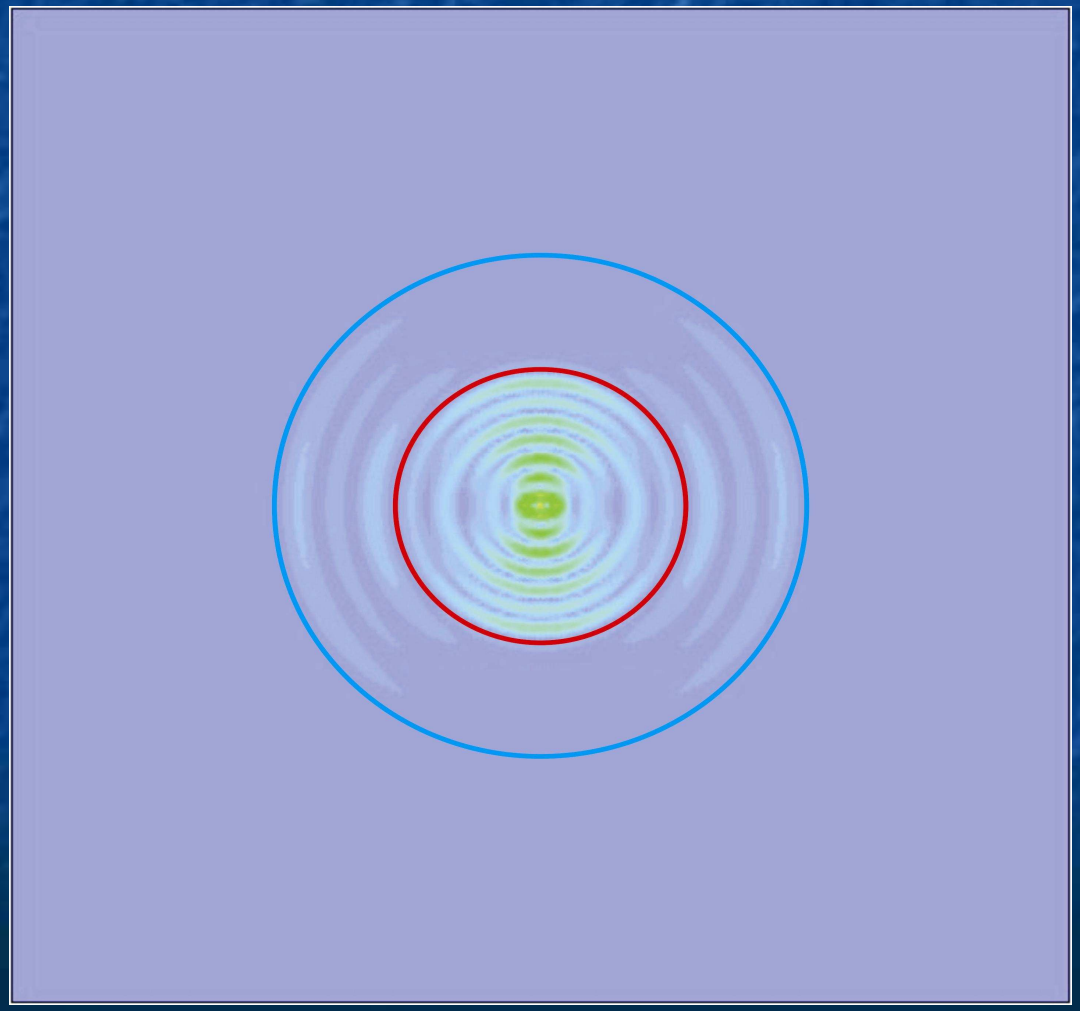
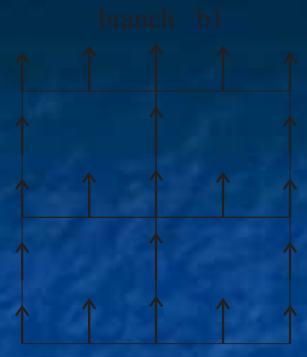
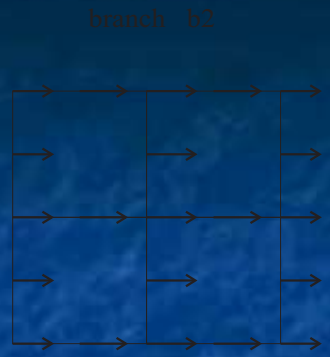
LO - longitudinal optical
TO - transverse optical

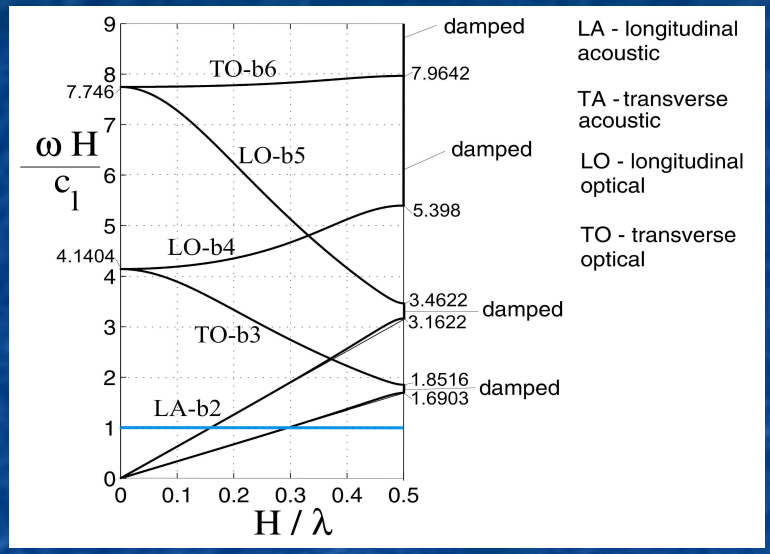

cg /c1
ω · H / c1

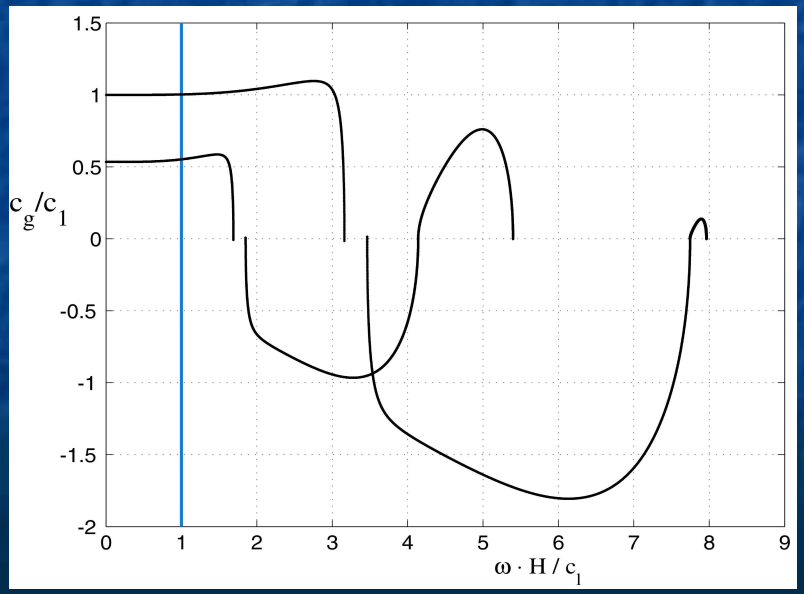


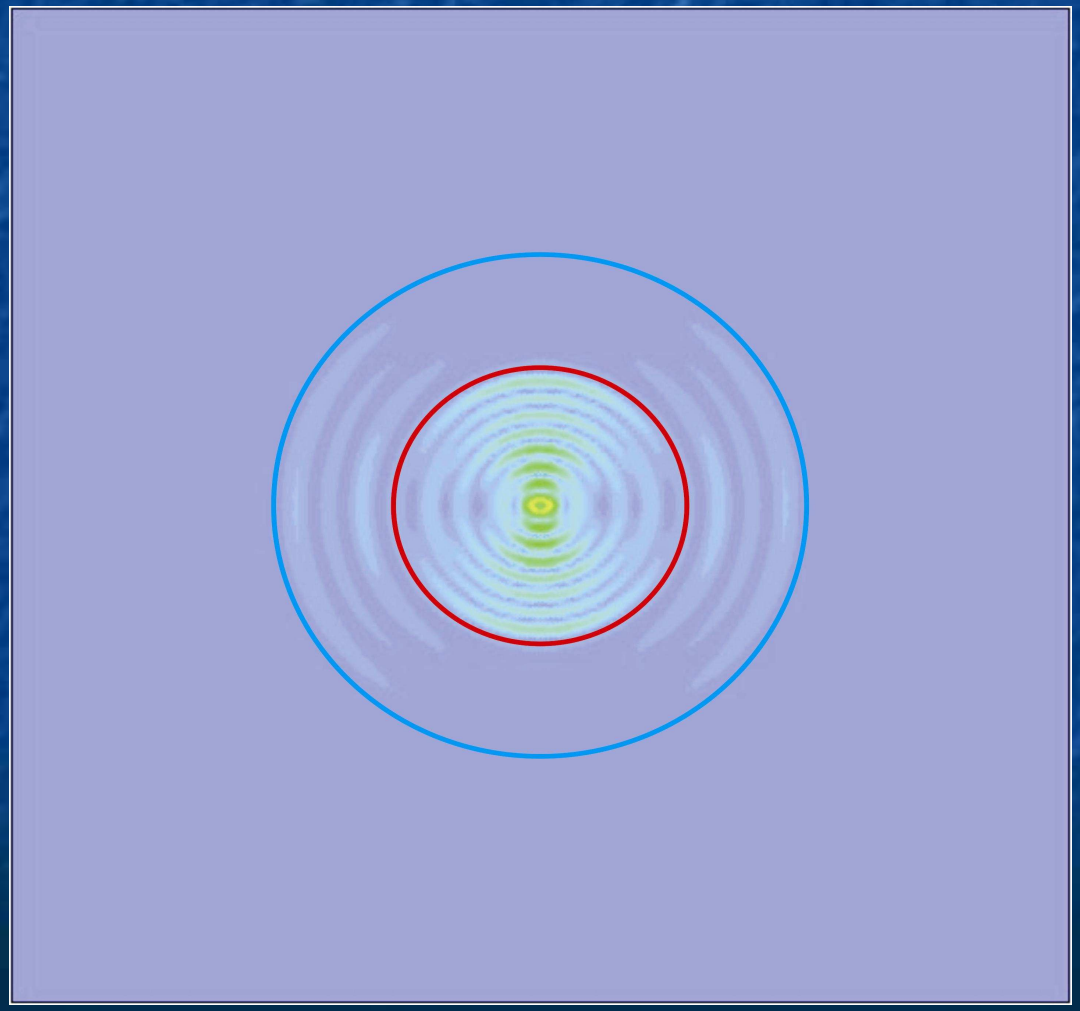

branch b1

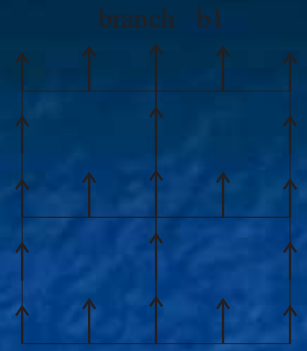

branch b2

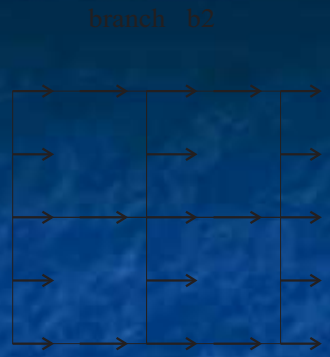
$$\omega H / c_1 = 1.0$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

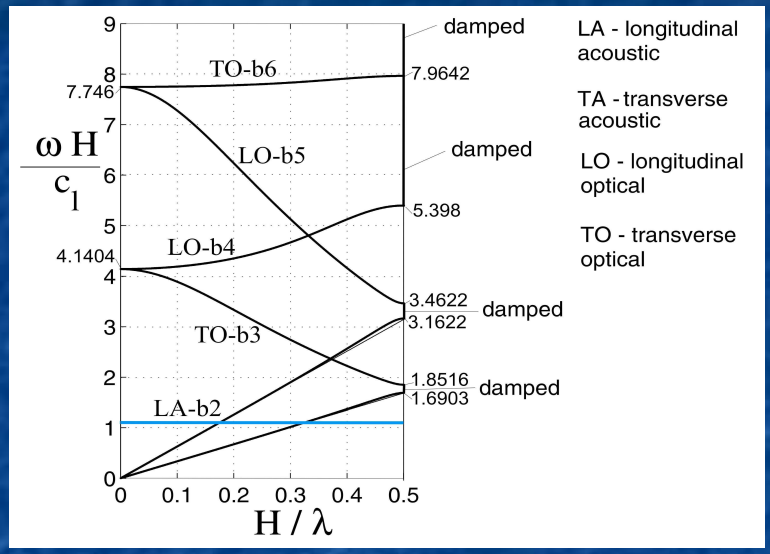

cg /c1
ω · H / c1

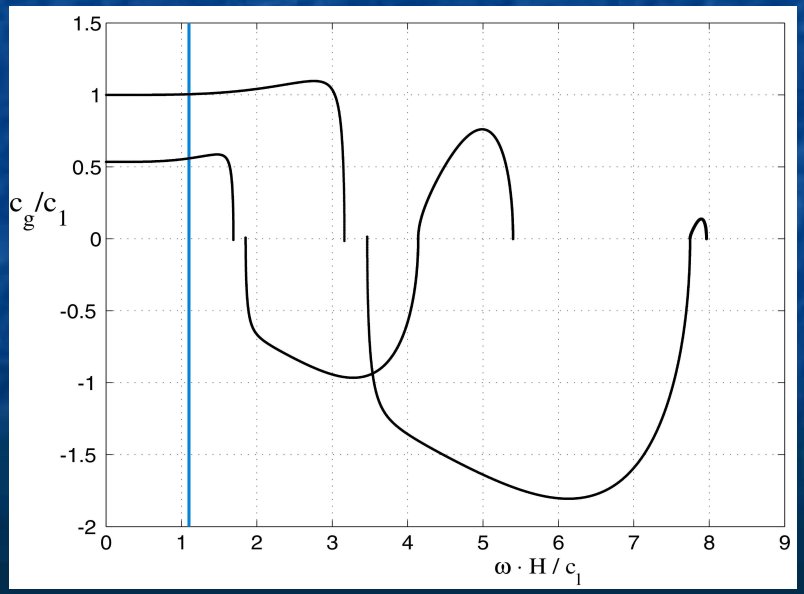


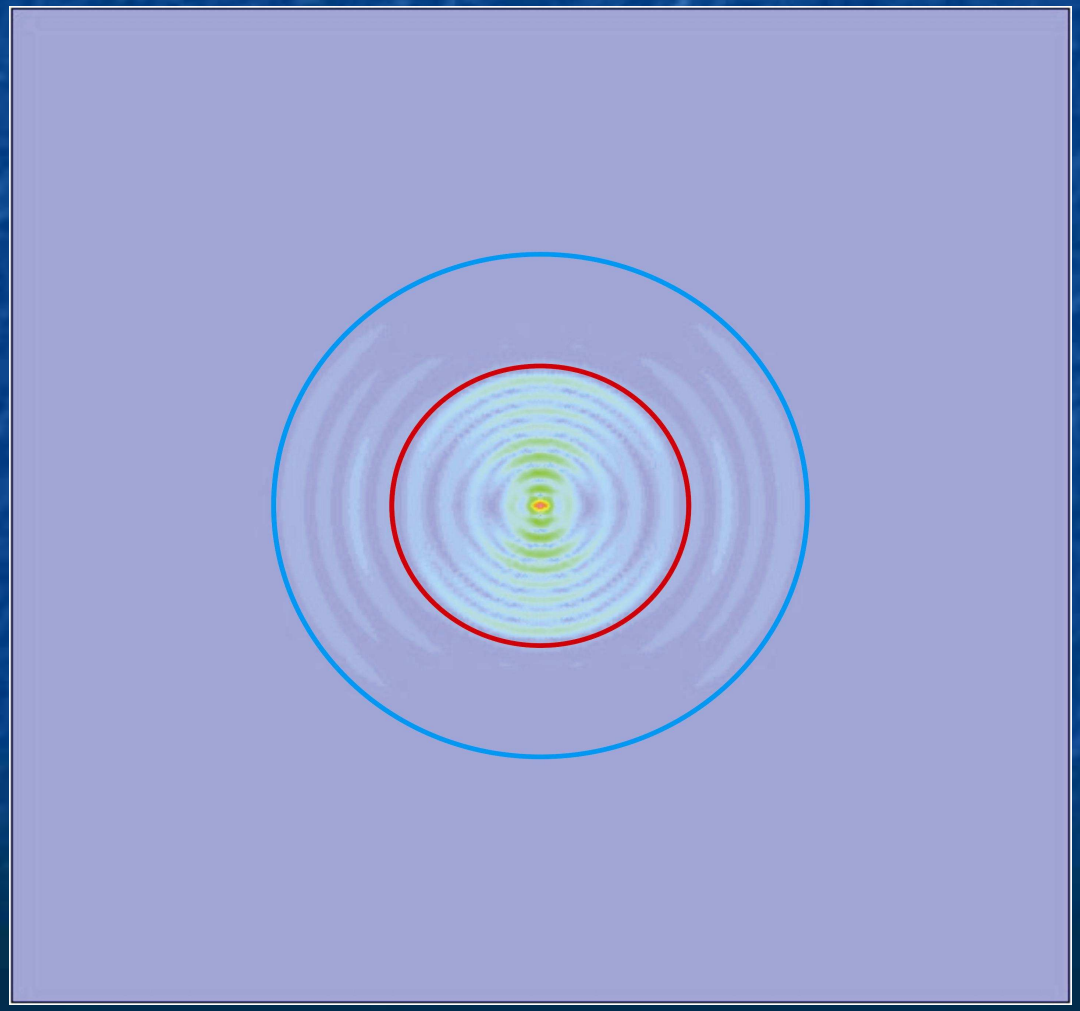

branch b1

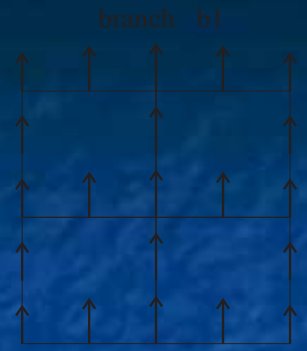

branch b2

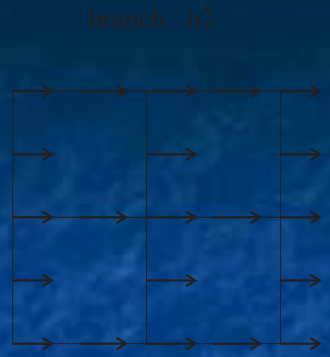
$$\omega H / c_1 = 1.1$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

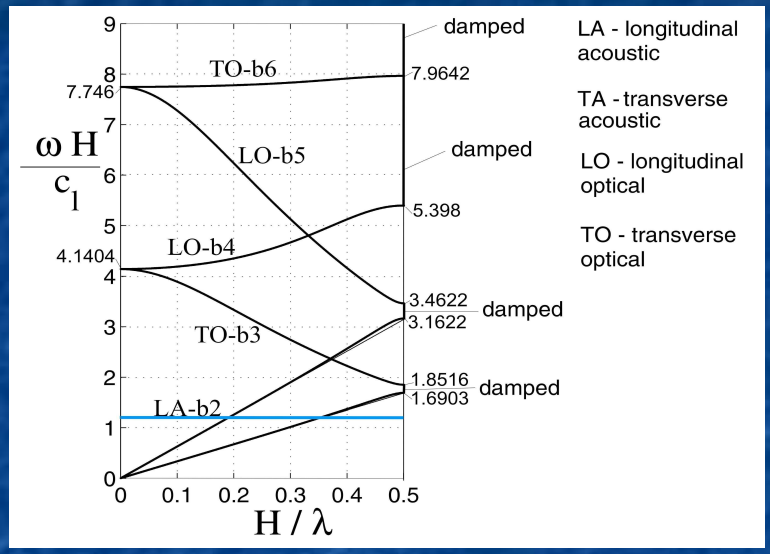

cg /c1
ω · H / c1

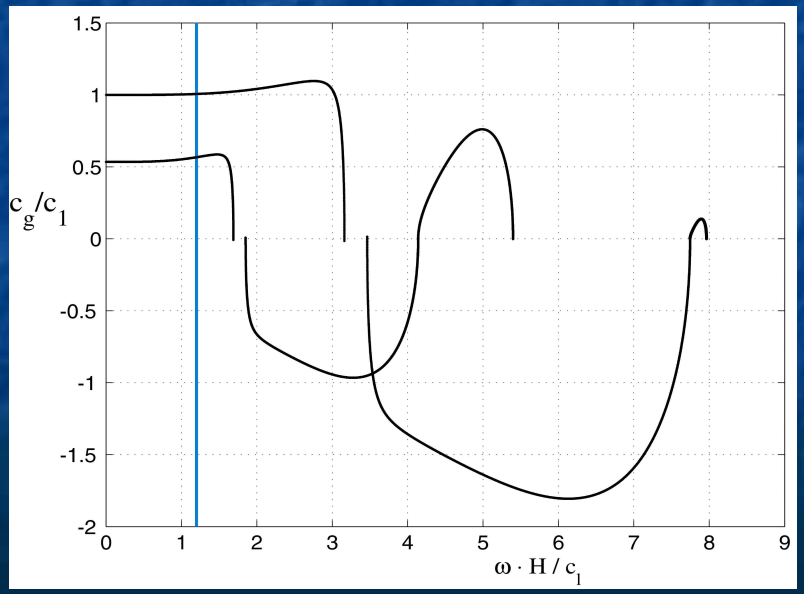


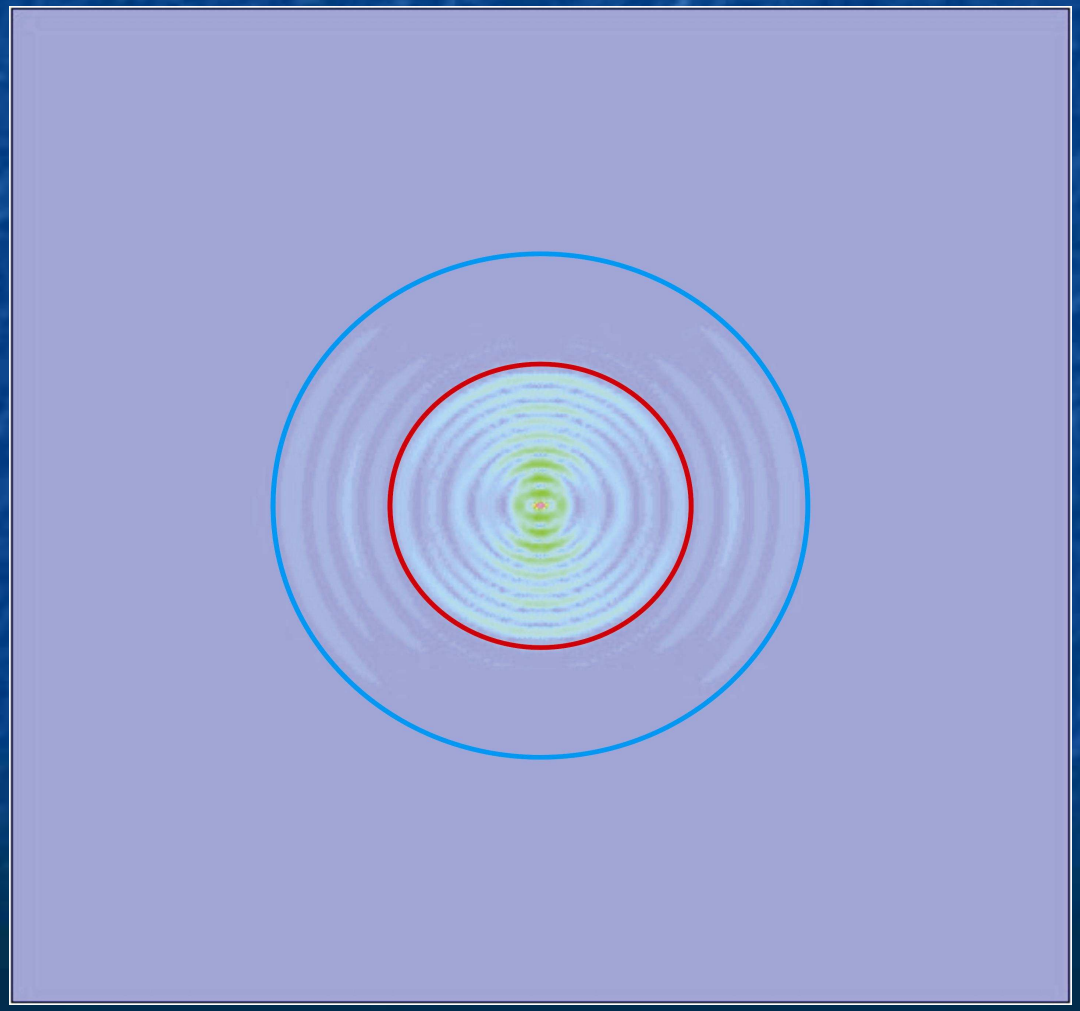

branch b1

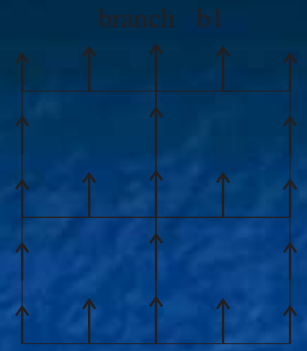

branch b2

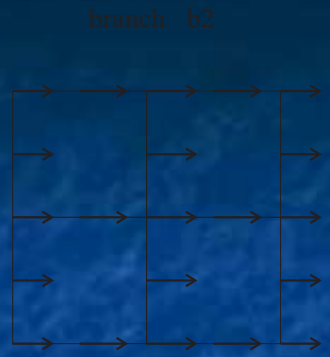
$$\omega H / c_1 = 1.2$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

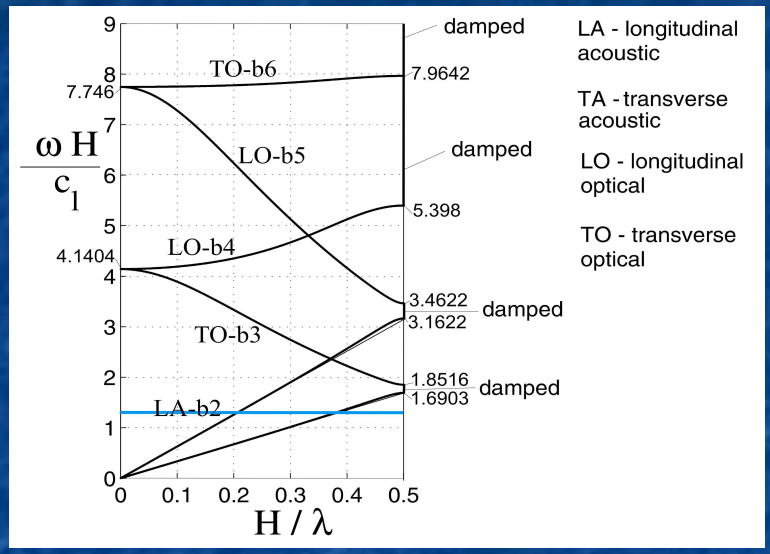

cg /c1
ω · H / c1

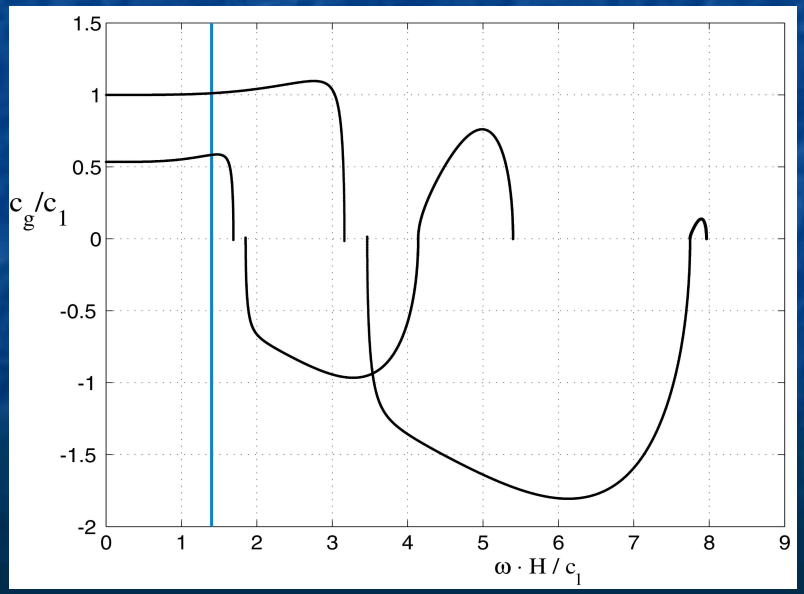


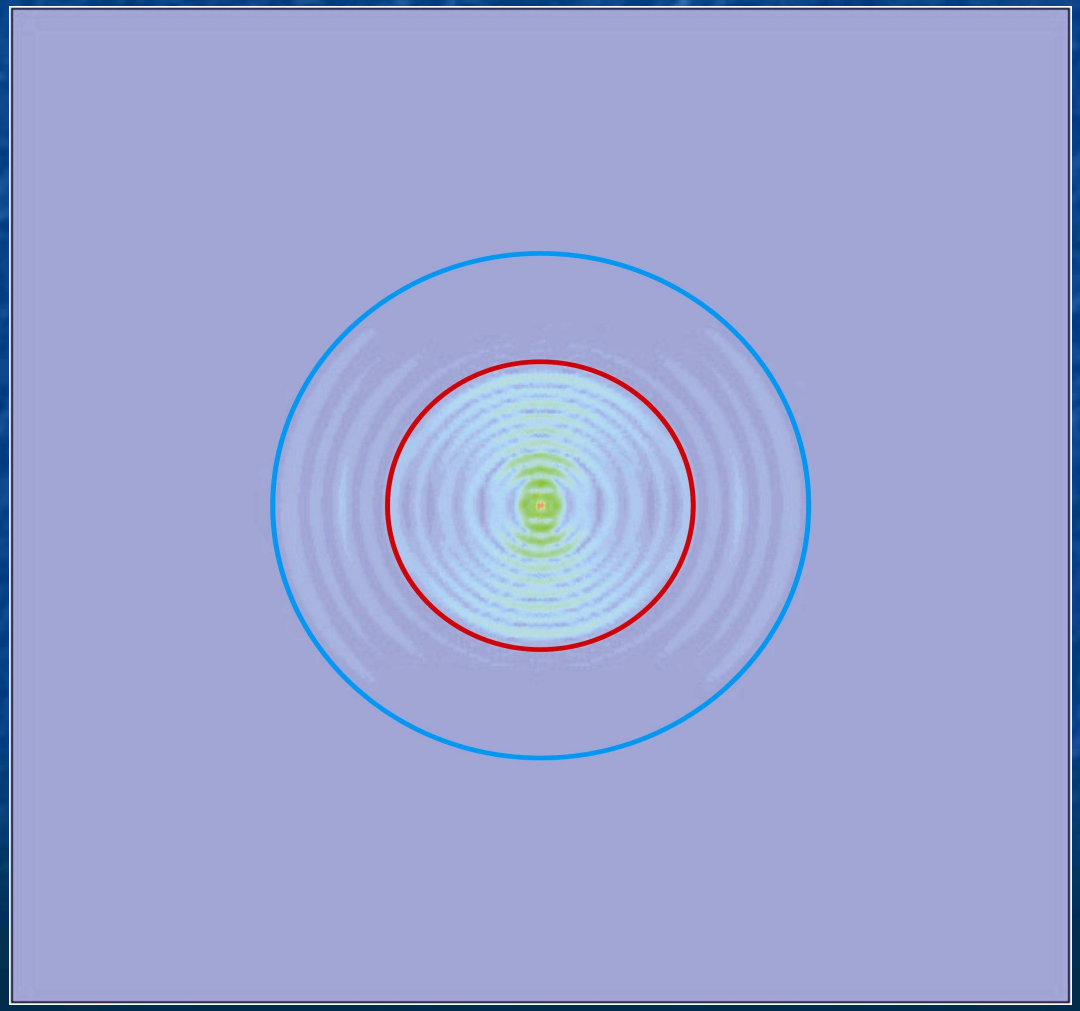

branch b1

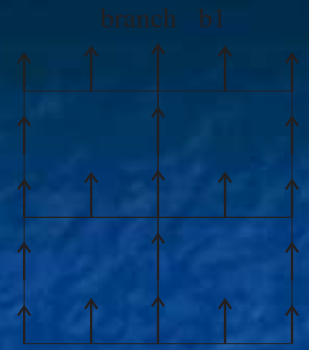

branch b2

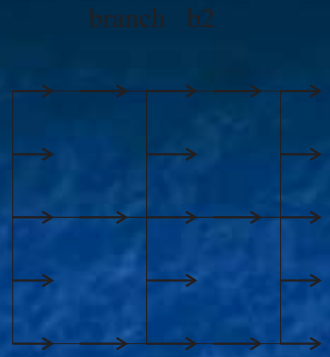
$$\omega H / c_1 = 1.3$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

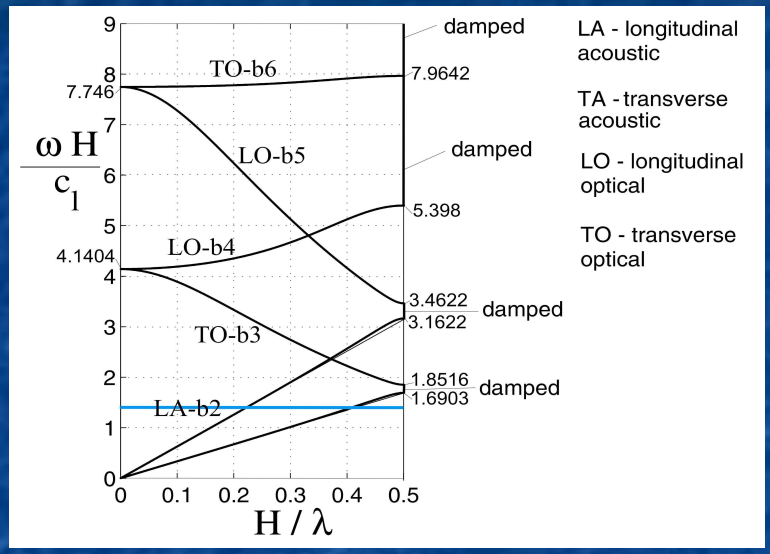

cg /c1
ω · H / c1

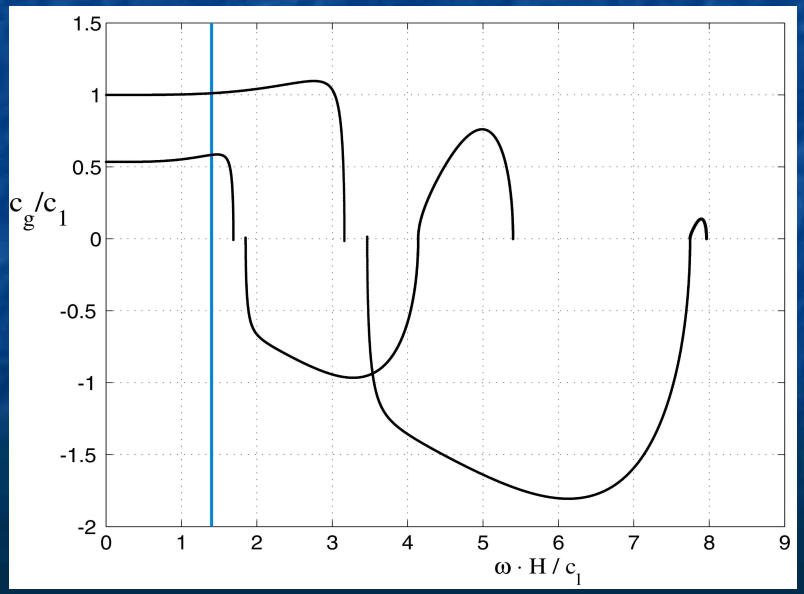


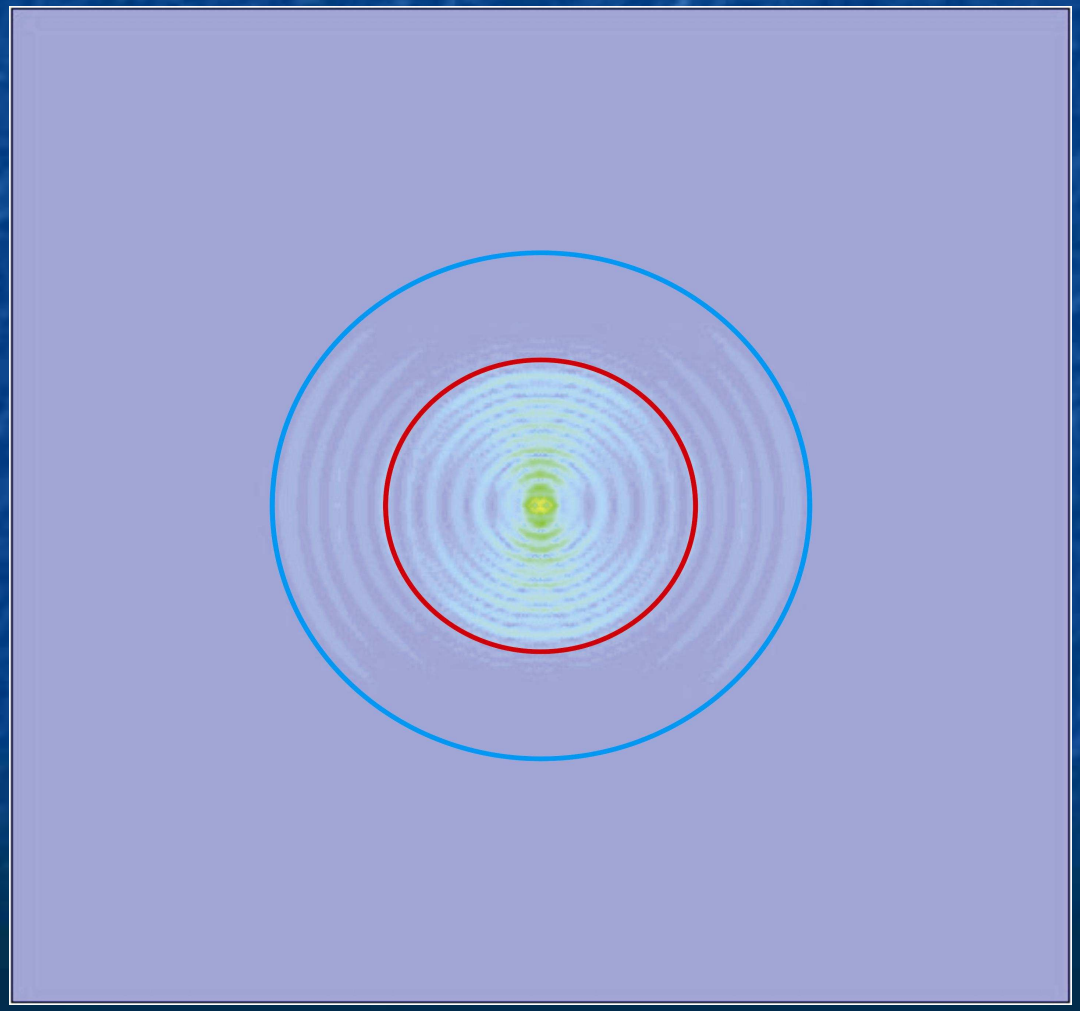

branch b1

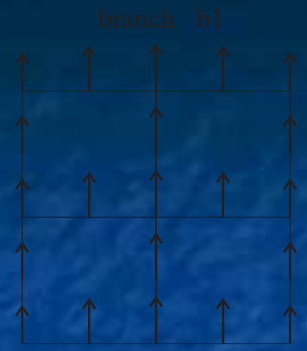

branch b2

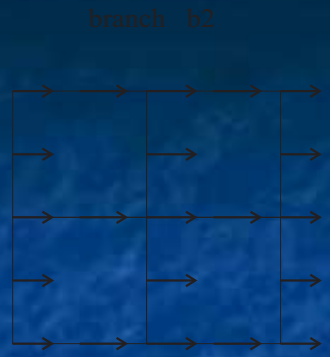
$$\omega H / c_1 = 1.4$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

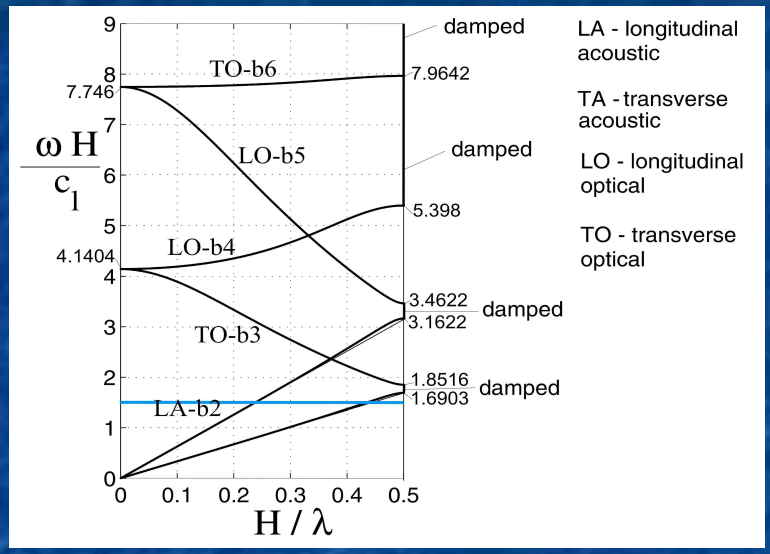

cg /c1
ω · H / c1

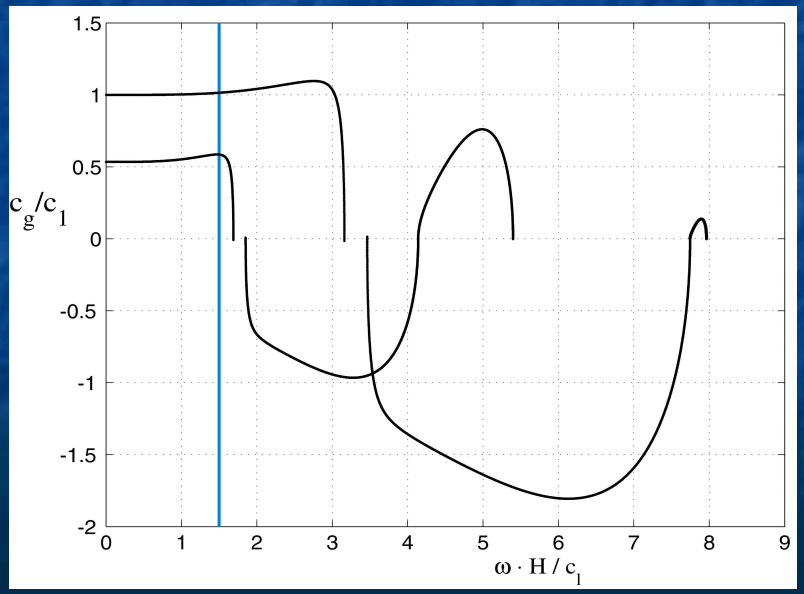


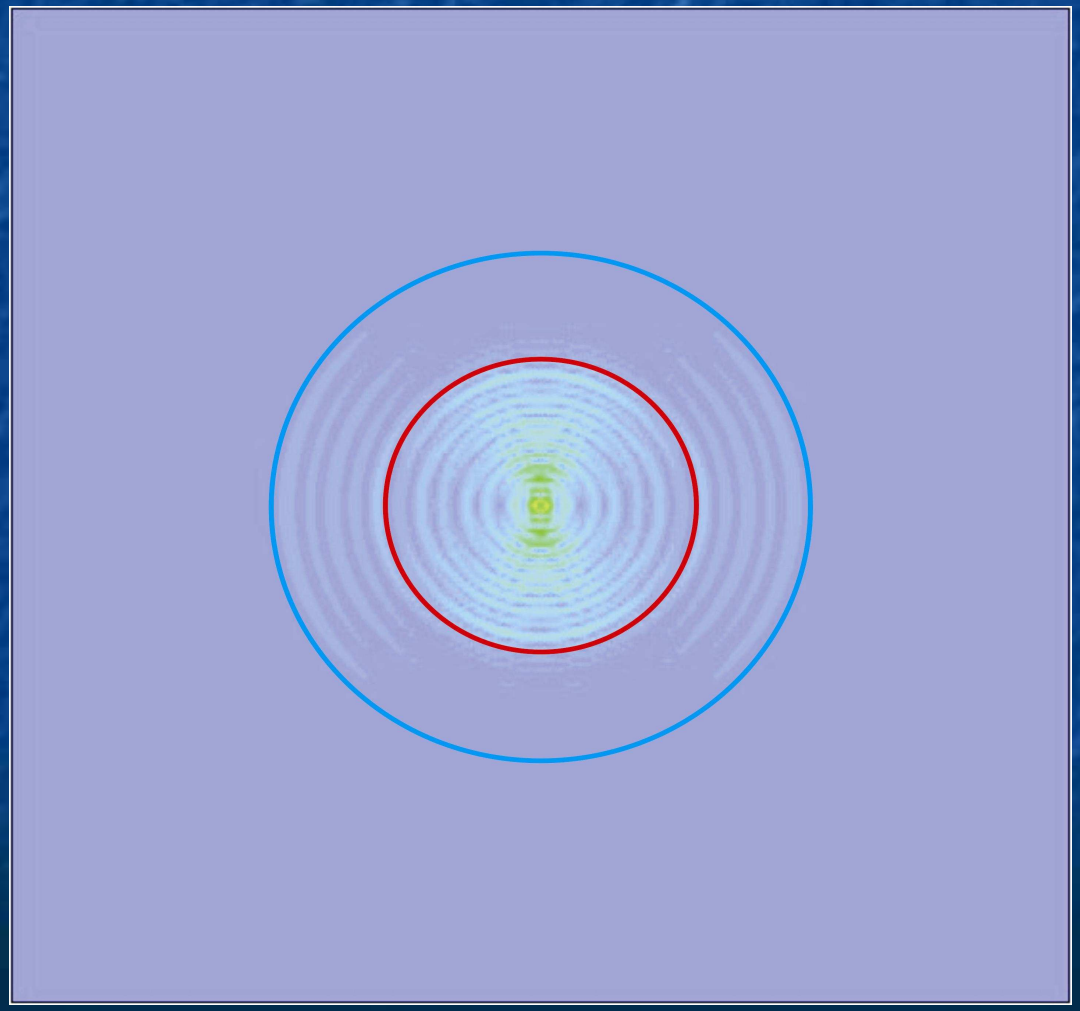

branch b1

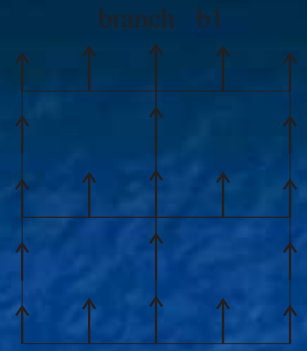

branch b2

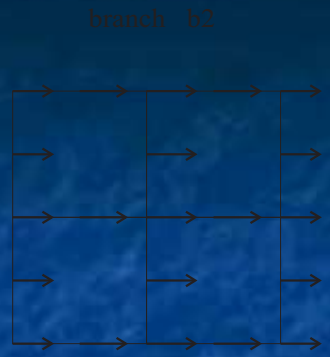
$$\omega H / c_1 = 1.5$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

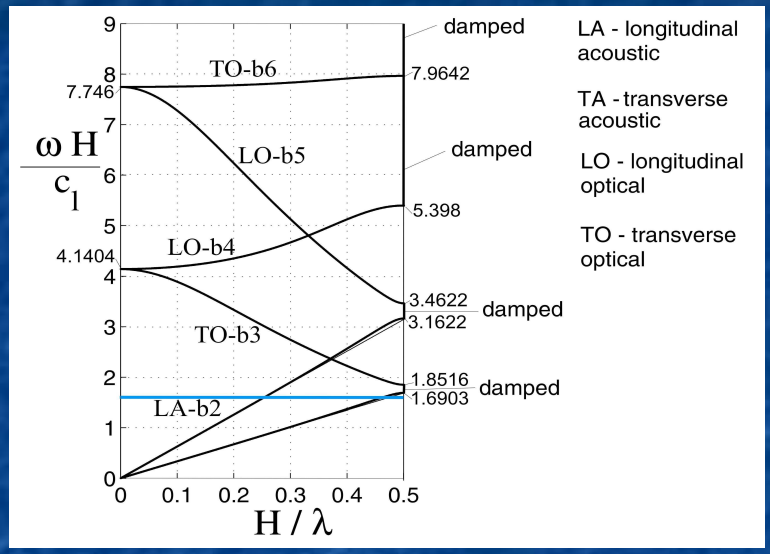

cg /c1
ω · H / c1

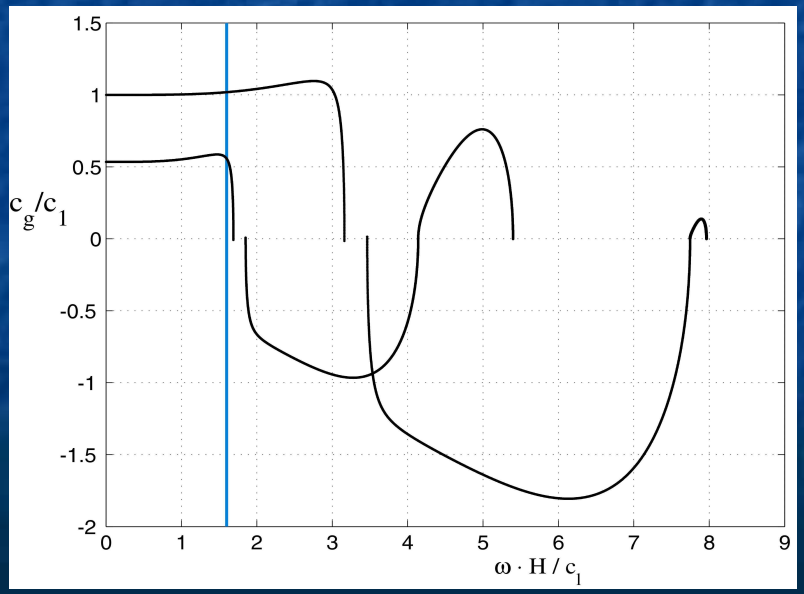


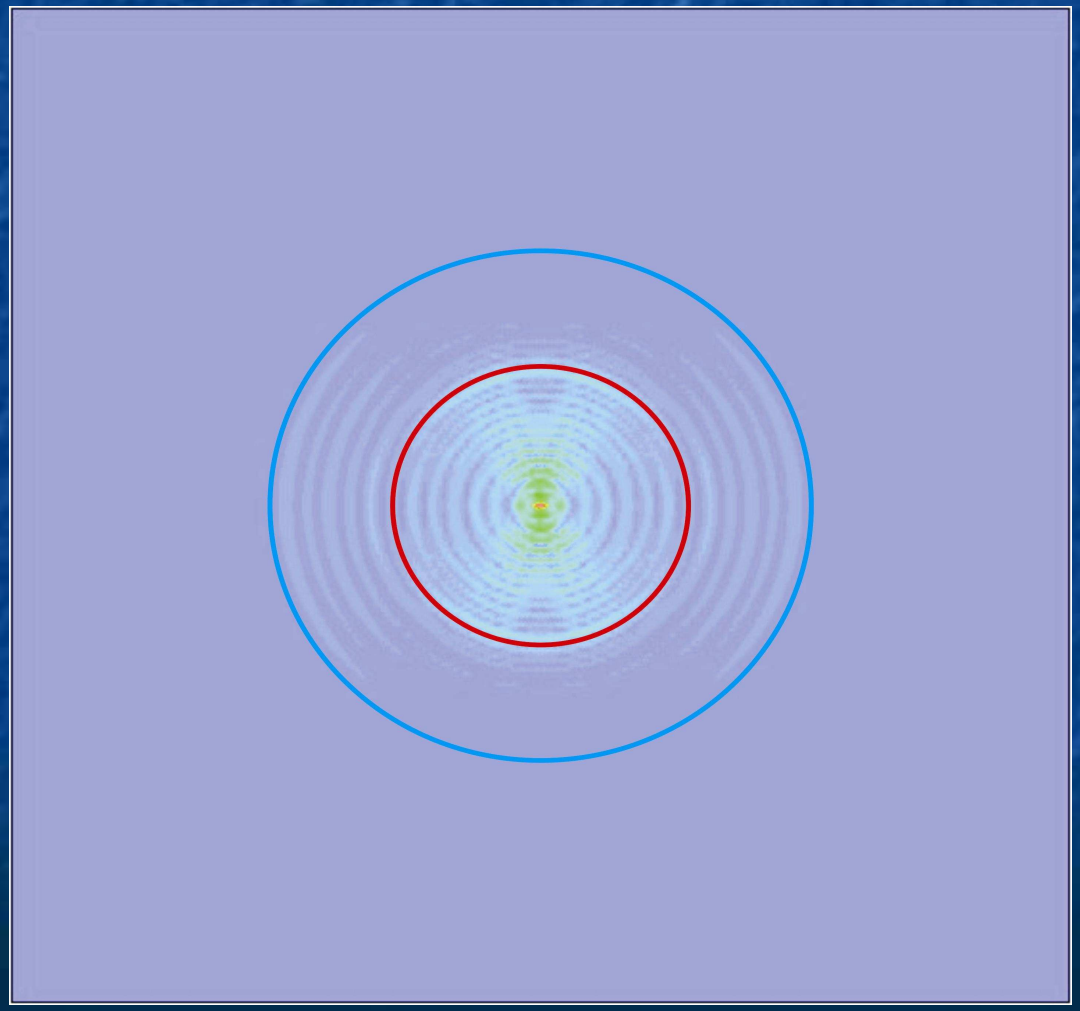

branch b1


branch b2

$$\omega H / c_1 = 1.6$$

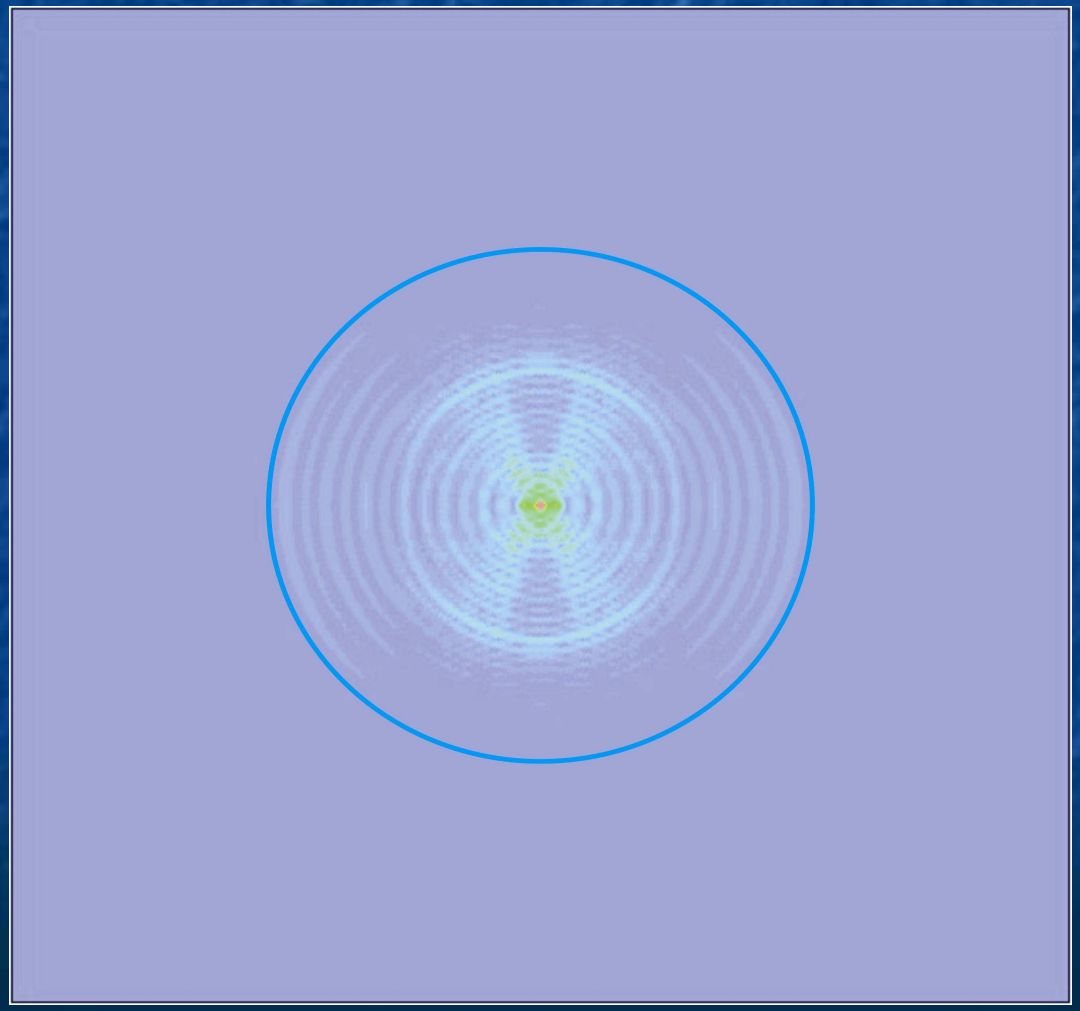

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

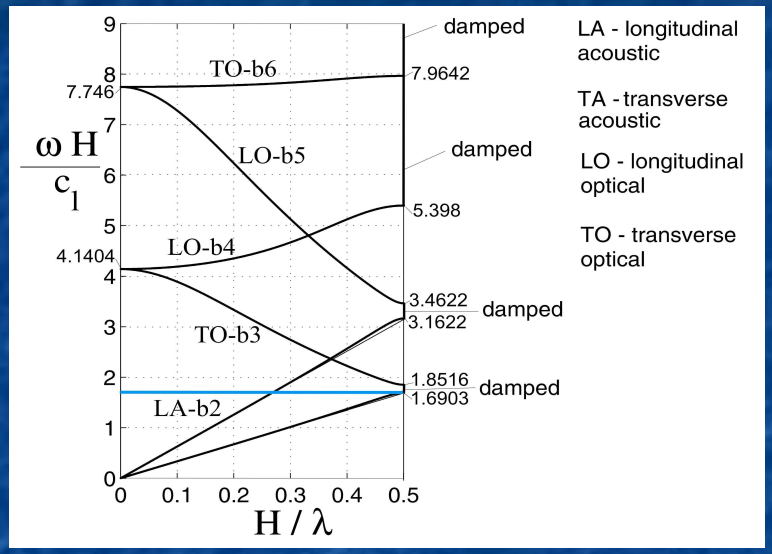

cg /c1
ω · H / c1

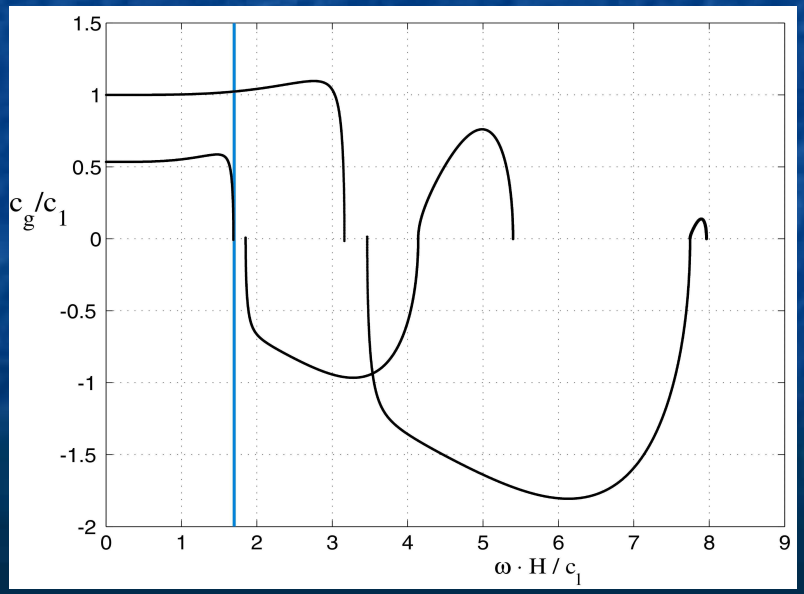


branch b2

$$\omega H / c_1 = 1.7$$

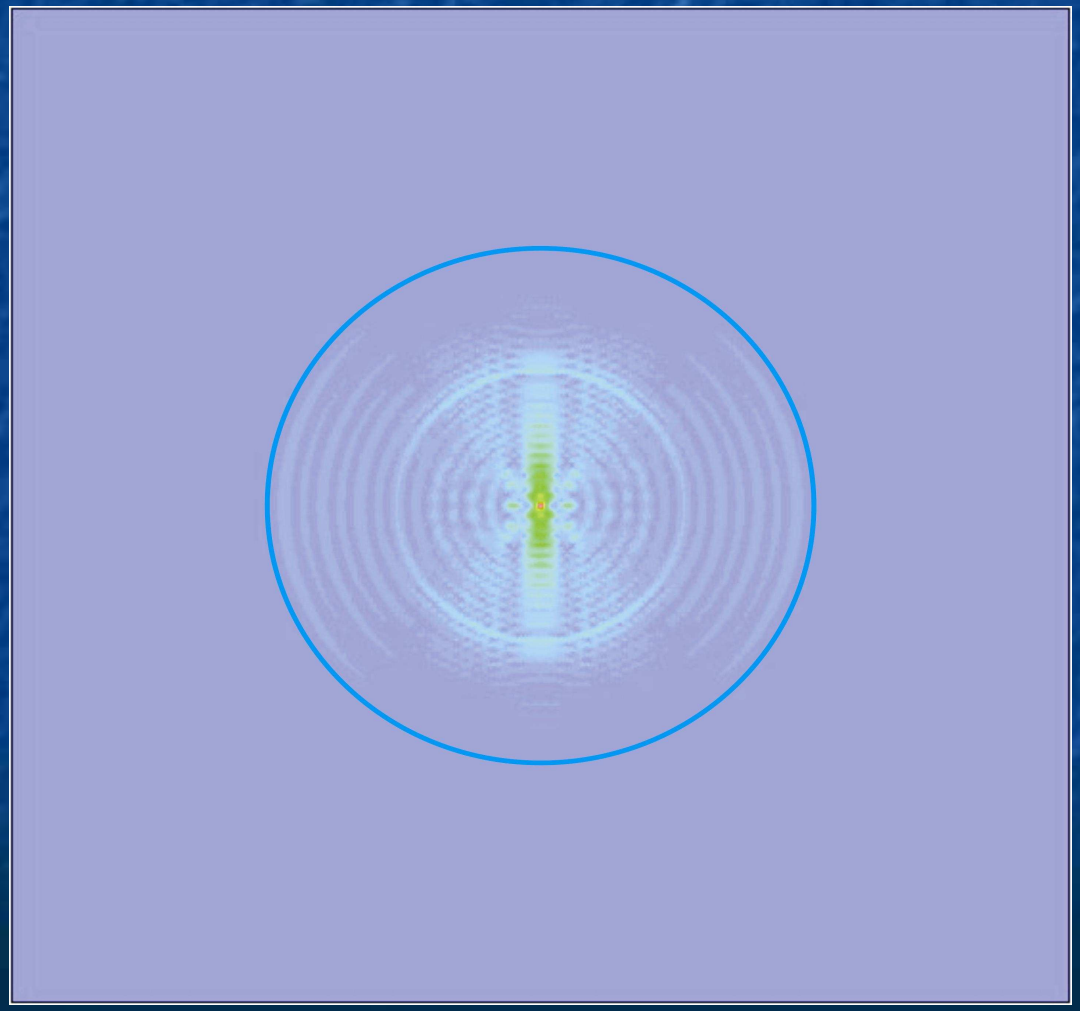


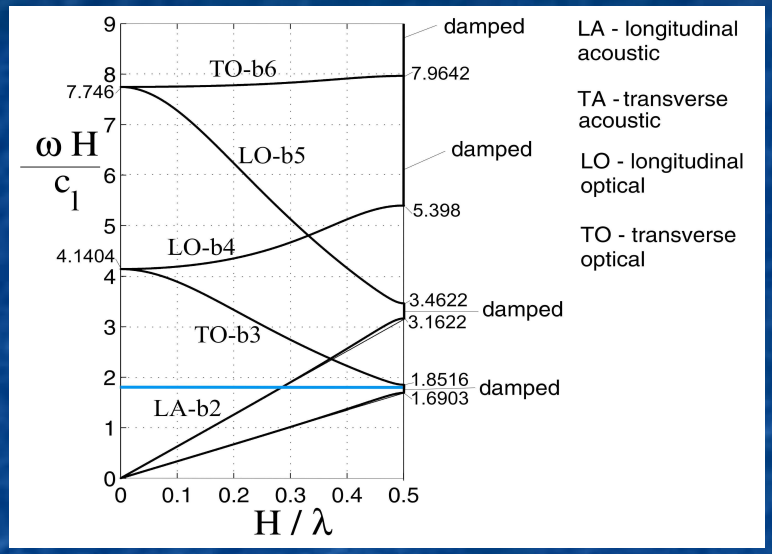


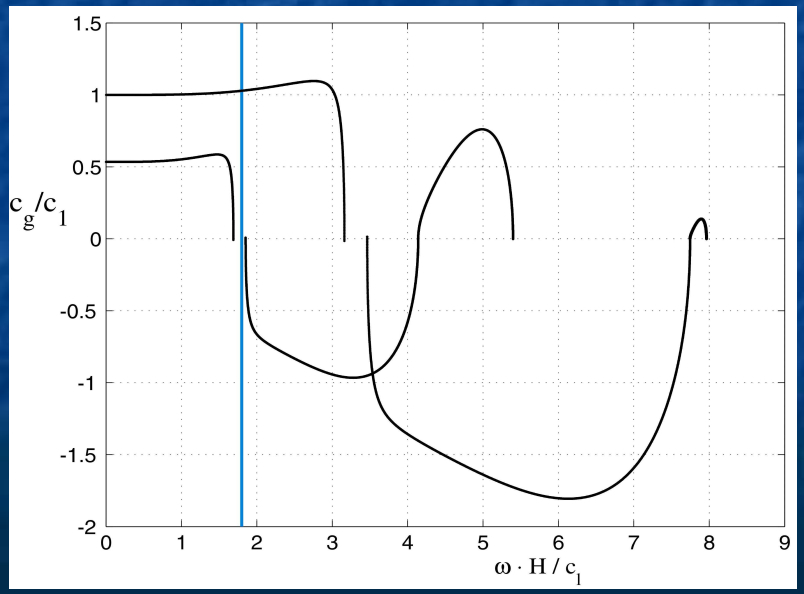


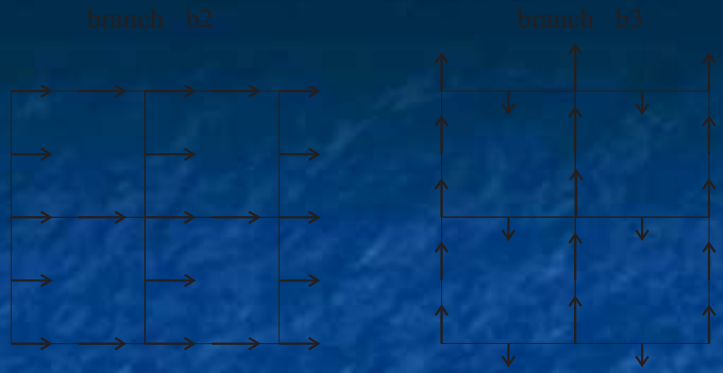
branch b2

$$\omega H / c_1 = 1.8$$

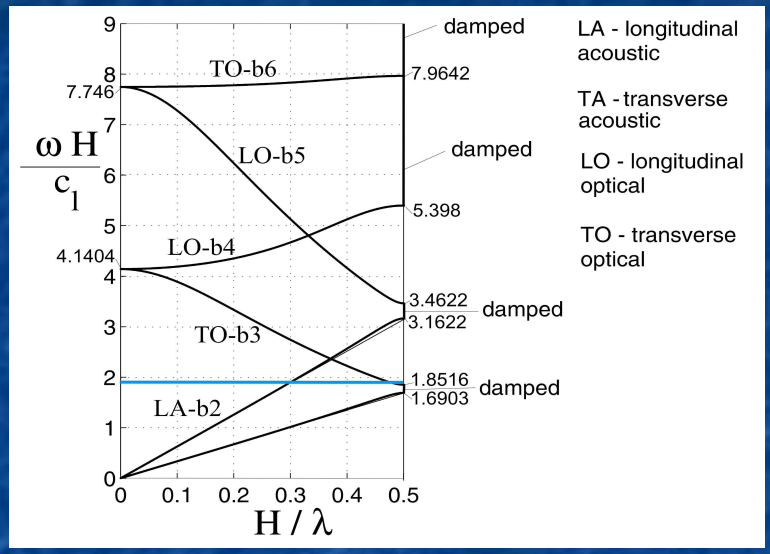


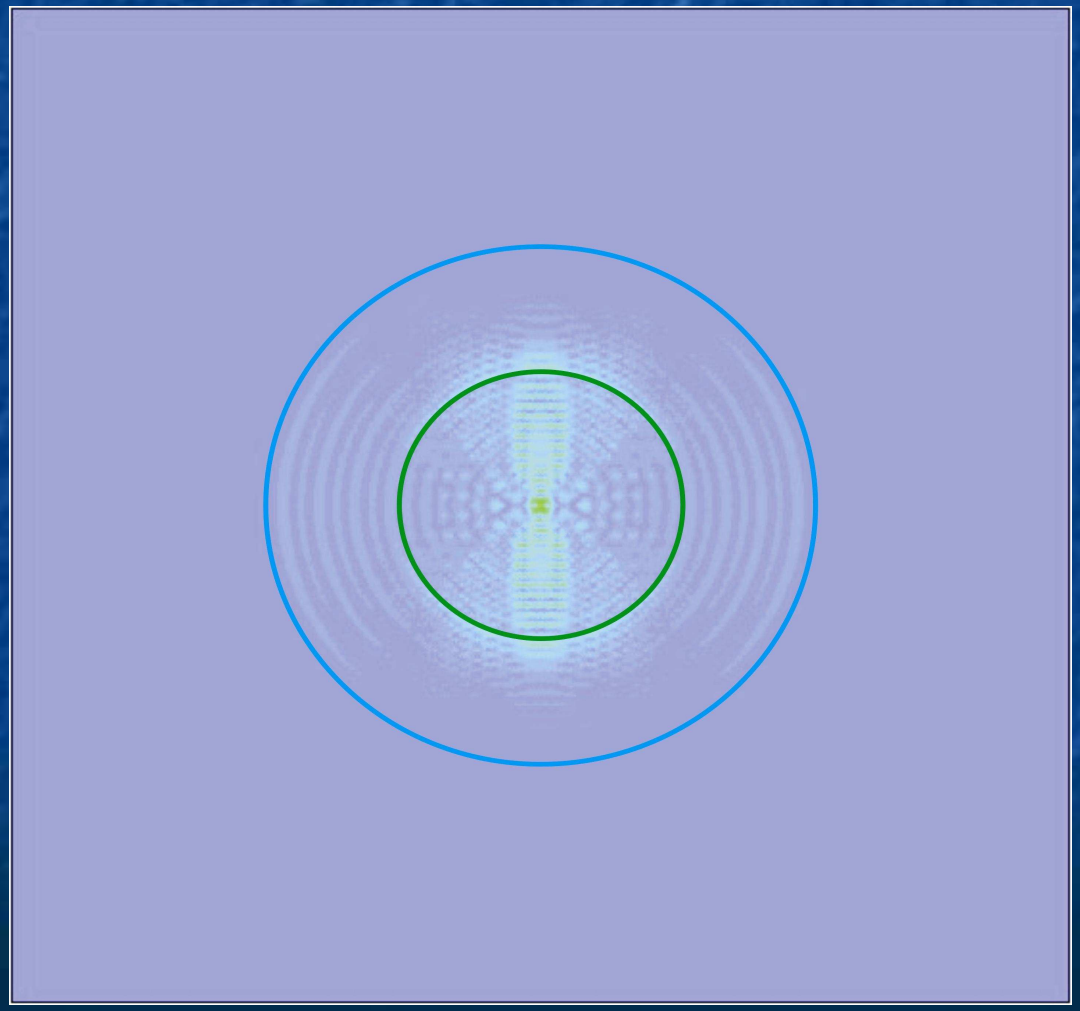


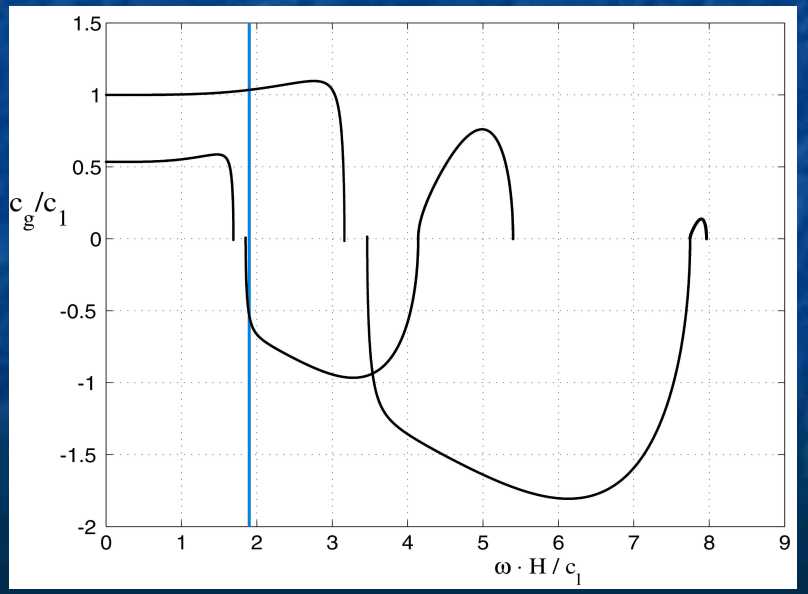


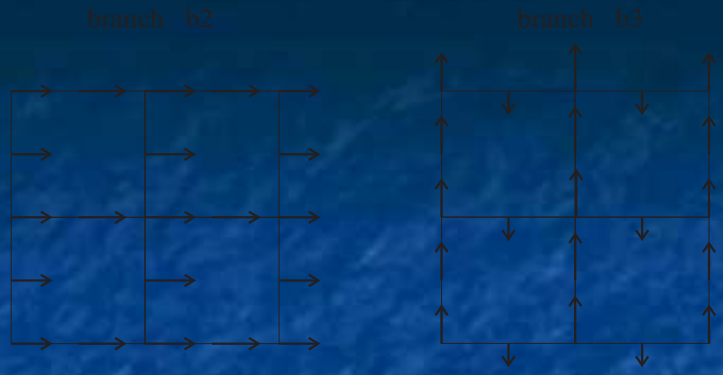

branch b2
branch b3

$$\omega H / c_1 = 1.9$$

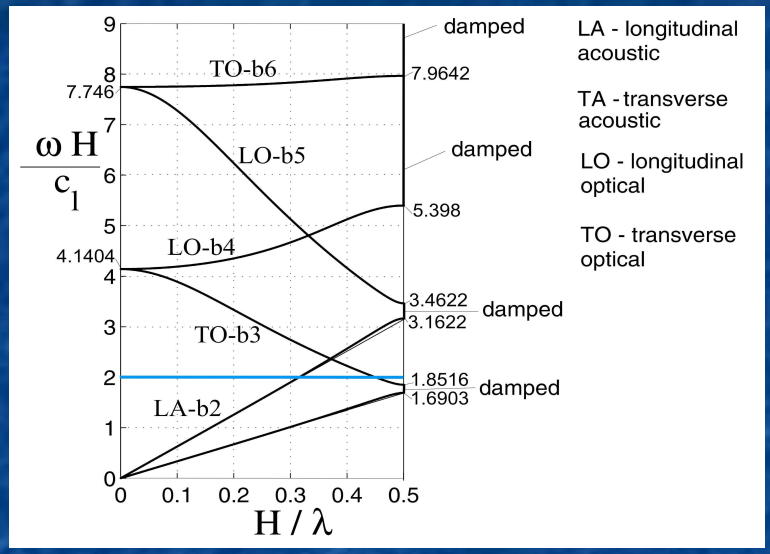

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

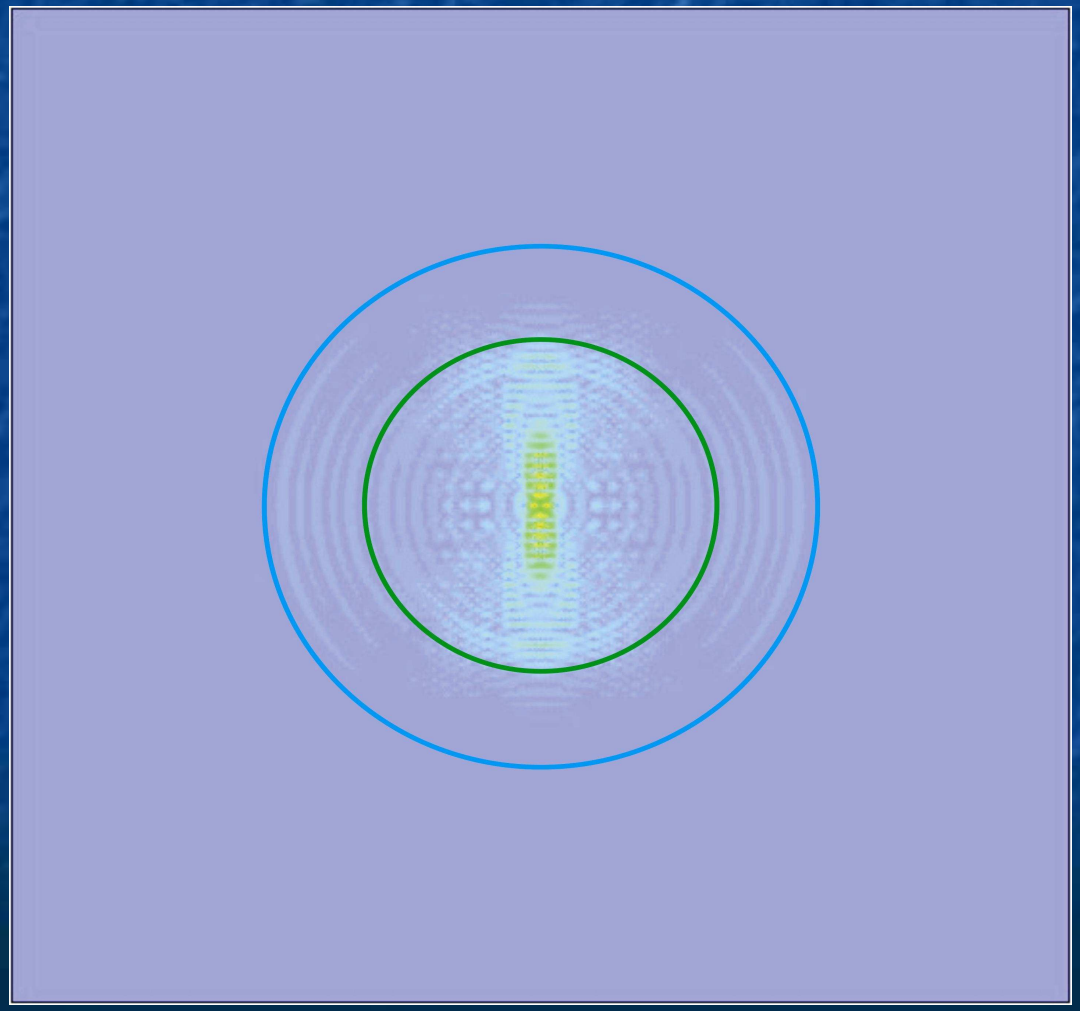


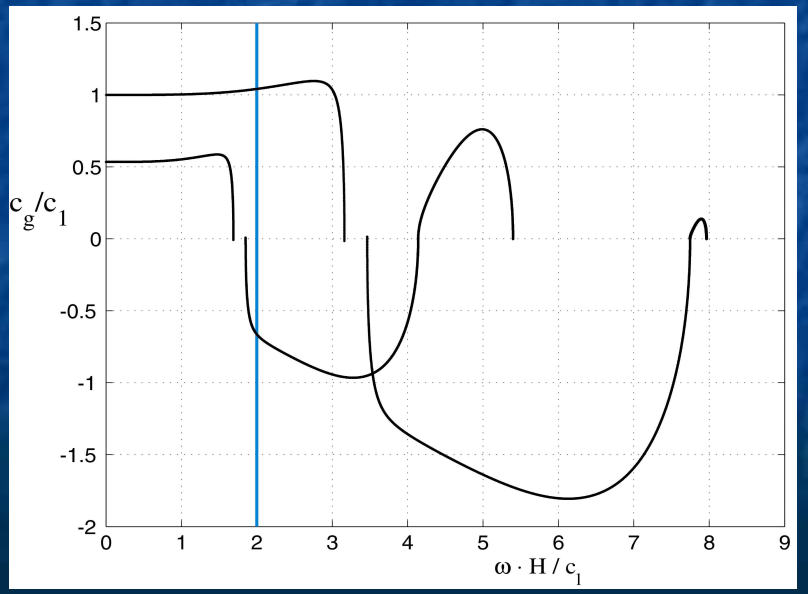

cg/c1
ω · H / c1

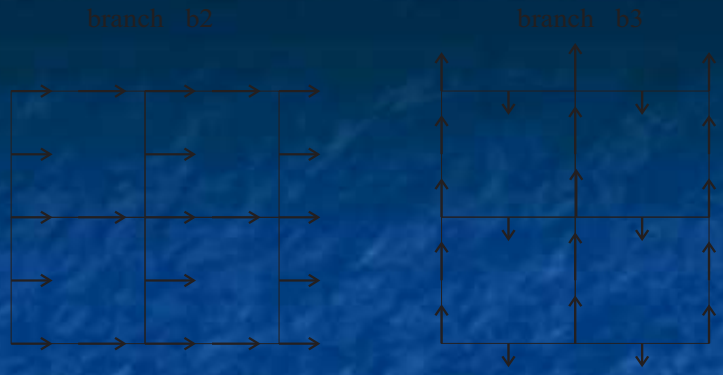

branch b2
branch b3

$$\omega H / c_1 = 2.0$$

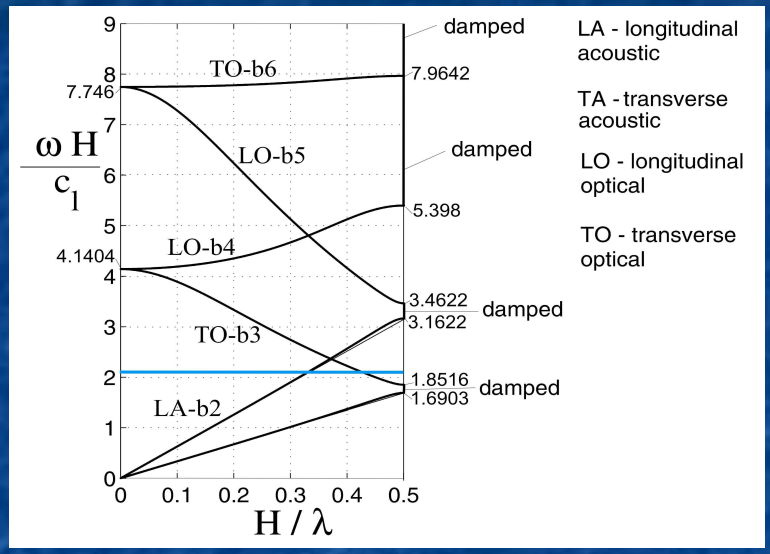

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

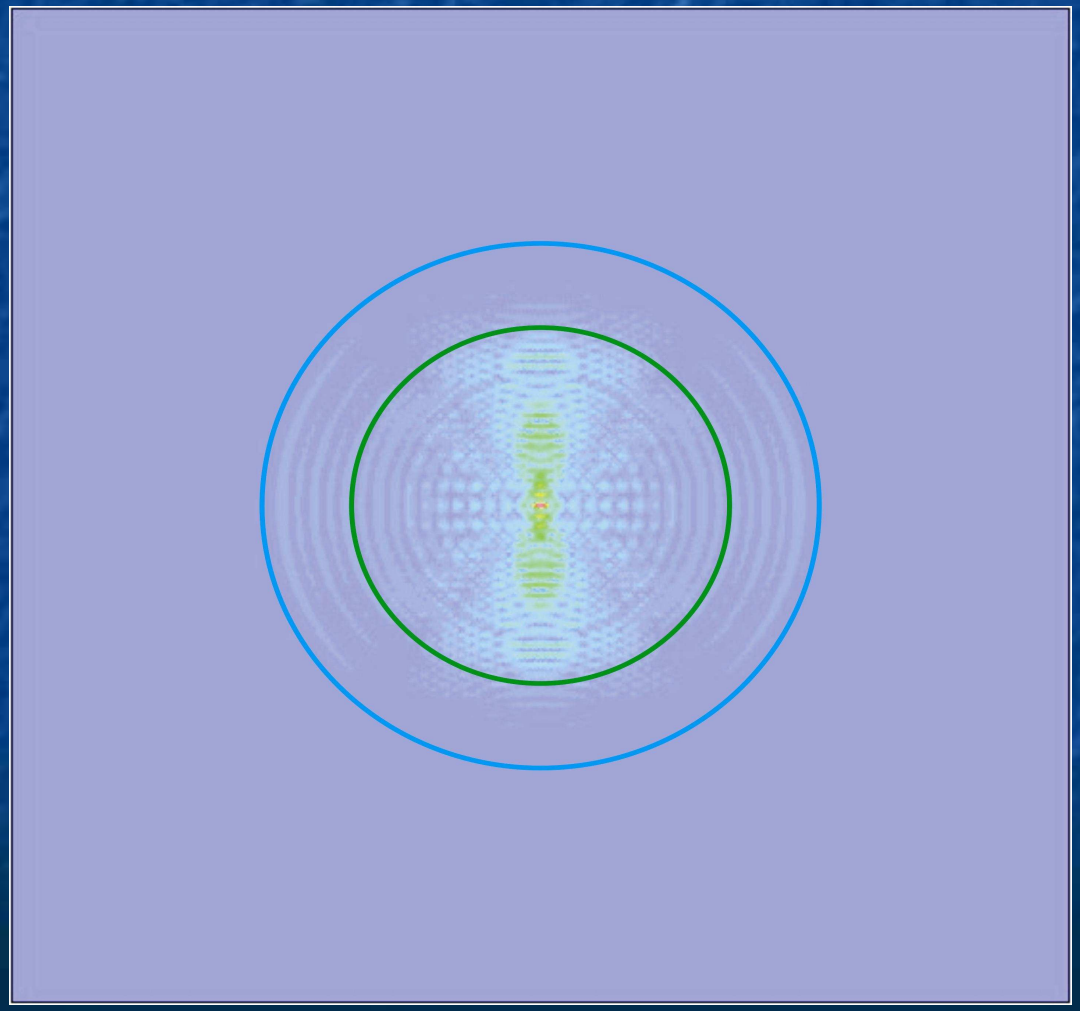


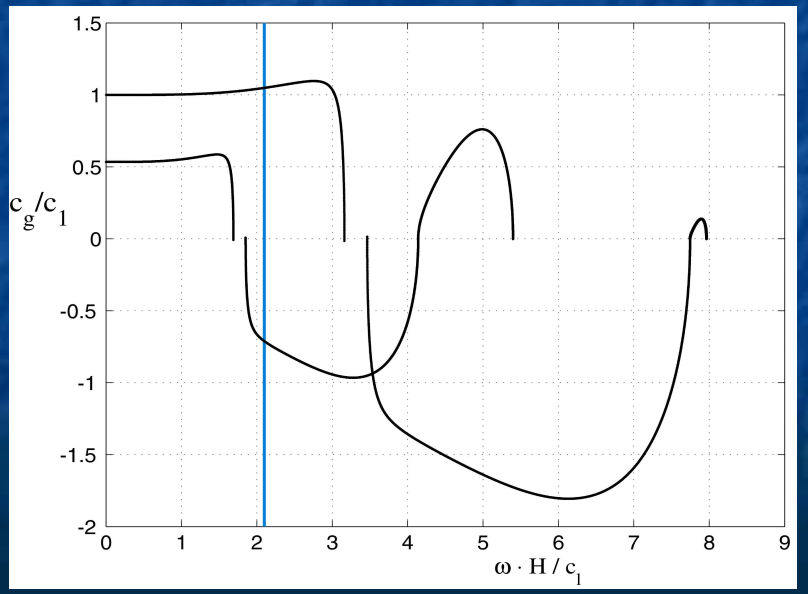

cg/c1
ω · H / c1

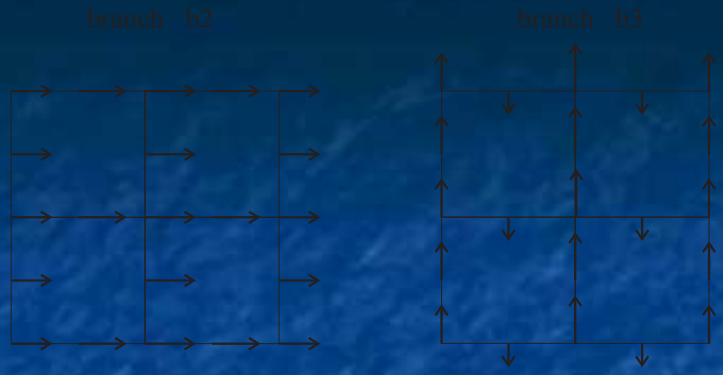

branch b2
branch b3

$$\omega H / c_1 = 2.1$$

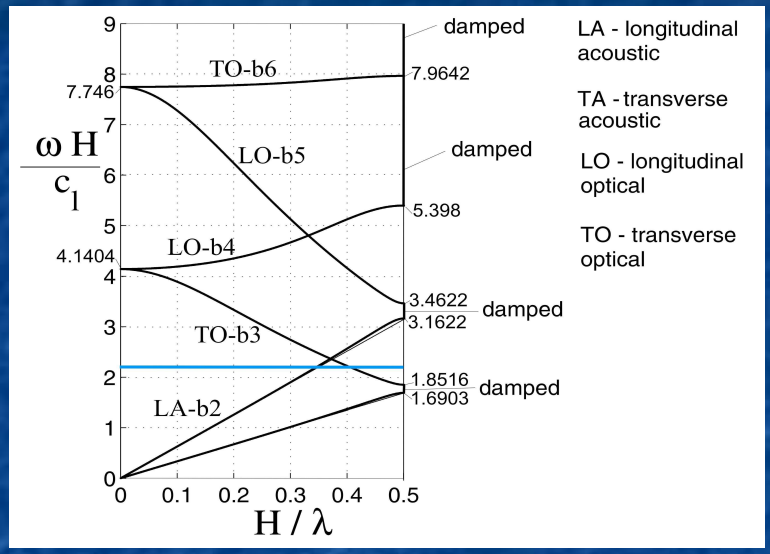

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

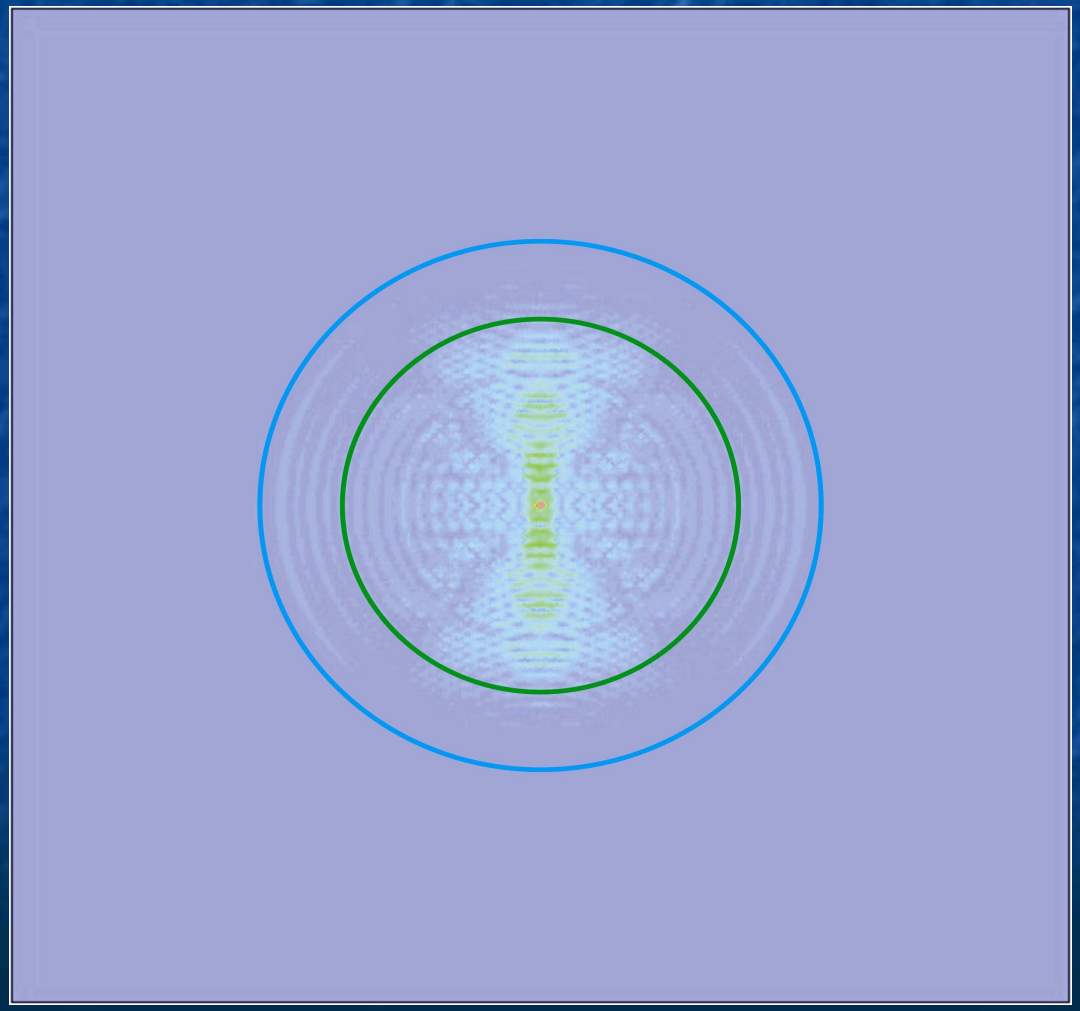


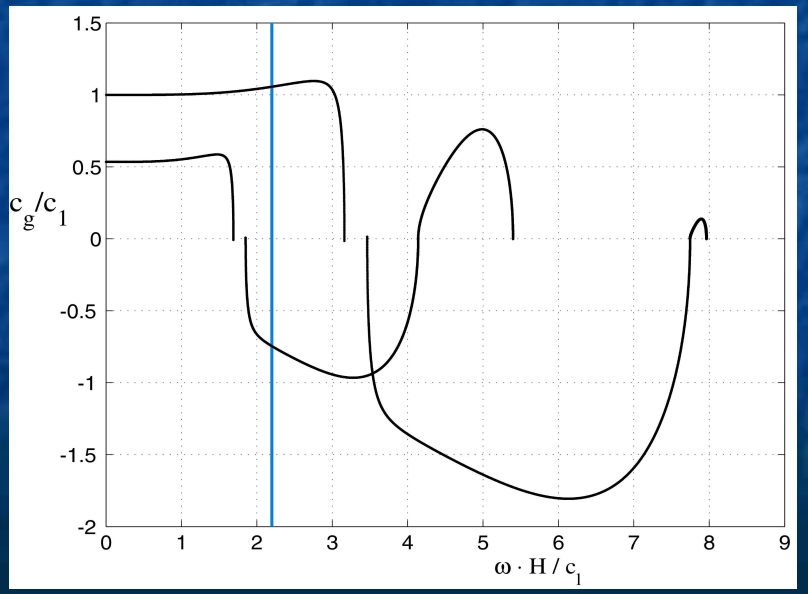

cg/c1
ω · H / c1

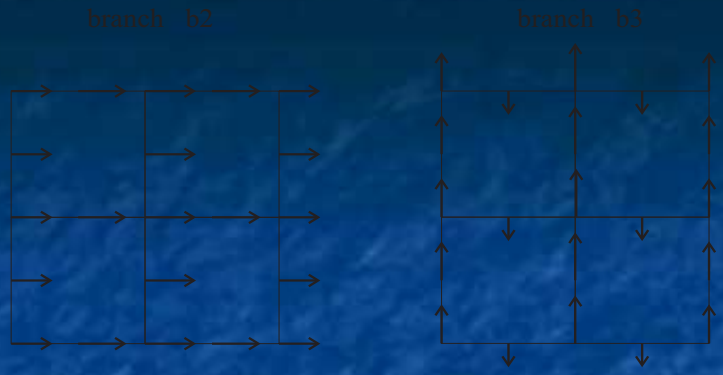

branch b2
branch b3

$$\omega H / c_1 = 2.2$$

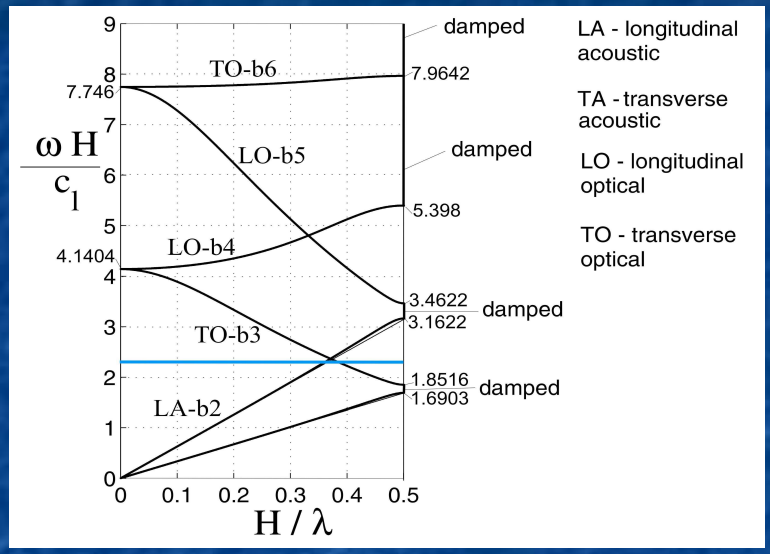

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

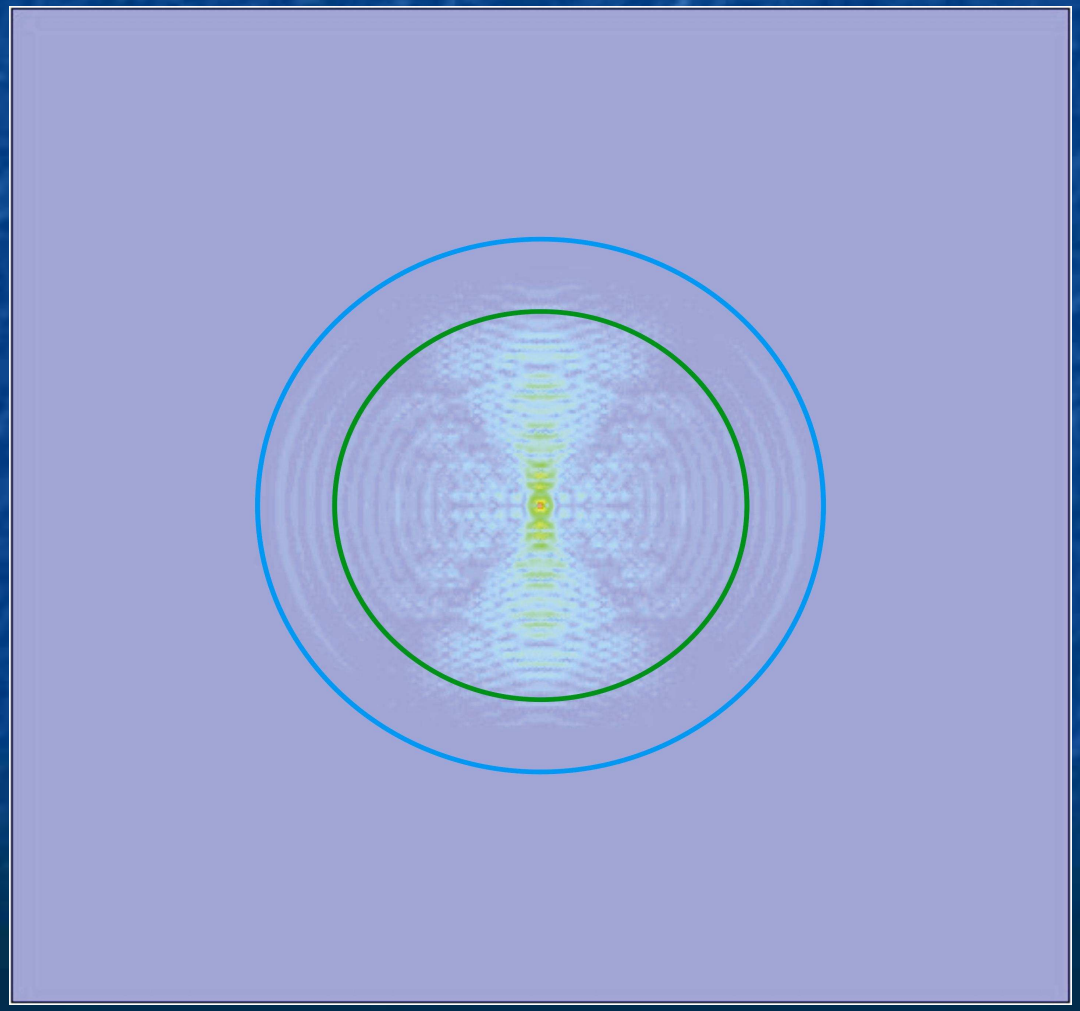


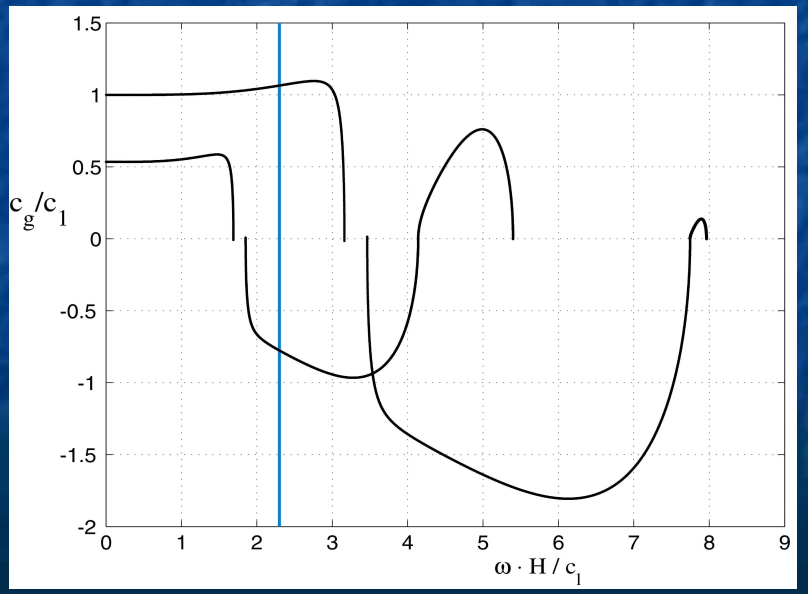

cg/c1
ω · H / c1

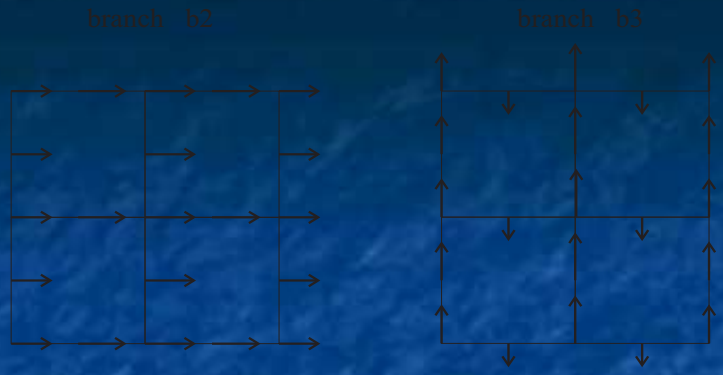

branch b2
branch b3

$$\omega H / c_1 = 2.3$$

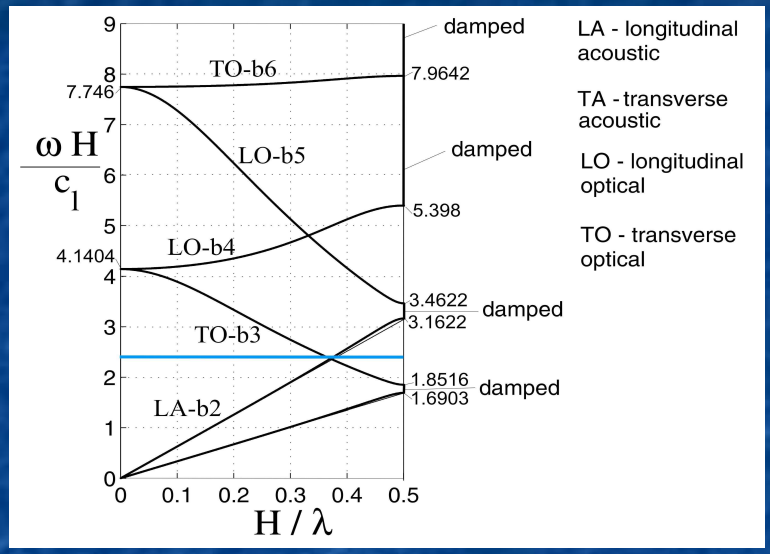

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

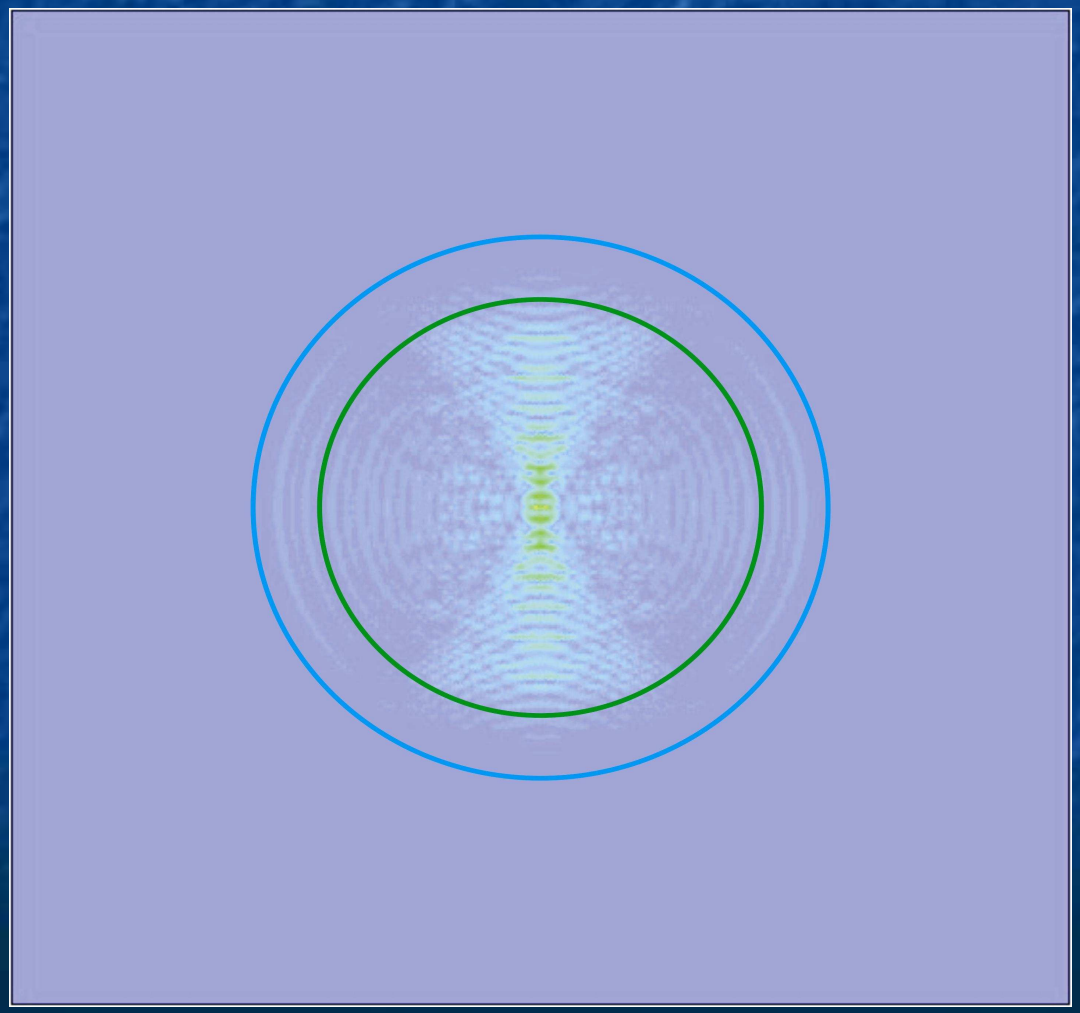


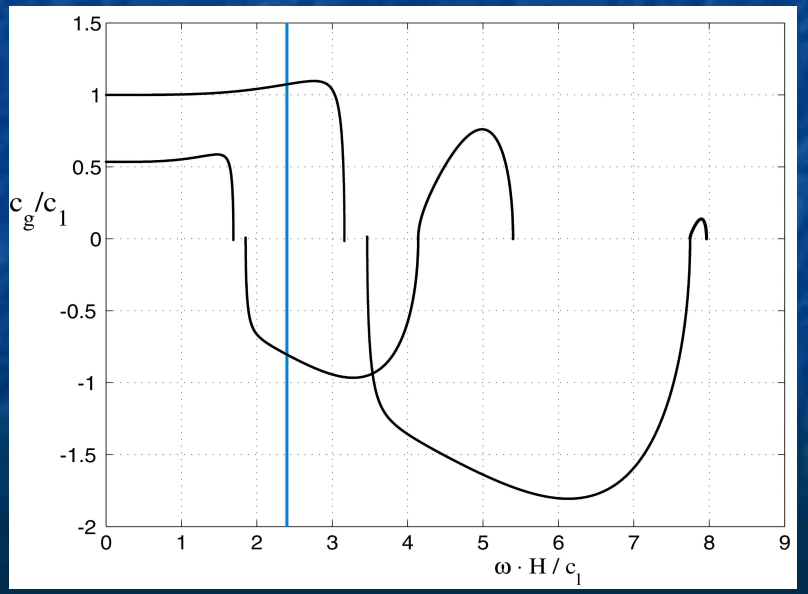

cg/c1
ω · H / c1

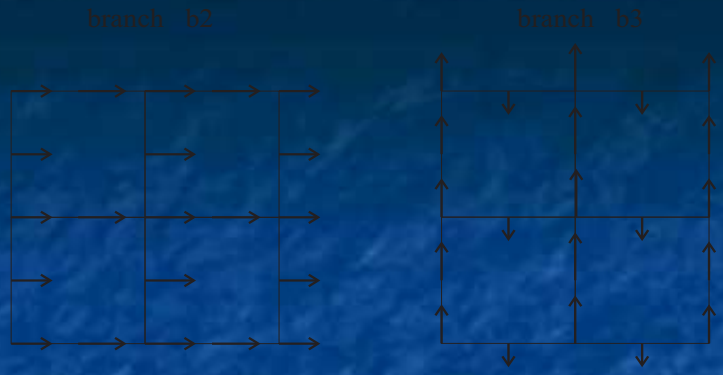

branch b2
branch b3

$$\omega H / c_1 = 2.4$$

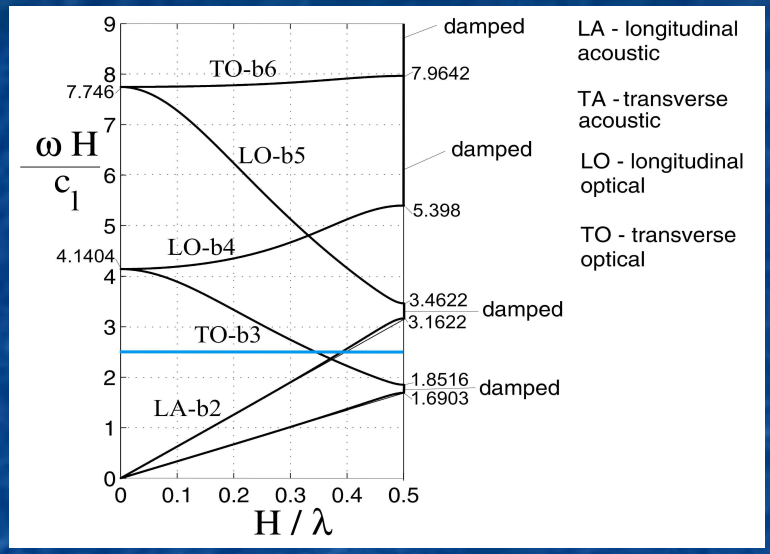

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

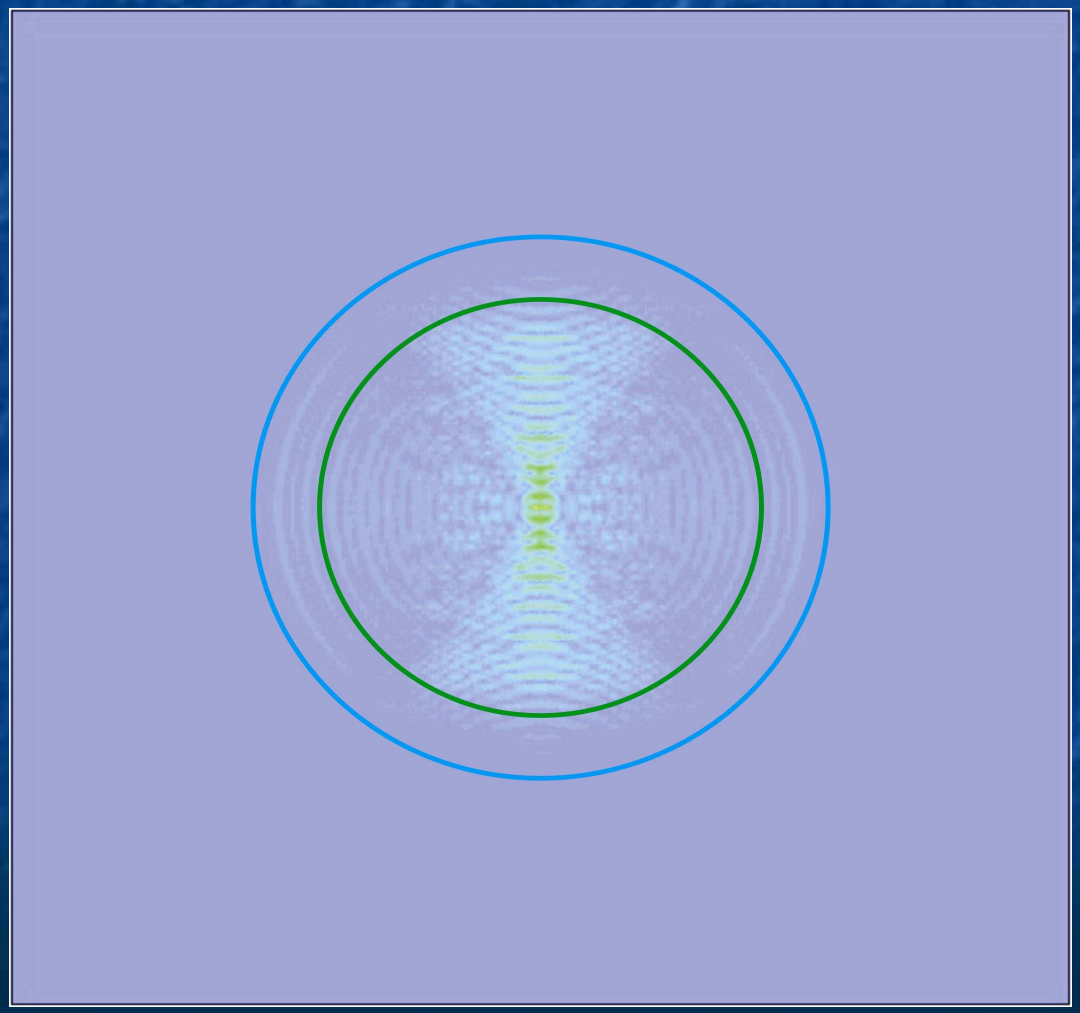


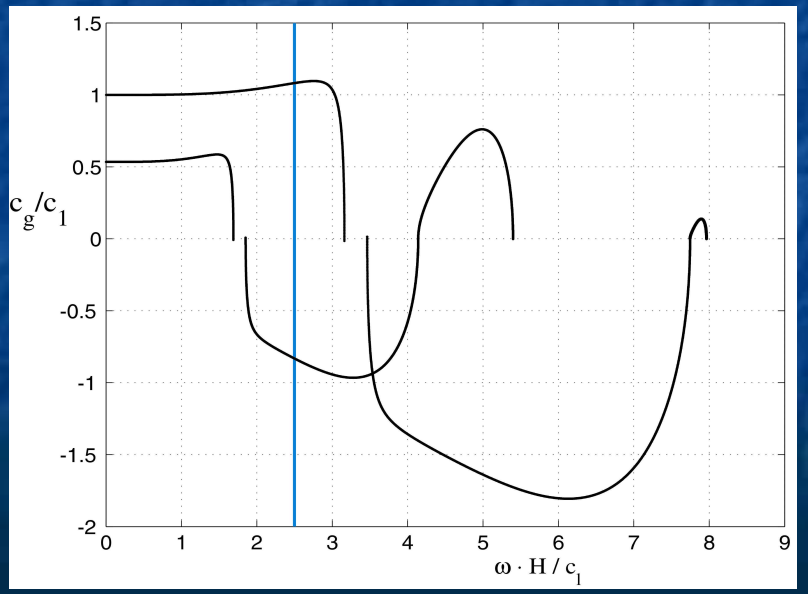

cg/c1
ω · H / c1

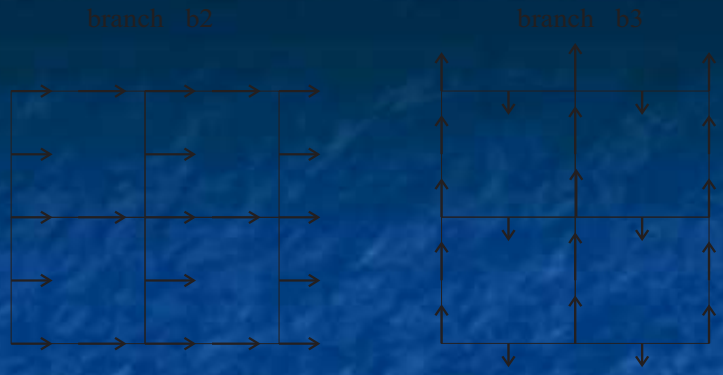

branch b2
branch b3

$$\omega H / c_1 = 2.5$$

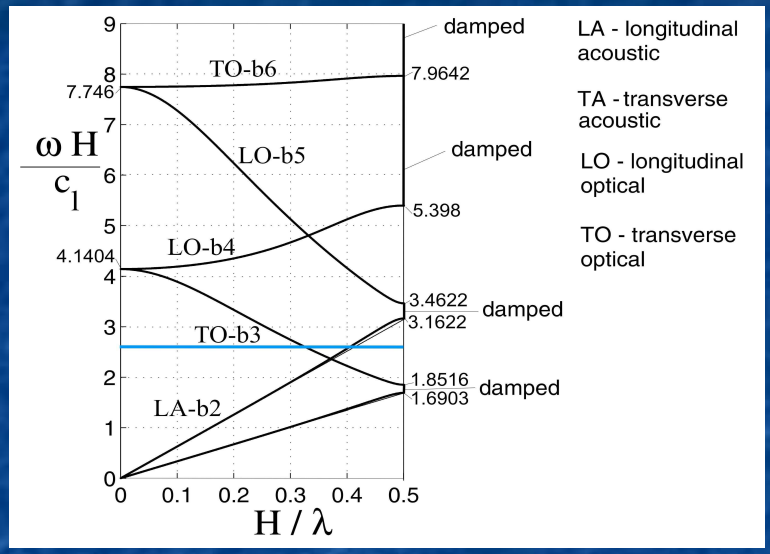

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

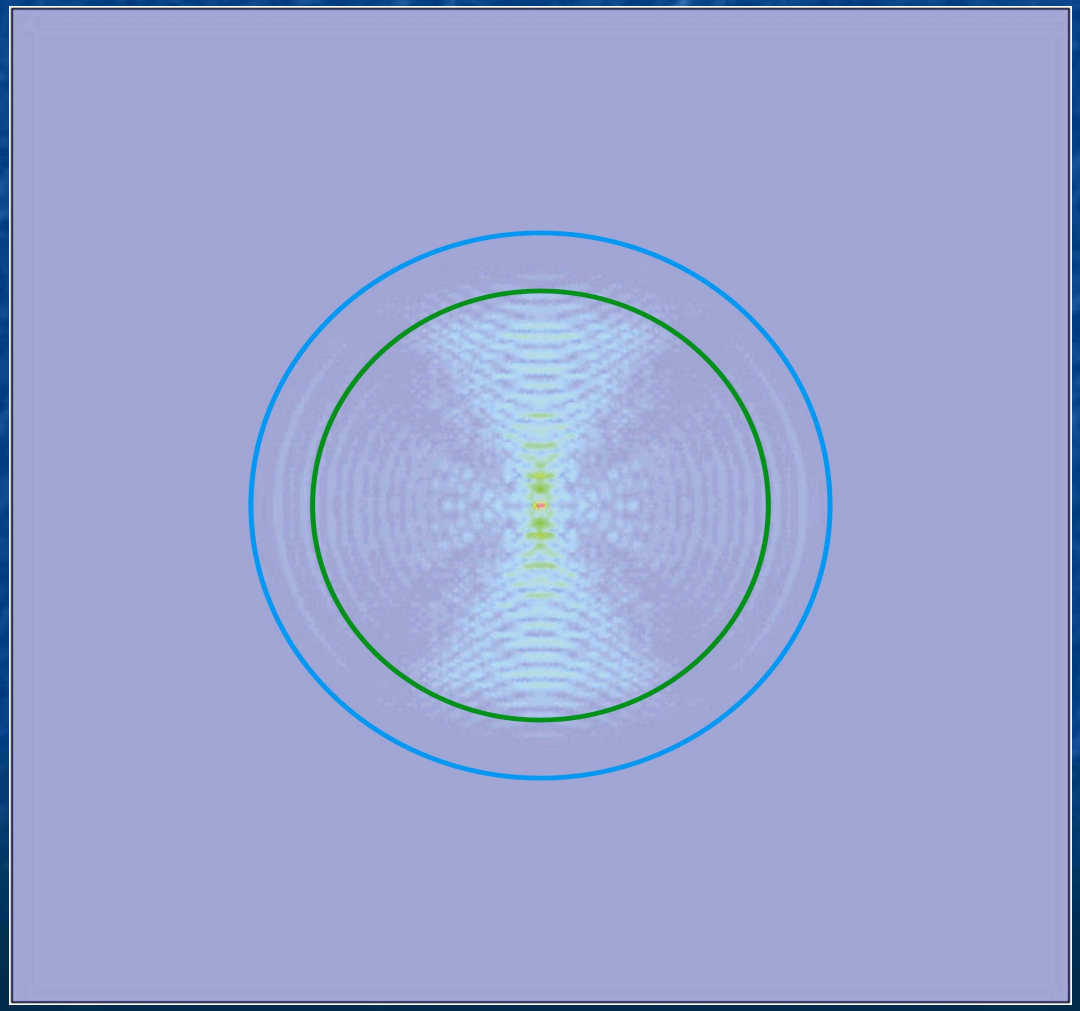


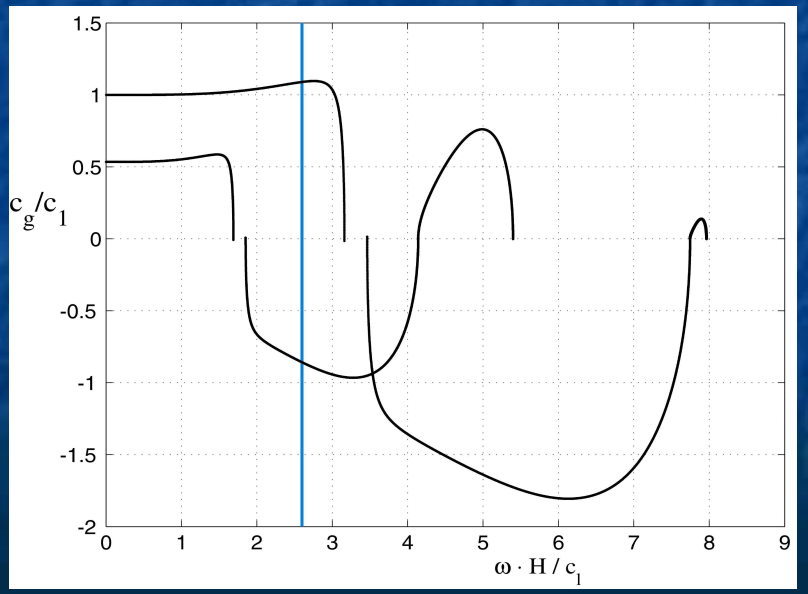

cg/c1
ω · H / c1

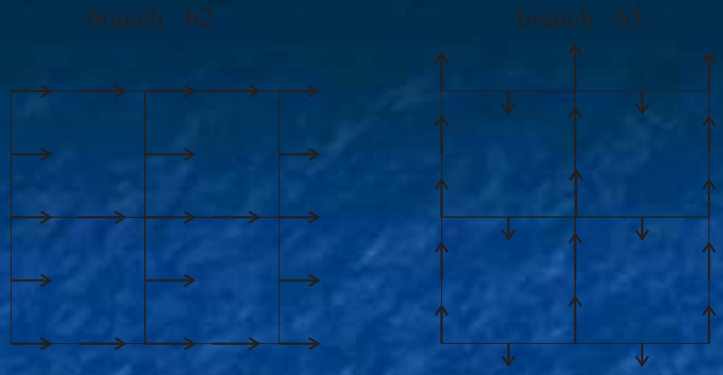

branch b2
branch b3

$$\omega H / c_1 = 2.6$$

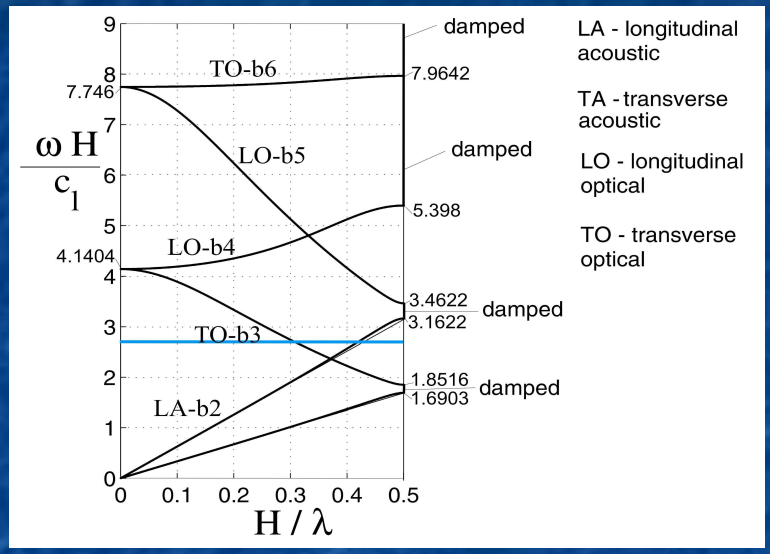

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

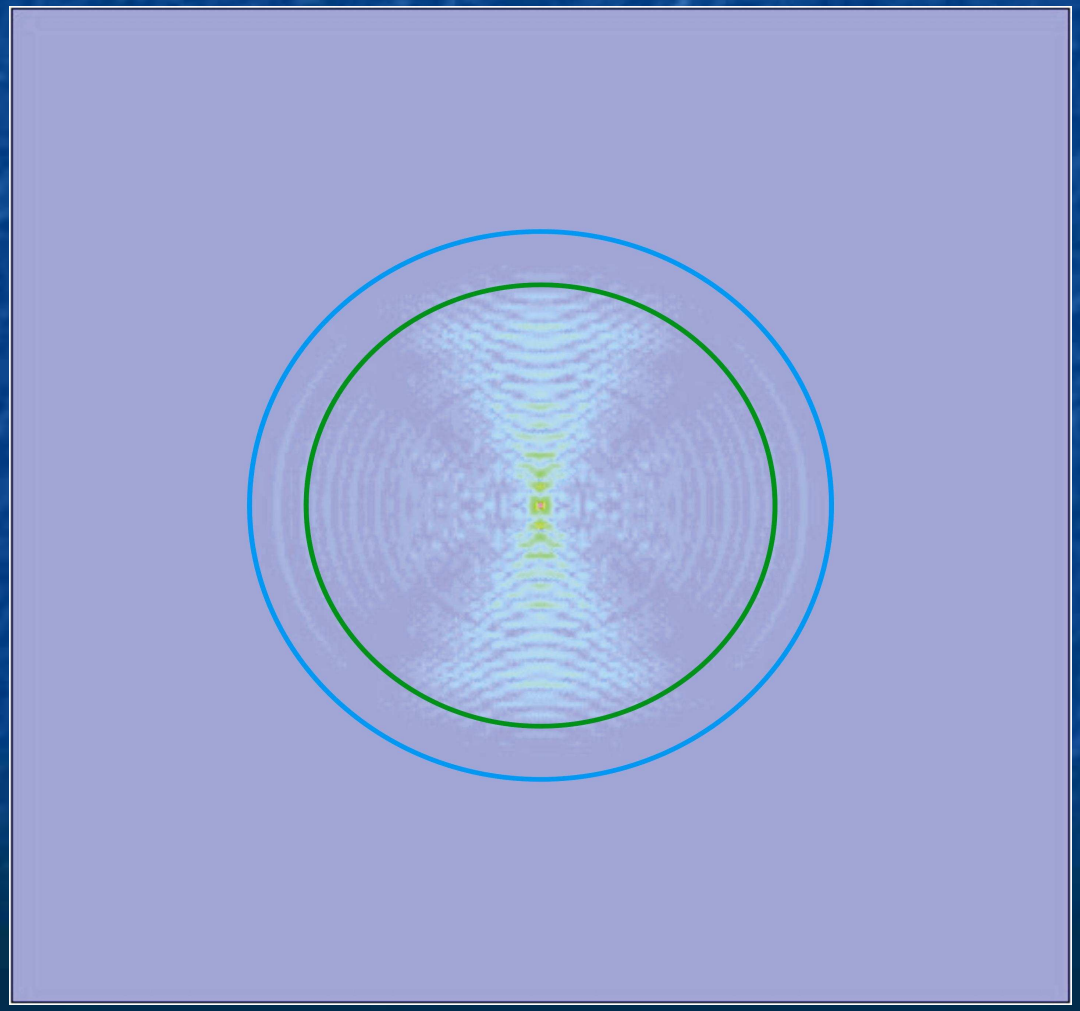


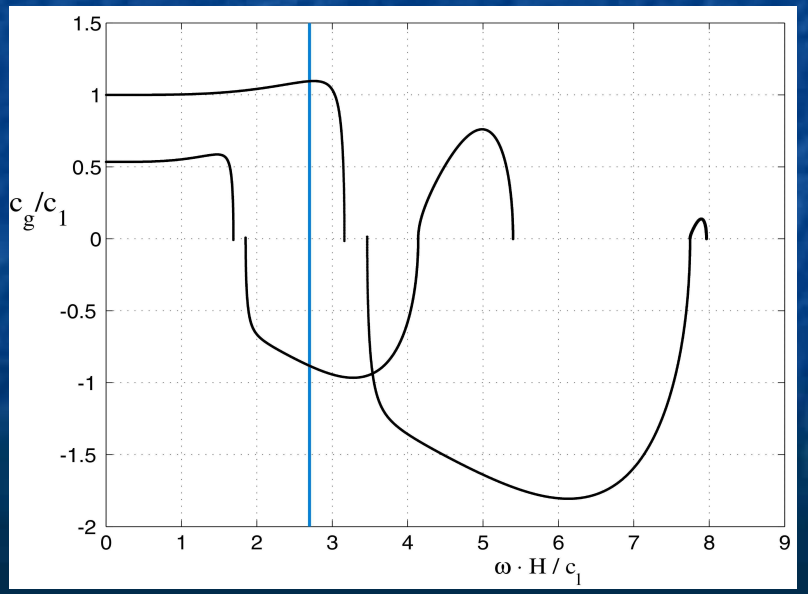

cg/c1
ω · H / c1

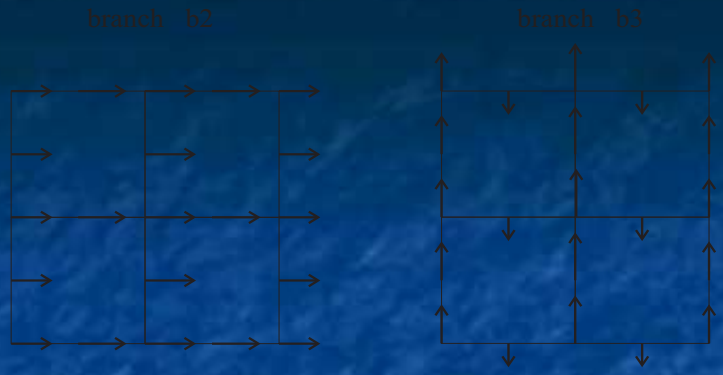

branch b2
branch b3

$$\omega H / c_1 = 2.7$$

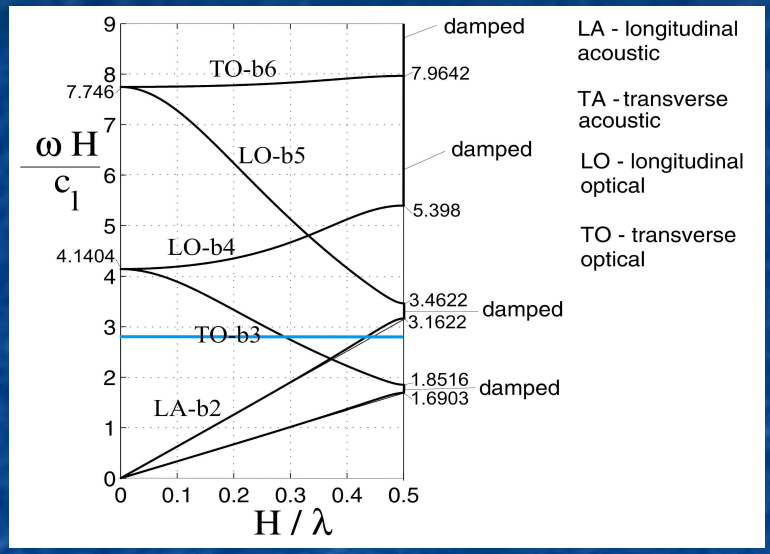

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

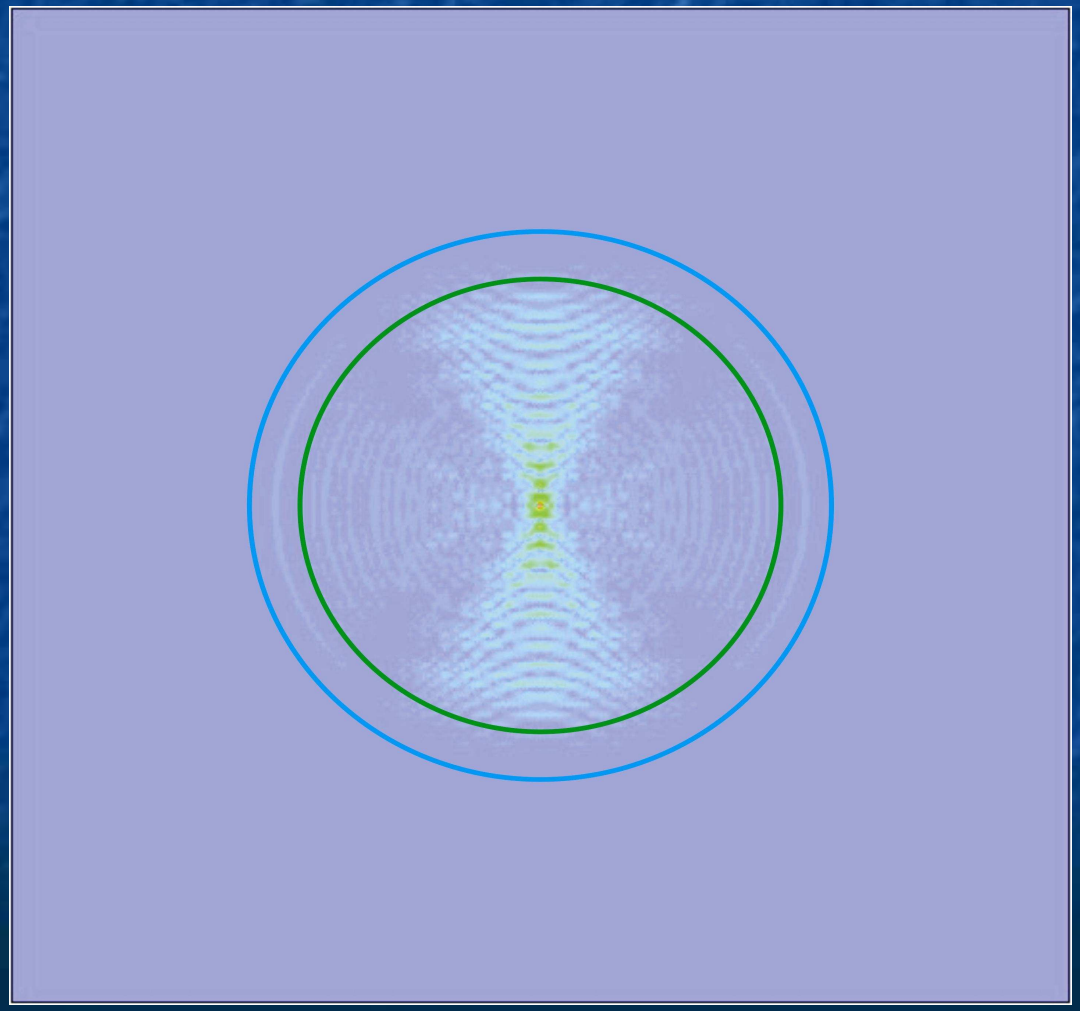


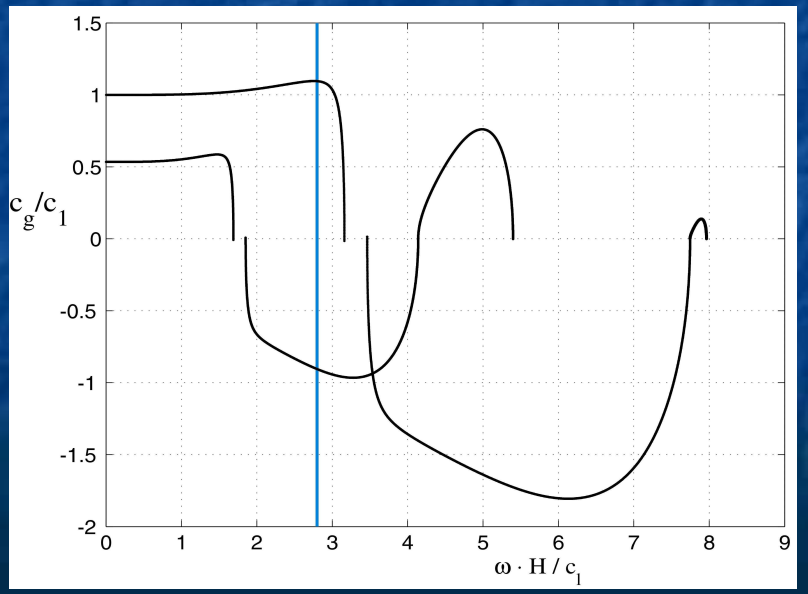

cg/c1
ω · H / c1

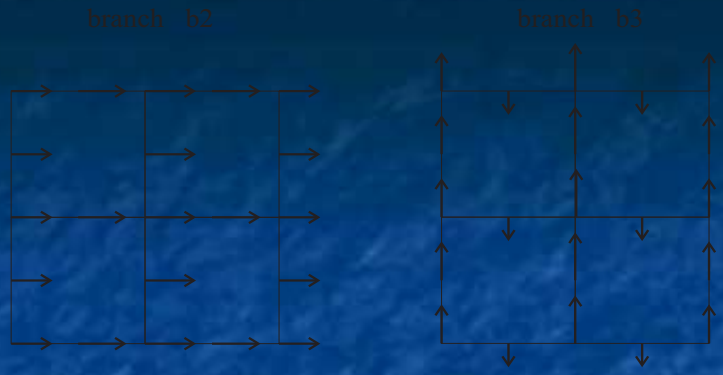

branch b2
branch b3

$$\omega H / c_1 = 2.8$$

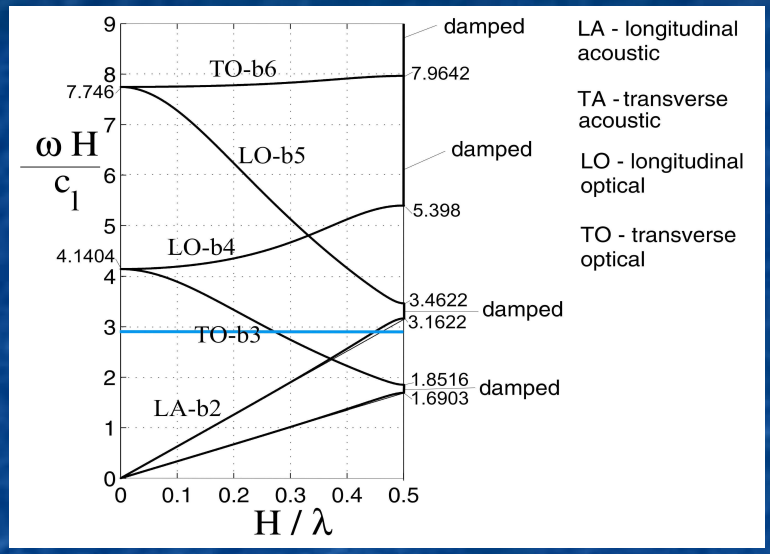

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

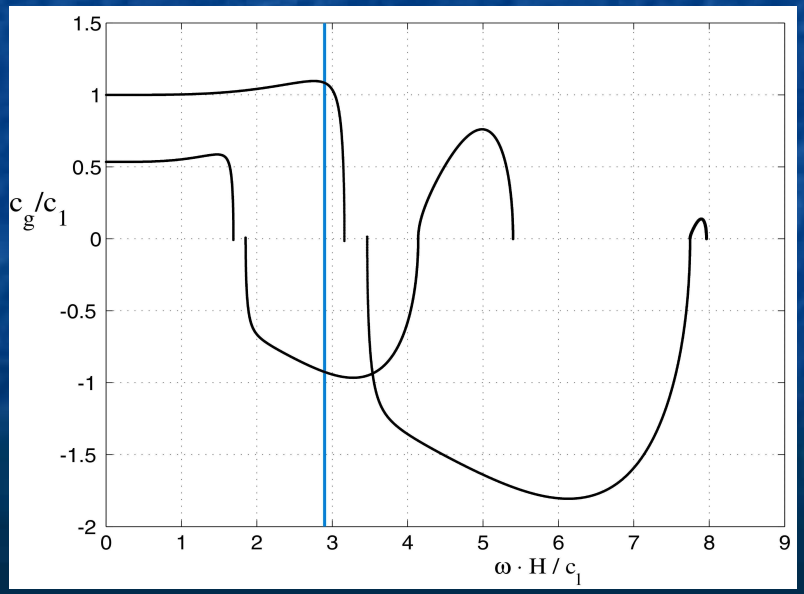


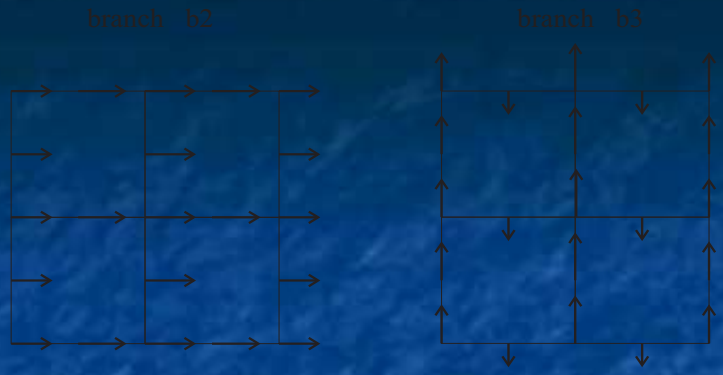

cg /c1
ω · H / c1


branch b2
branch b3

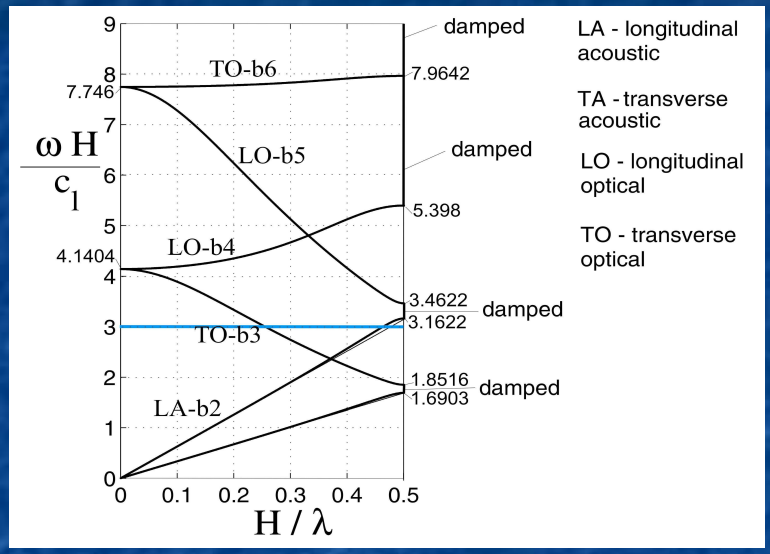
$$\omega H / c_1 = 2.9$$

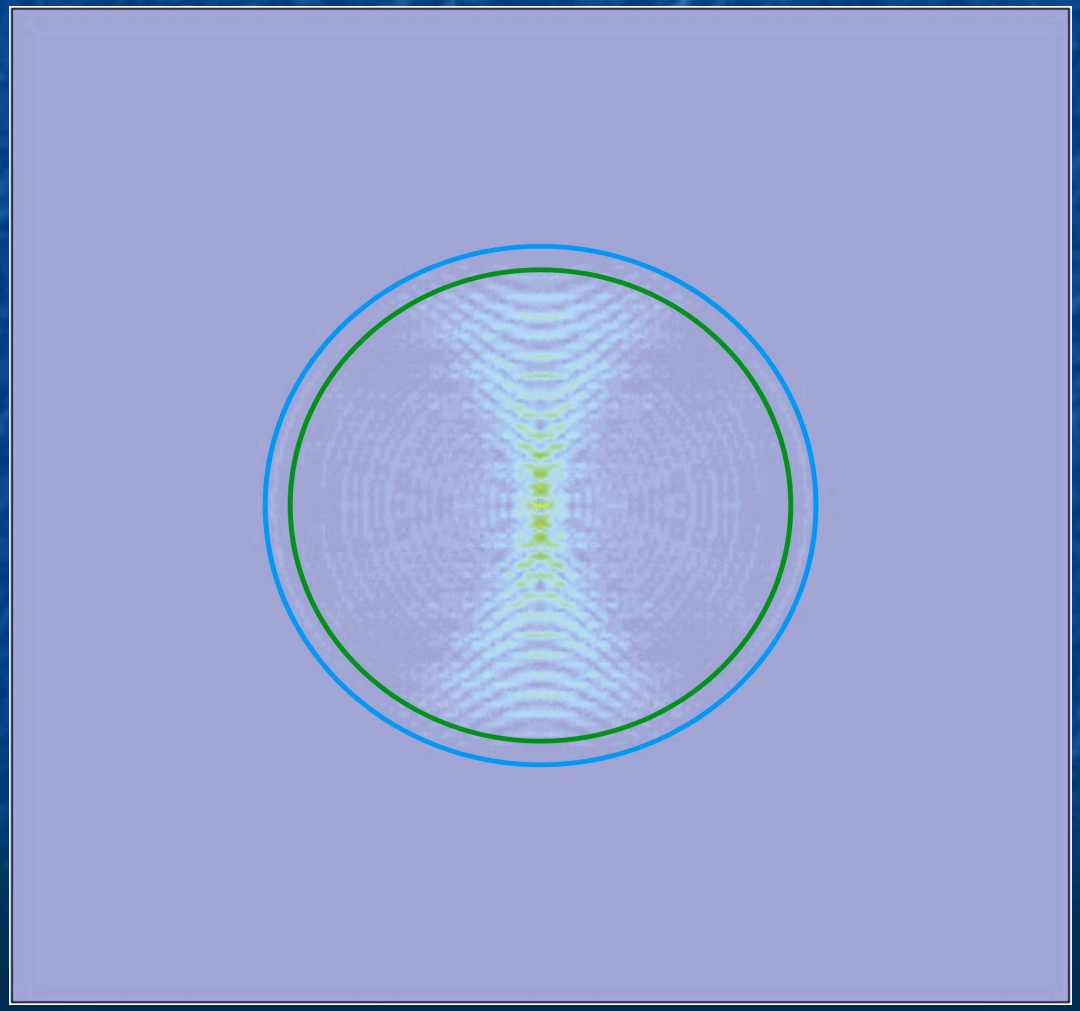

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

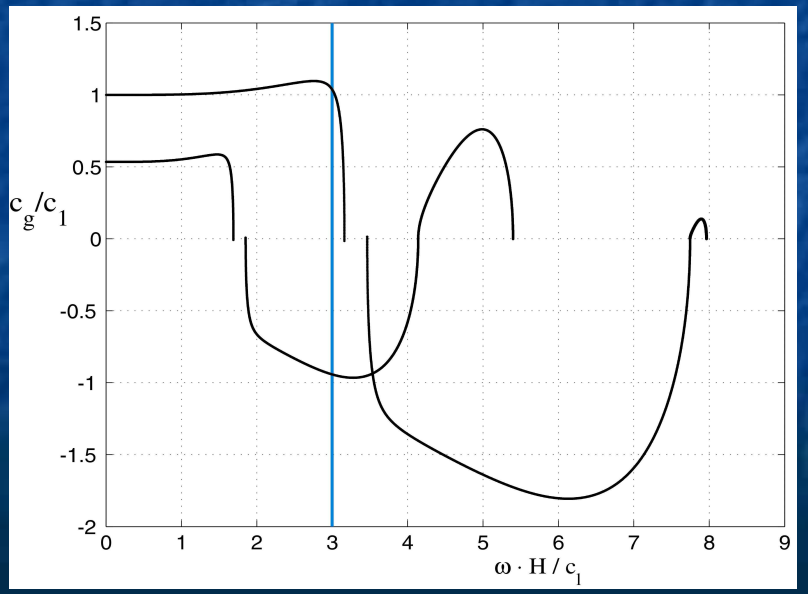

cg /c1
ω · H / c1

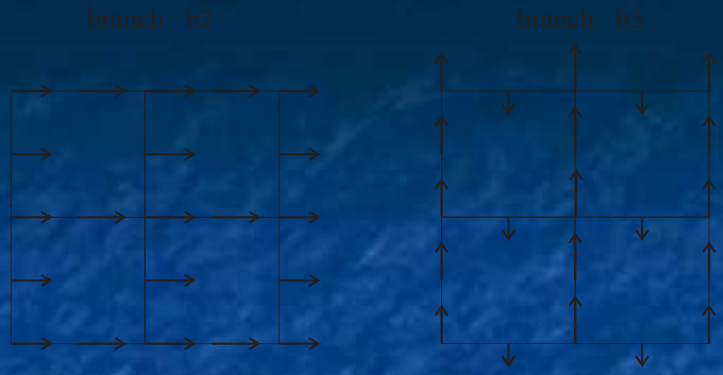

branch b2
branch b3

$$\omega H / c_1 = 3.0$$

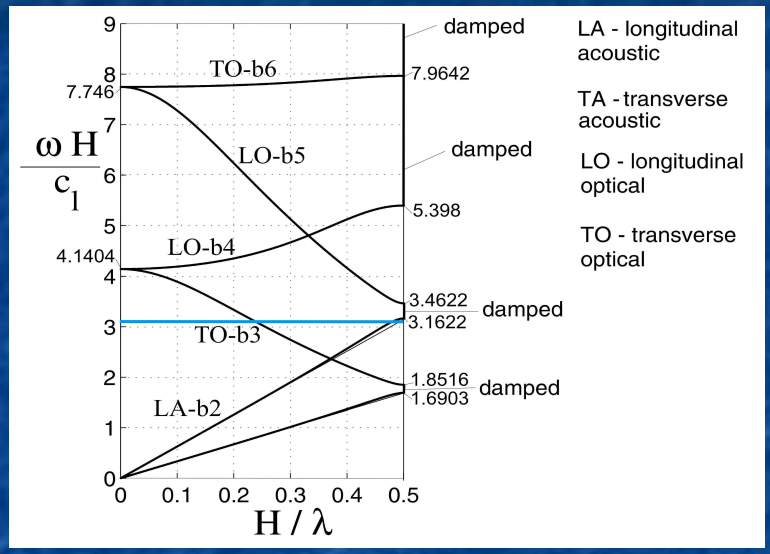

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

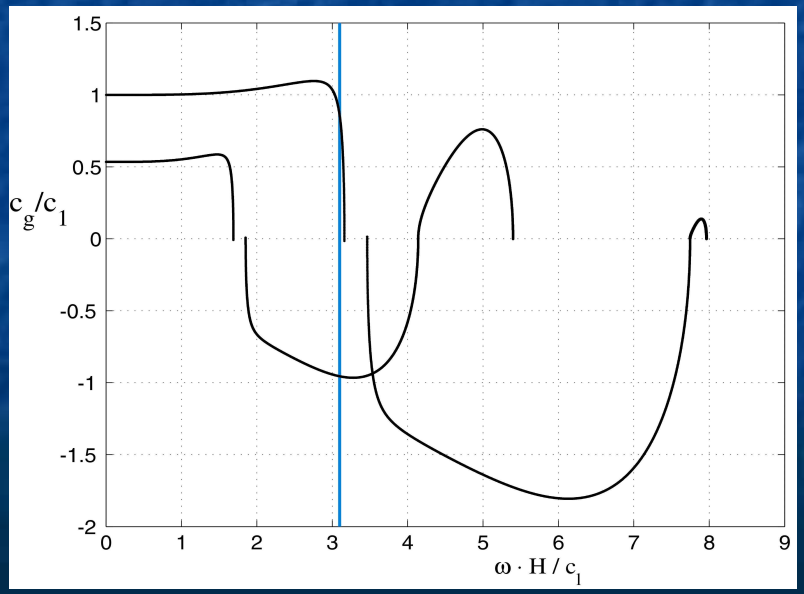


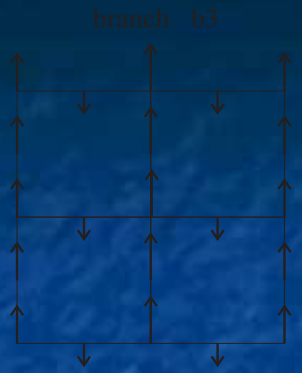

cg/c1
ω · H / c1


branch b2
branch b3

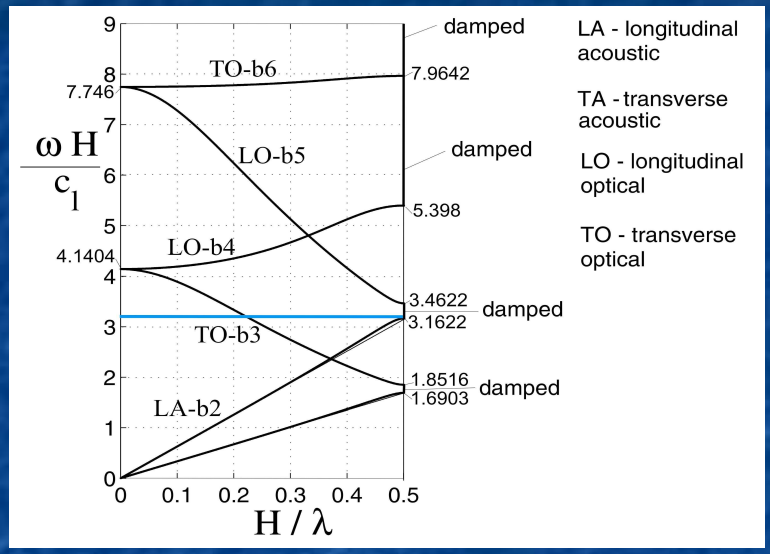
$$\omega H / c_1 = 3.1$$

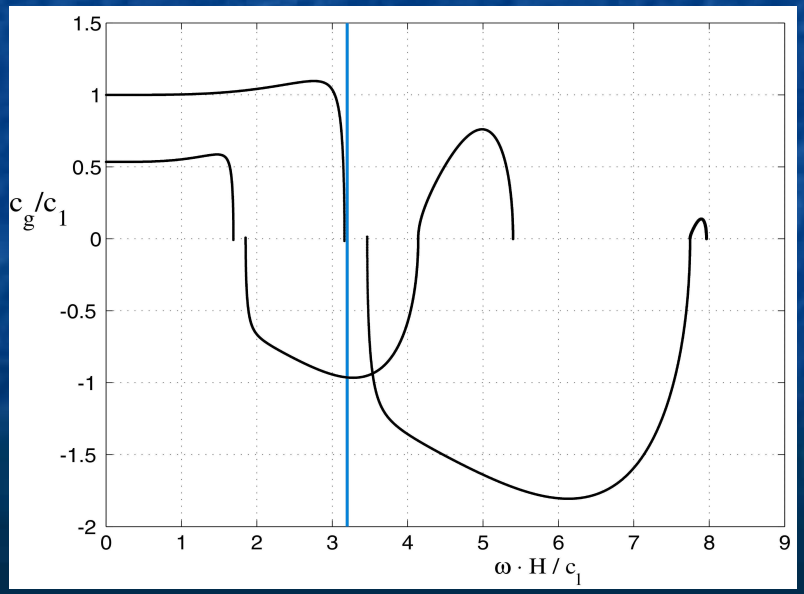

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

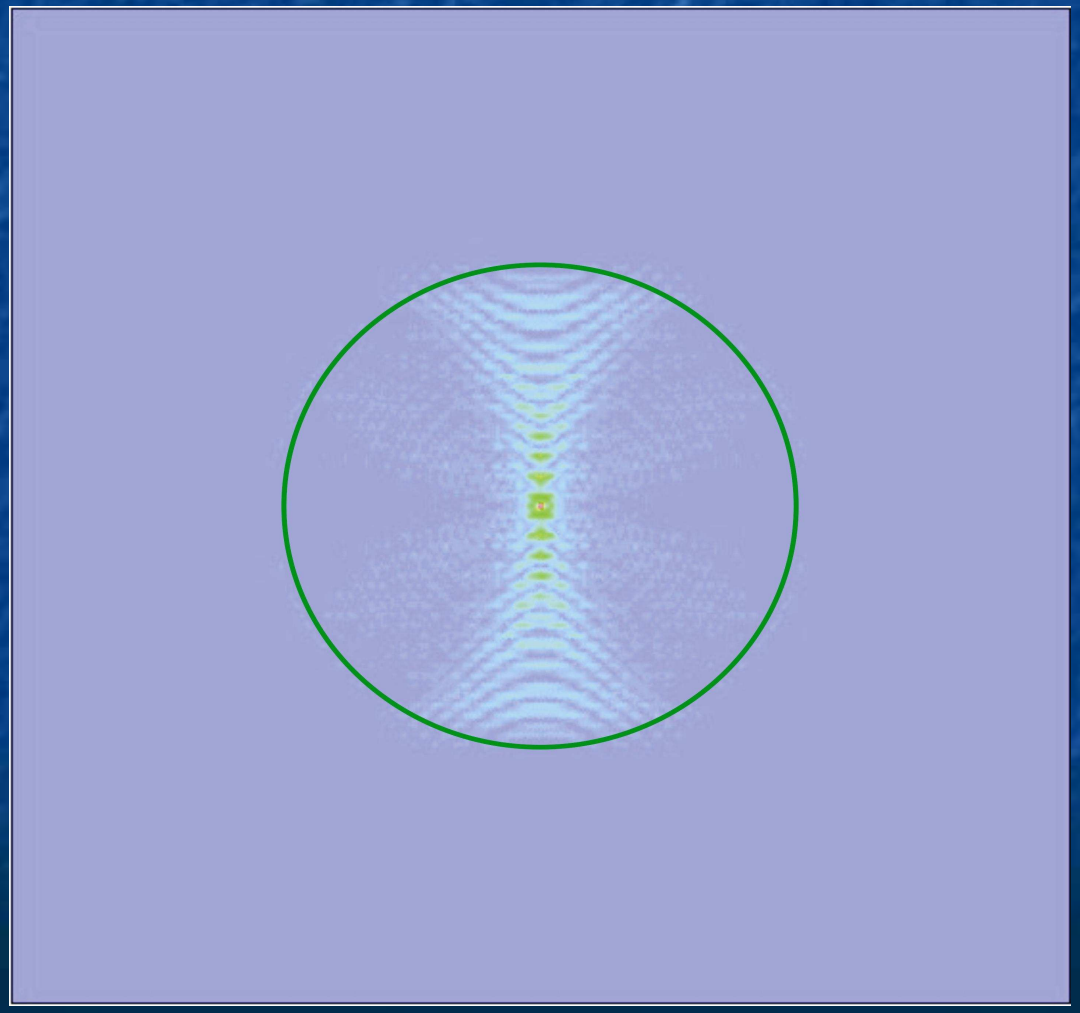

cg/c1
ω · H / c1


branch b3

$$\omega H / c_1 = 3.2$$

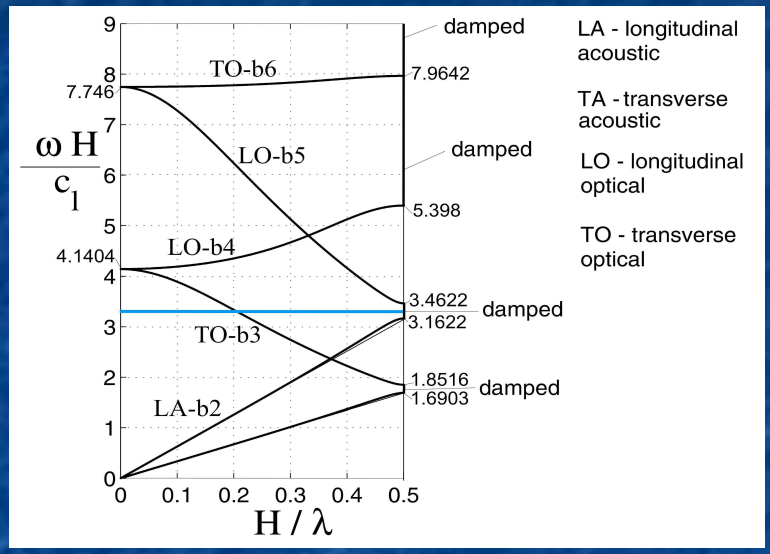

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

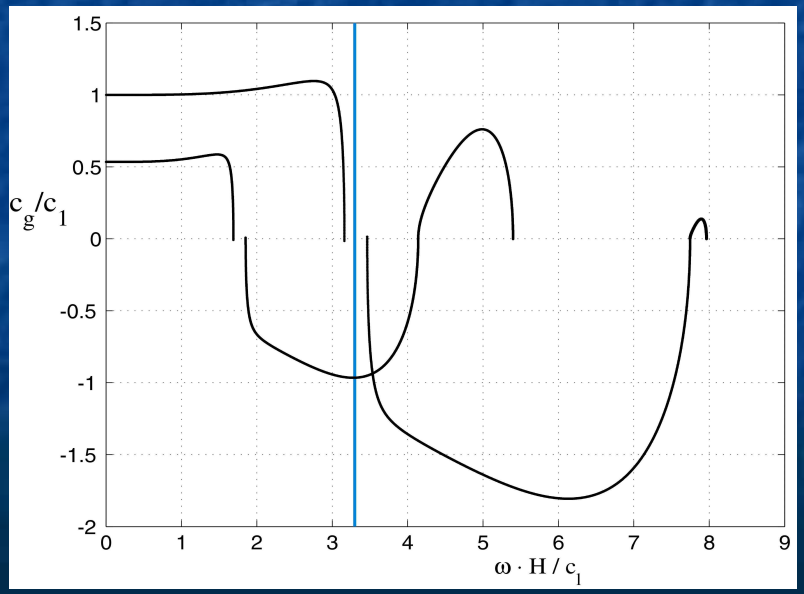

cg /c1
ω · H / c1



branch b3

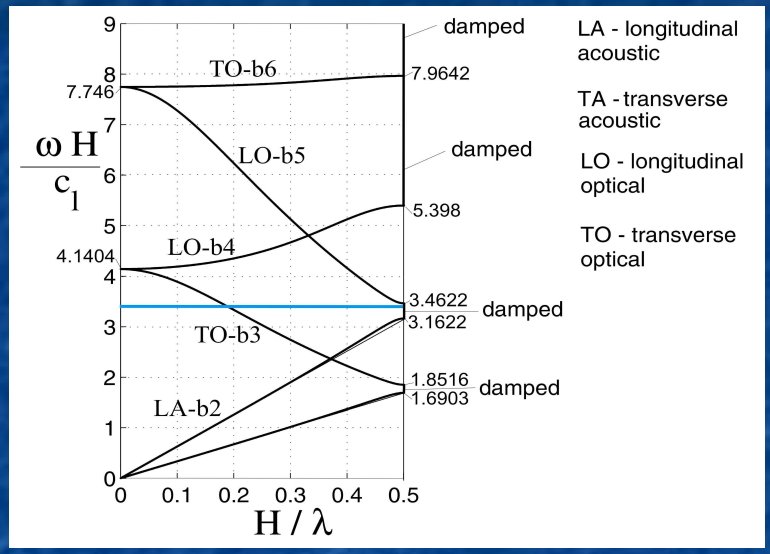
$$\omega H / c_1 = 3.3$$

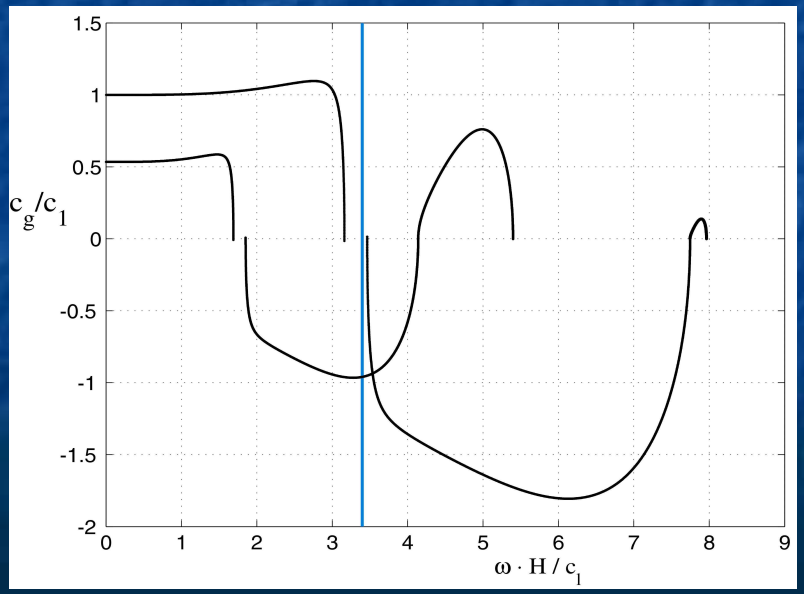

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

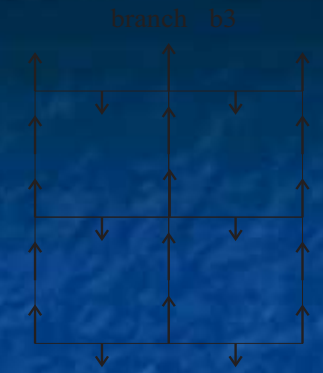

cg /c1
ω · H / c1

branch b3

$$\omega H / c_1 = 3.4$$

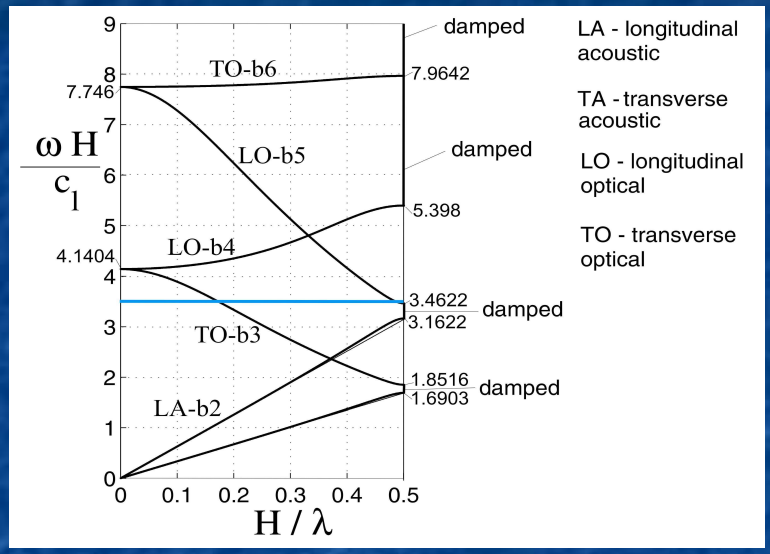

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

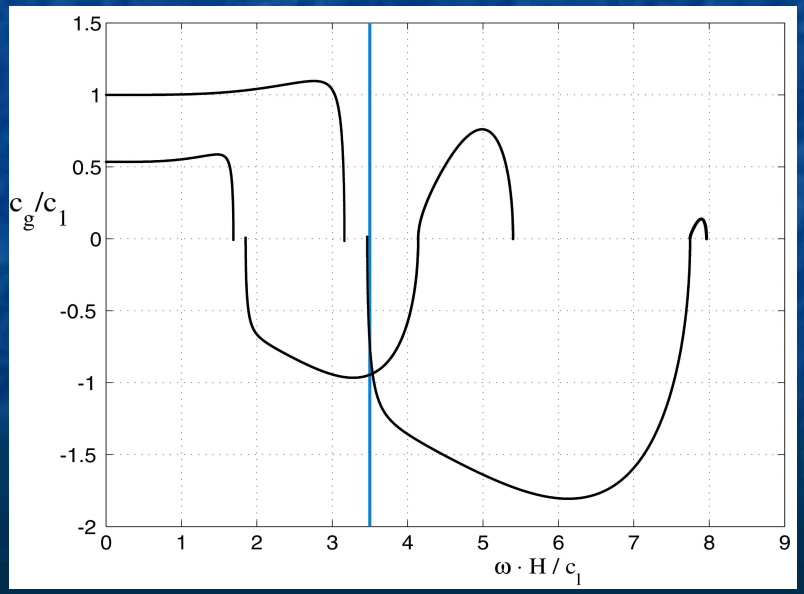

cg /c1
ω · H / c1

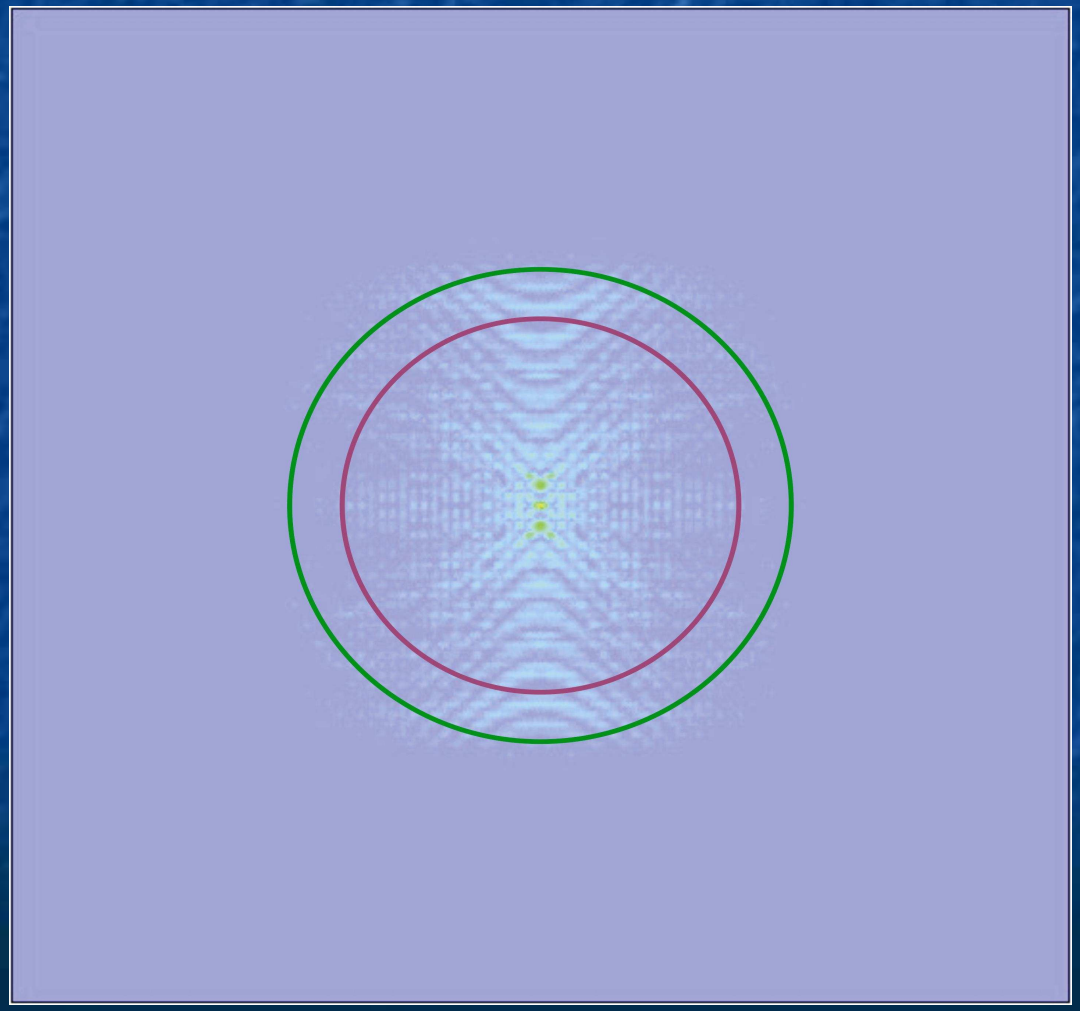

branch b3

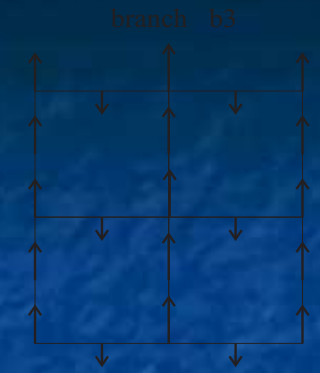
branch b5

$$\omega H / c_1 = 3.5$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

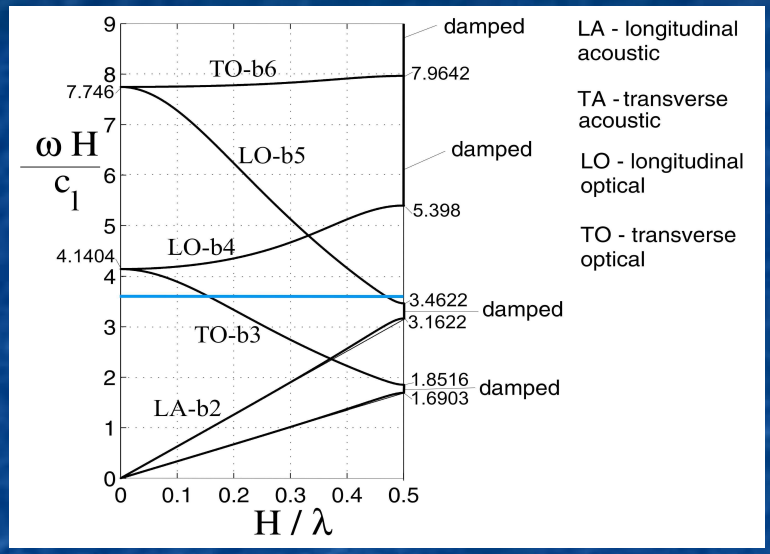

cg /c1
ω · H / c1

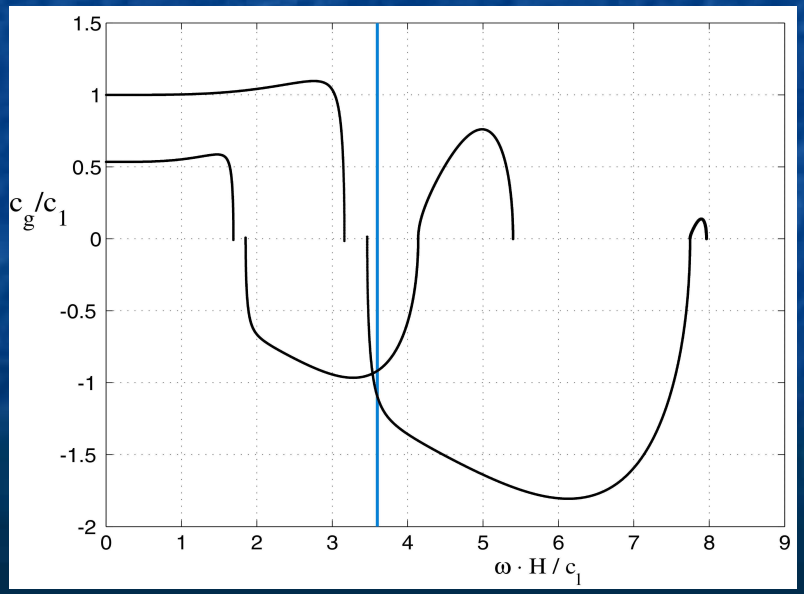



branch b3

branch b5

$$\omega H / c_1 = 3.6$$

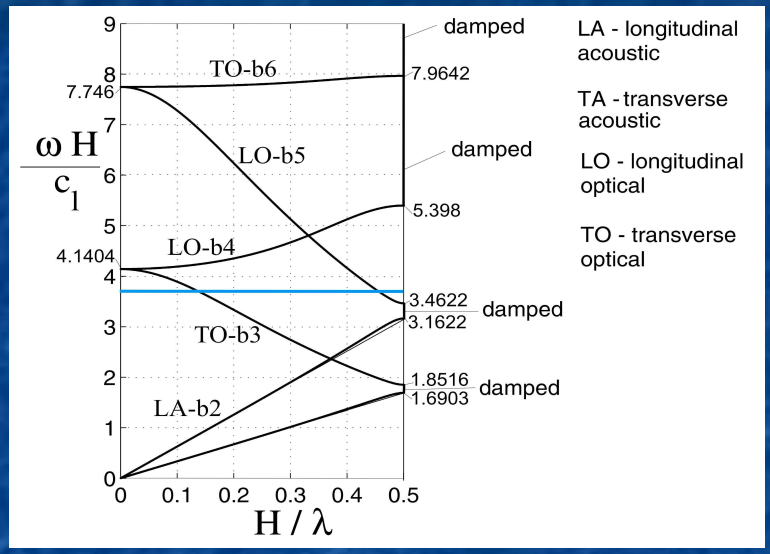

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

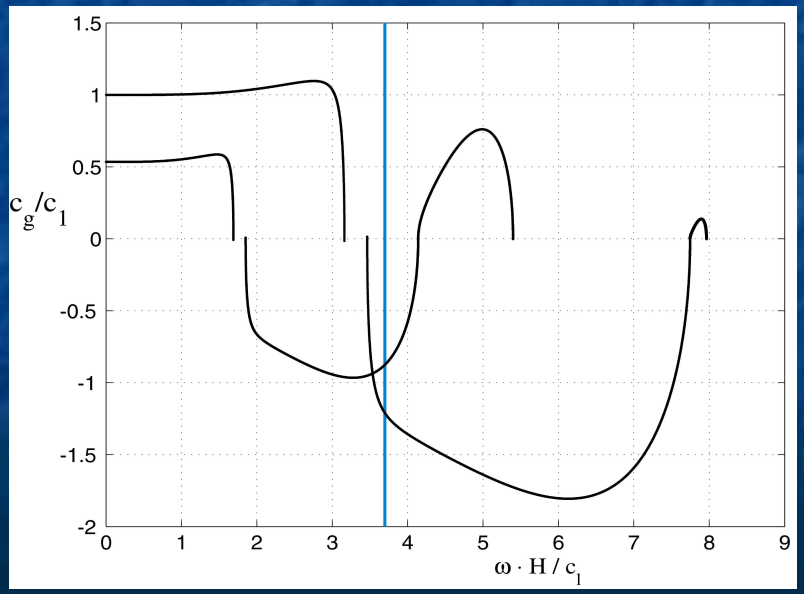

cg /c1
ω · H / c1

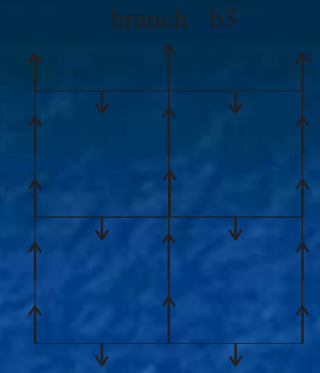
branch b3

branch b5

$$\omega H / c_1 = 3.7$$

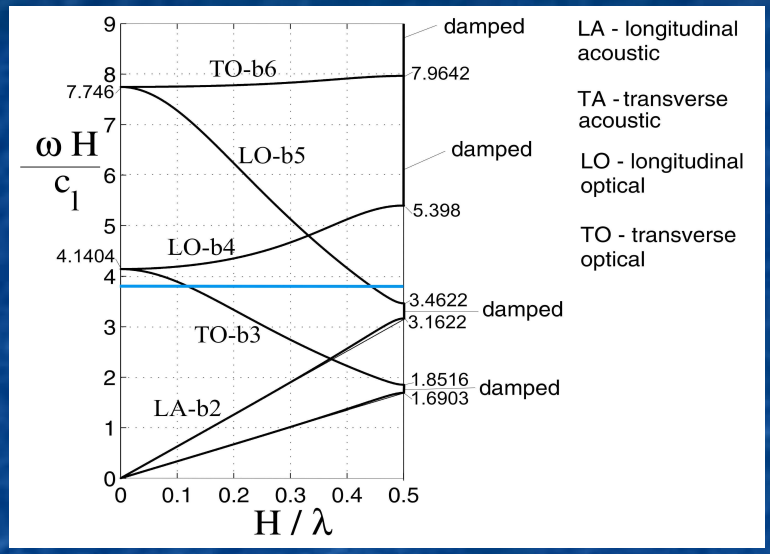

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

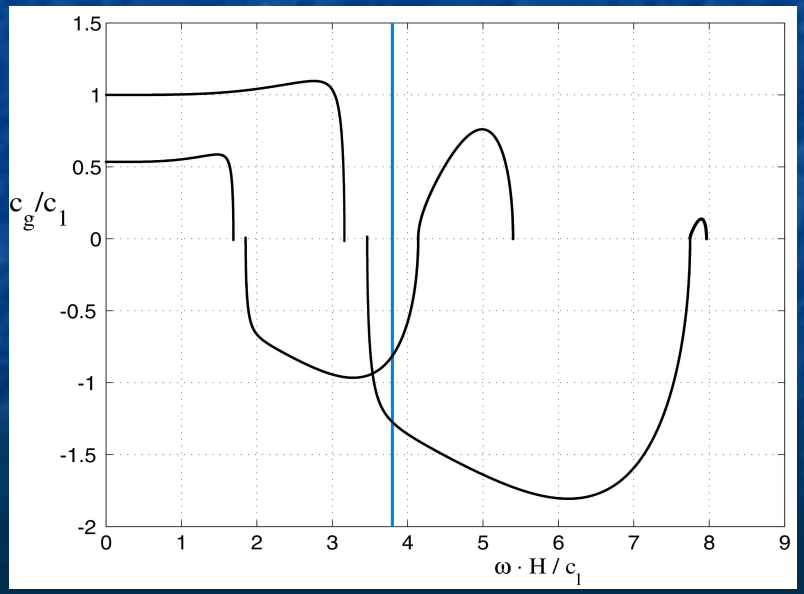

cg /c1
ω · H / c1

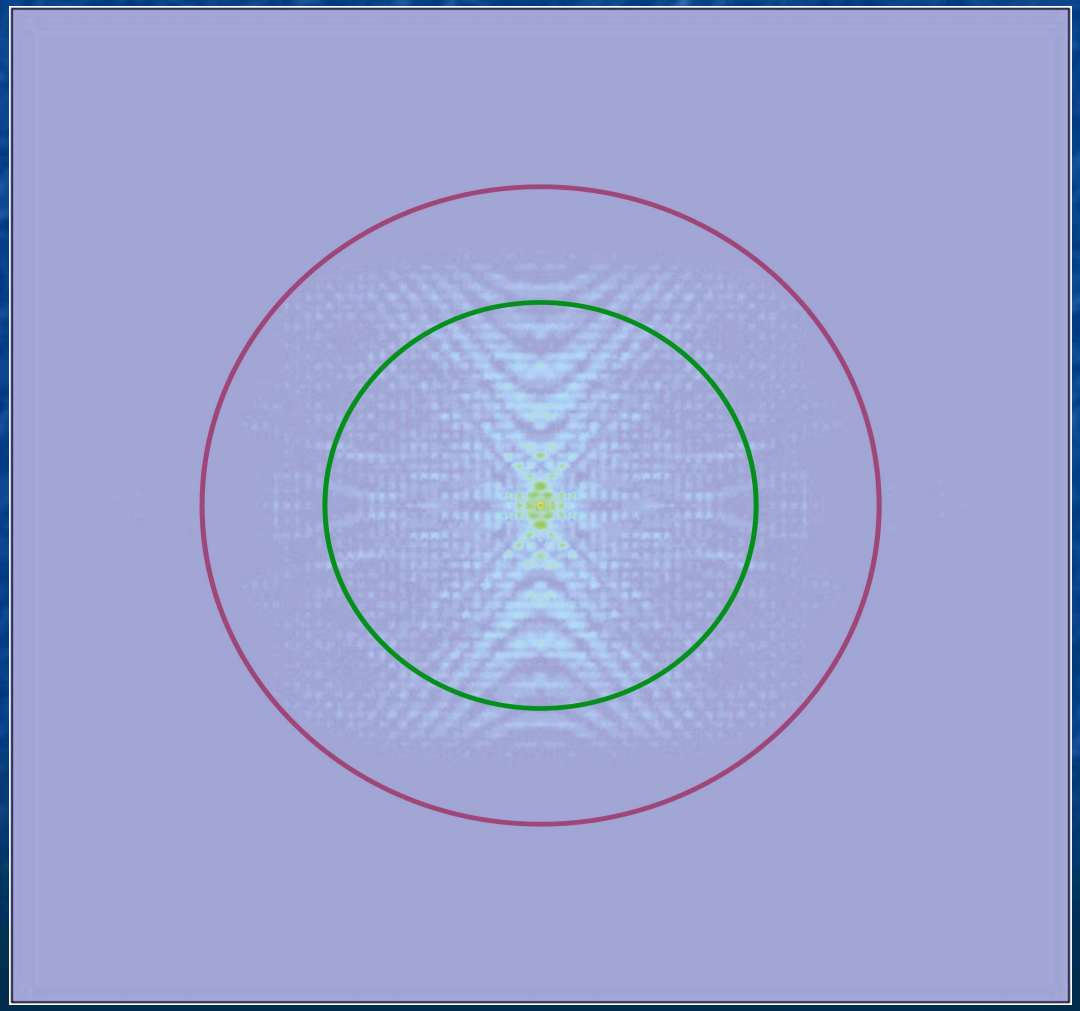

branch b3

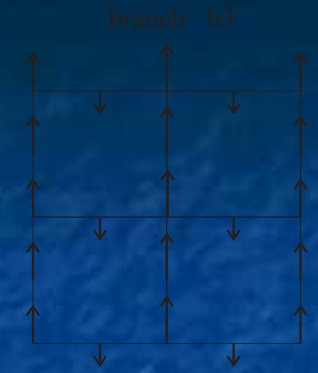
branch b5

$$\omega H / c_1 = 3.8$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

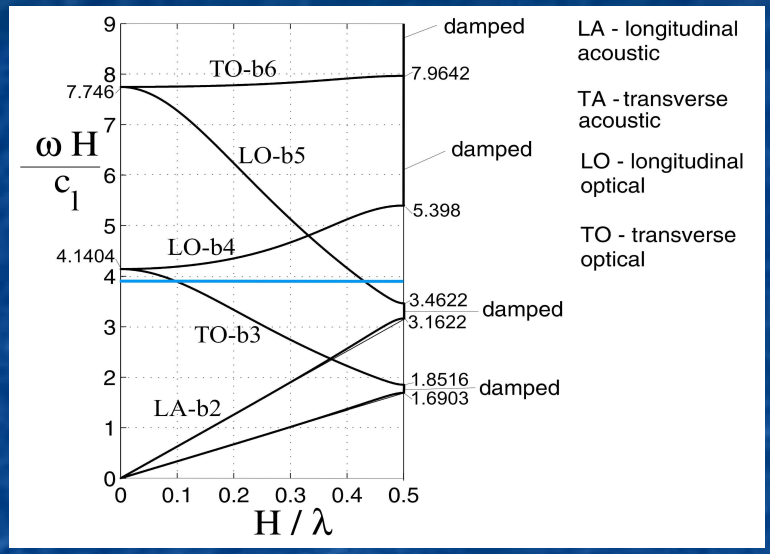

cg/c1
ω · H / c1

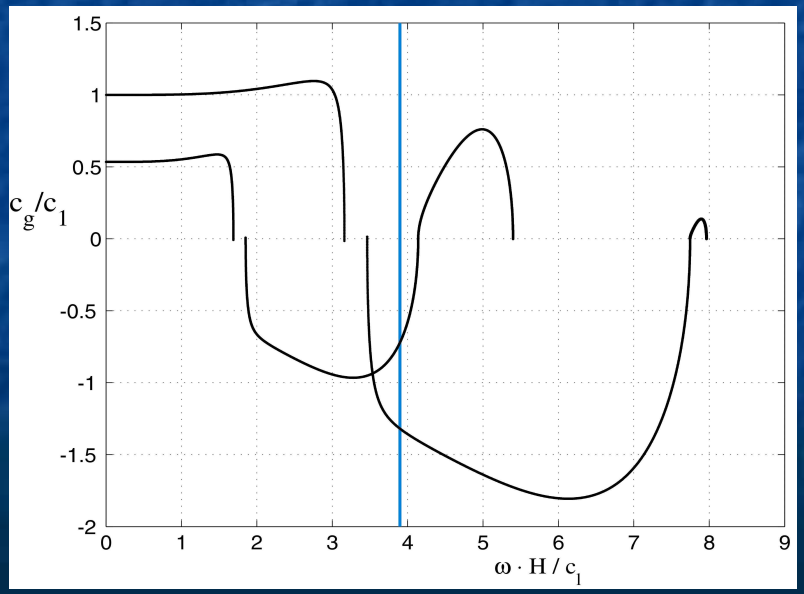


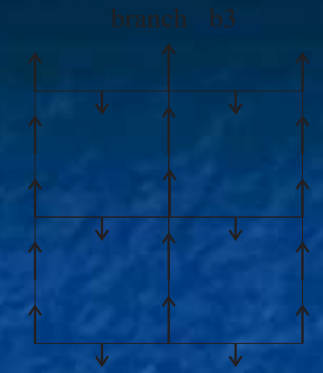

branch b3

branch b5

$$\omega H / c_1 = 3.9$$

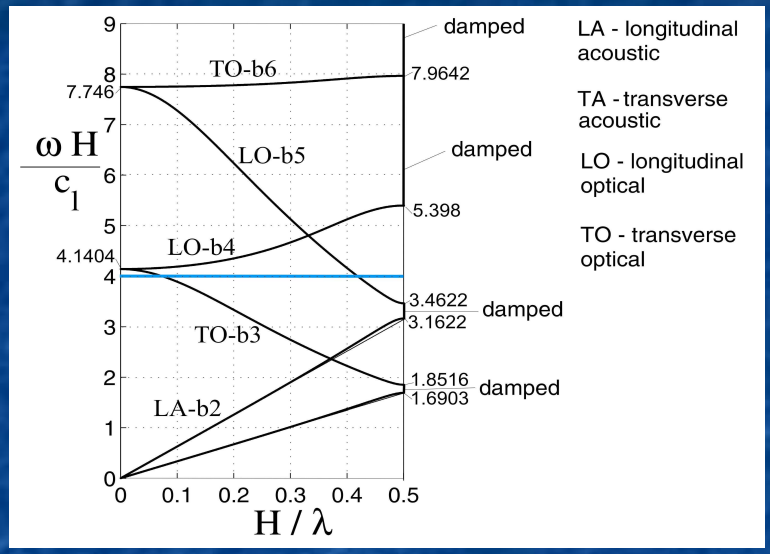

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

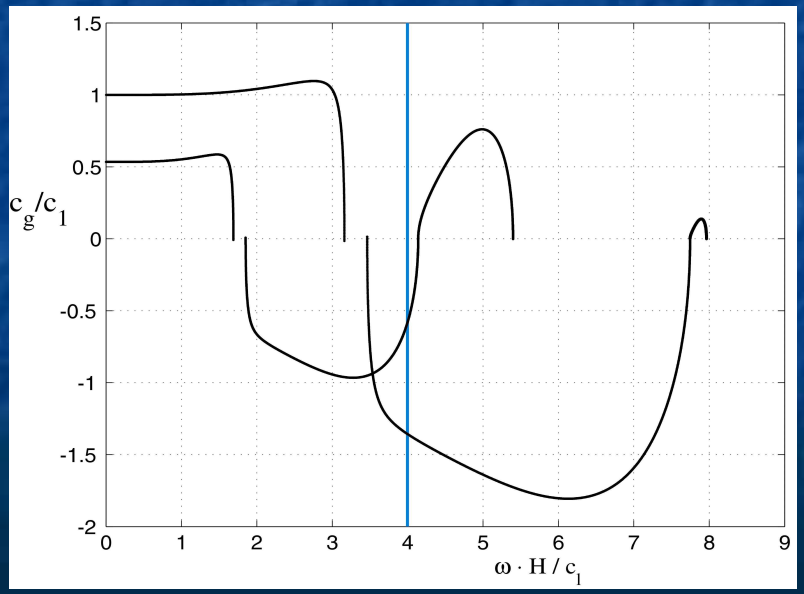

cg/c1
ω · H / c1


branch b3

branch b5

$$\omega H / c_1 = 4.0$$

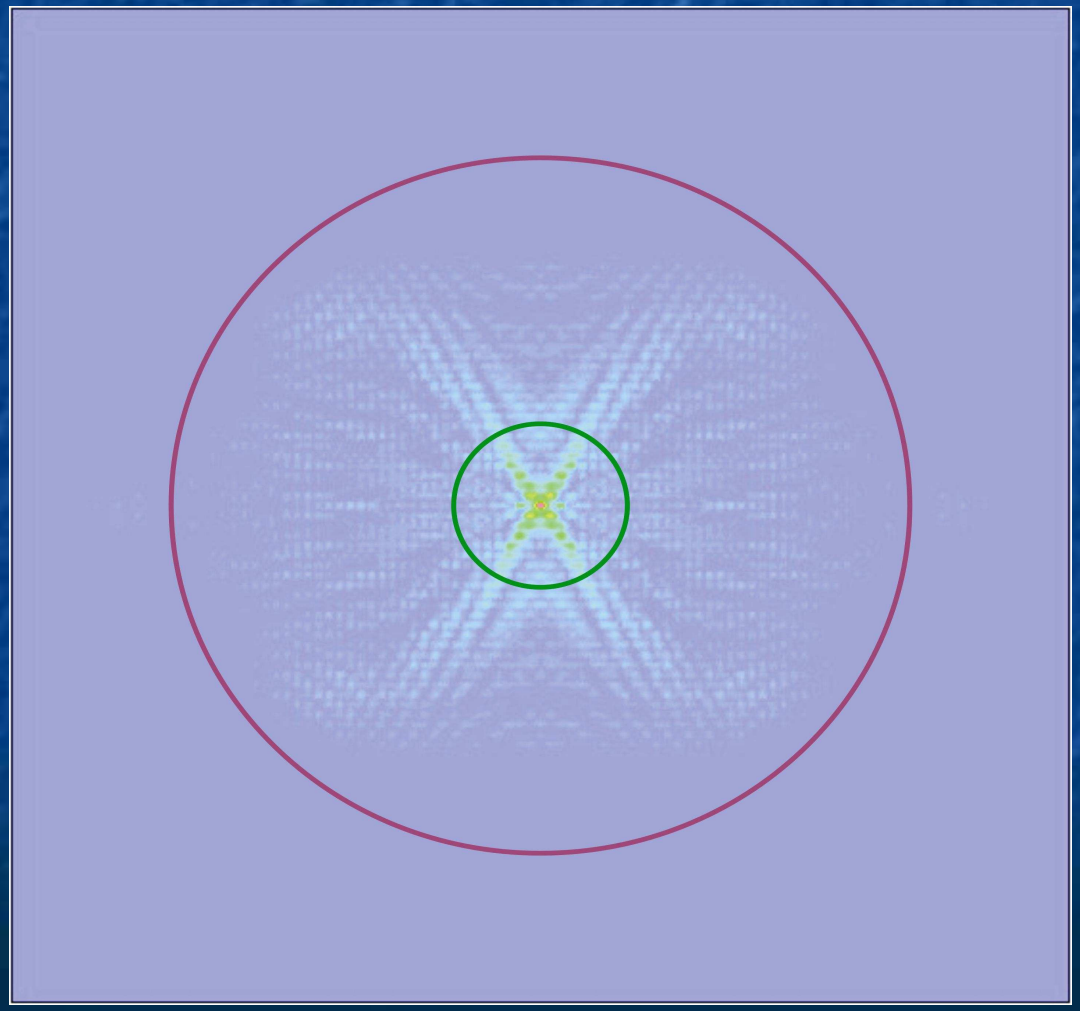

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

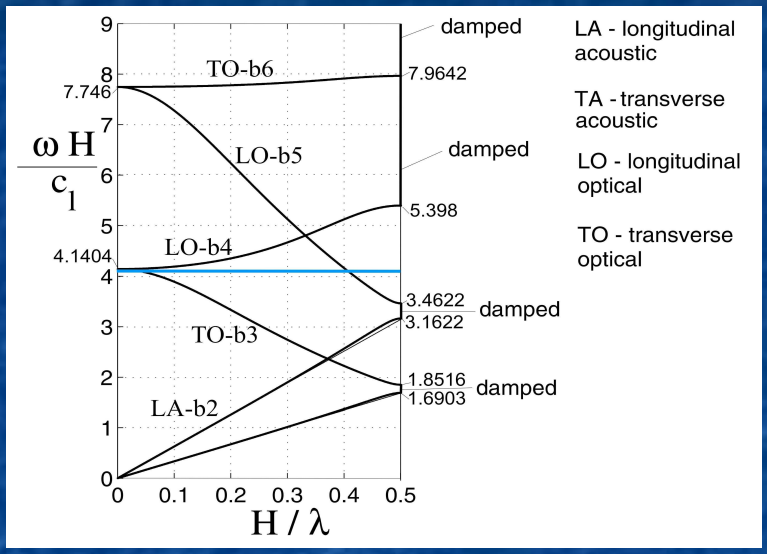

cg /c1
ω · H / c1

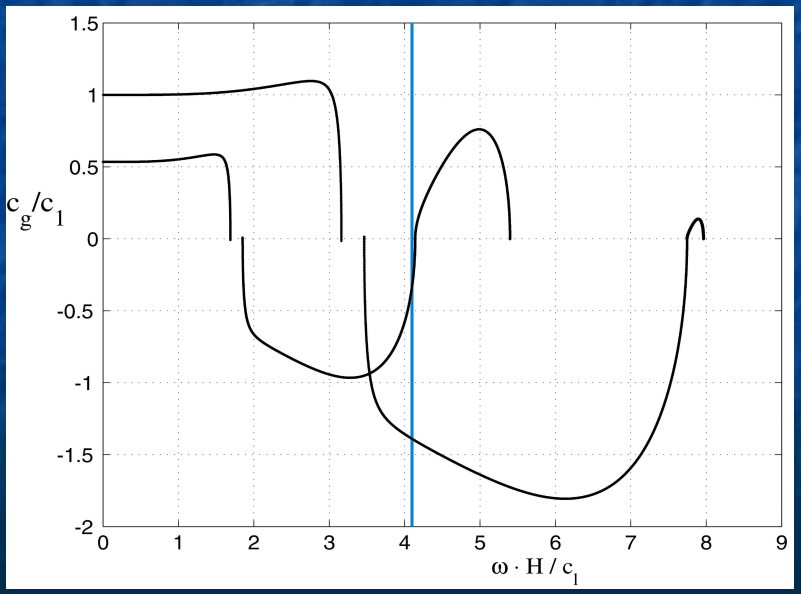
branch b3

branch b5

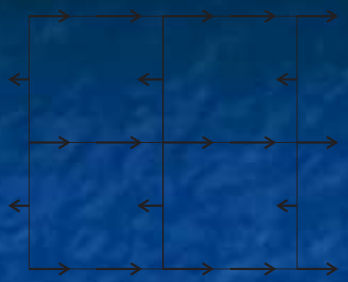
$$\omega H / c_1 = 4.1$$




damped
TO-b6
7.9642
7.746
damped
LO-b5
5.398
LO-b4
4.1404
3.4622
3.1622
damped
TO-b3
1.8516
1.6903
damped
LA-b2
ω H / c1
H / λ
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

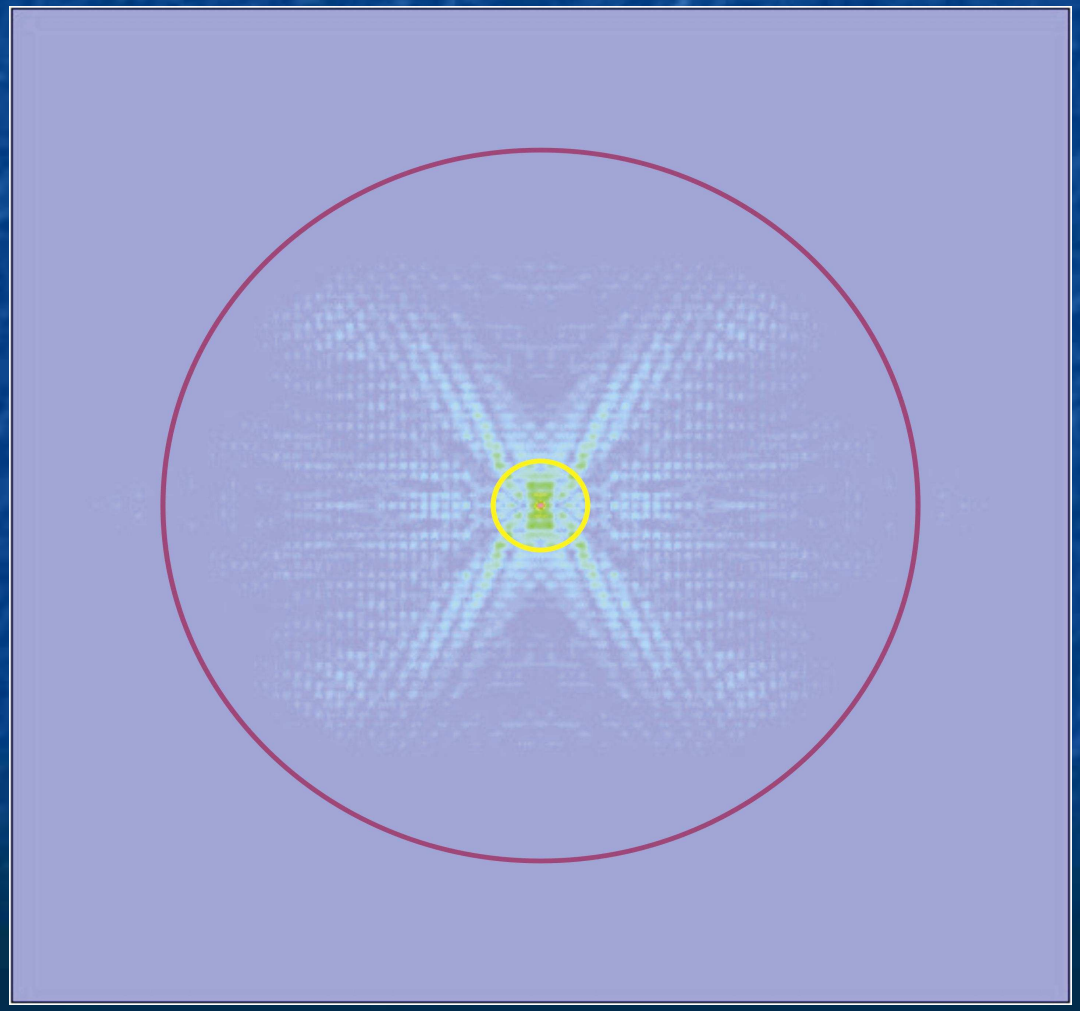

cg /c1
ω · H / c1

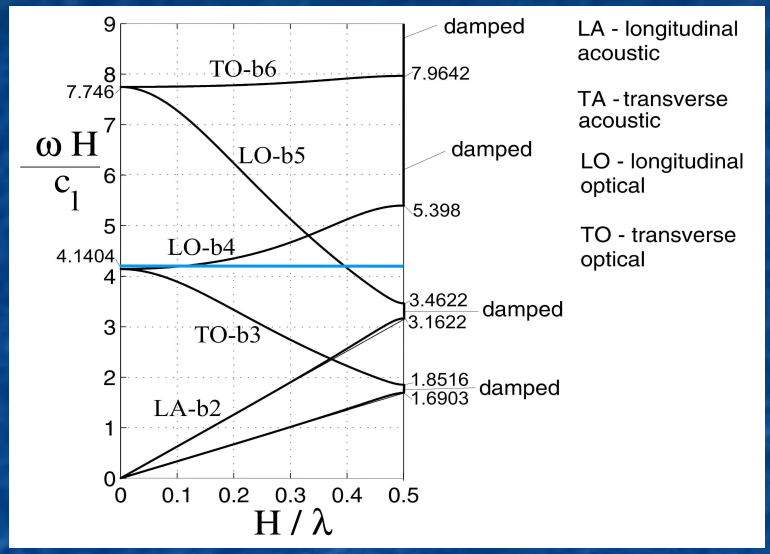
branch b4

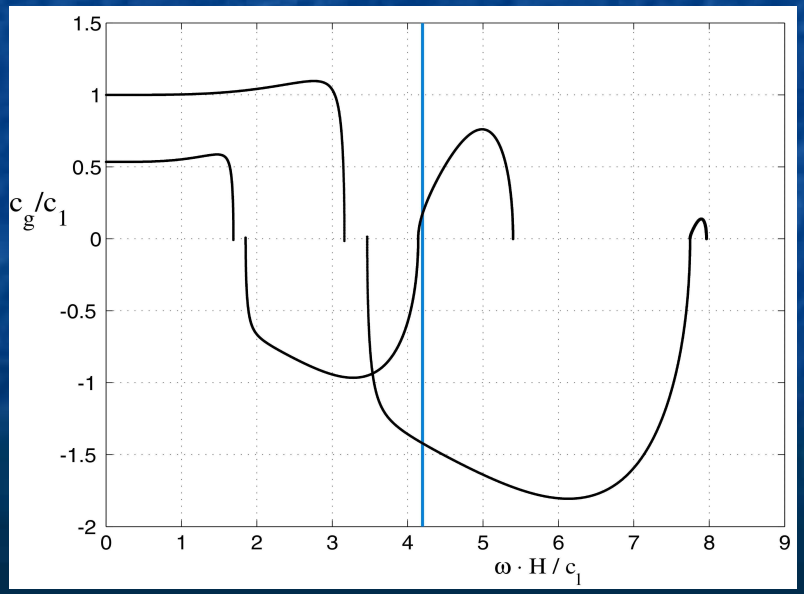


branch b5

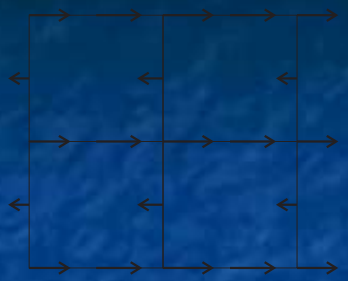
$$\omega H / c_1 = 4.2$$





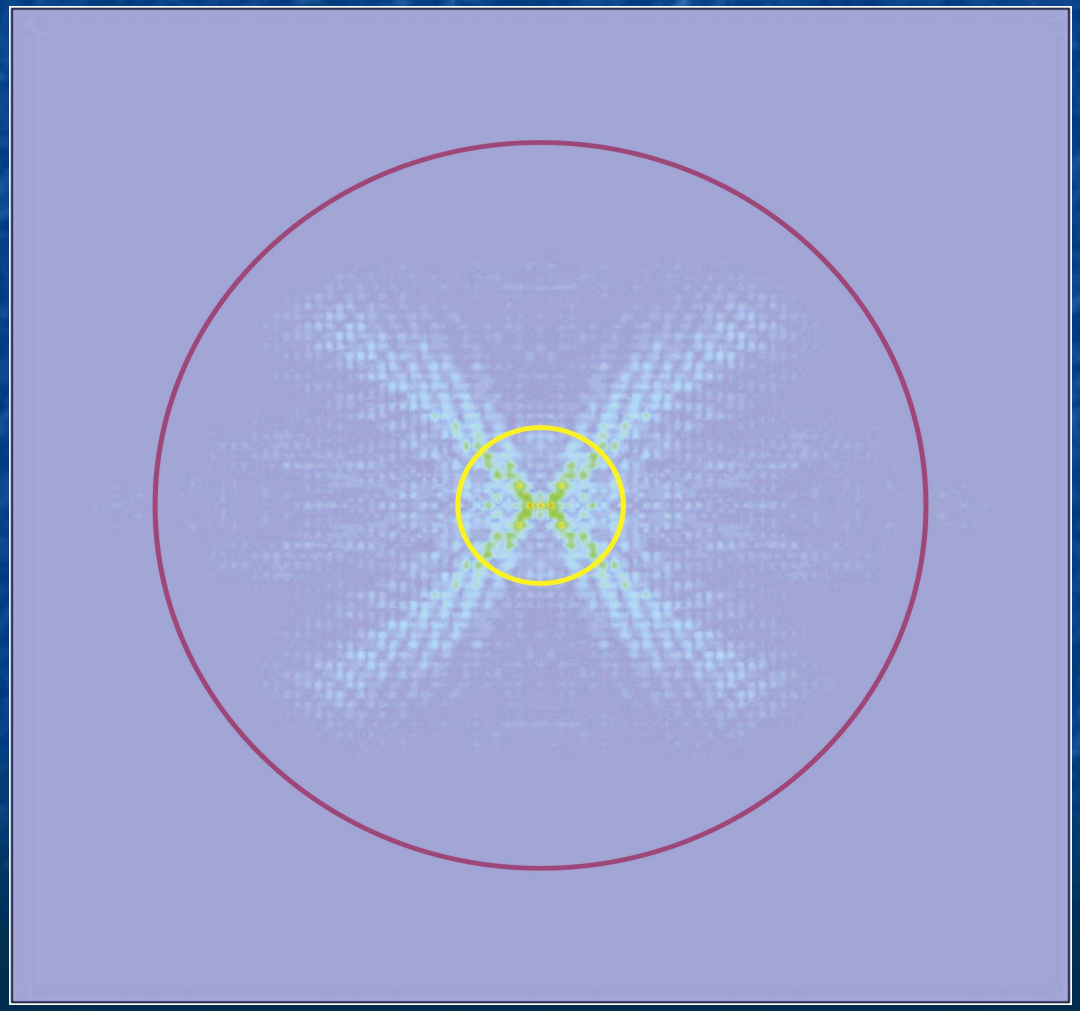


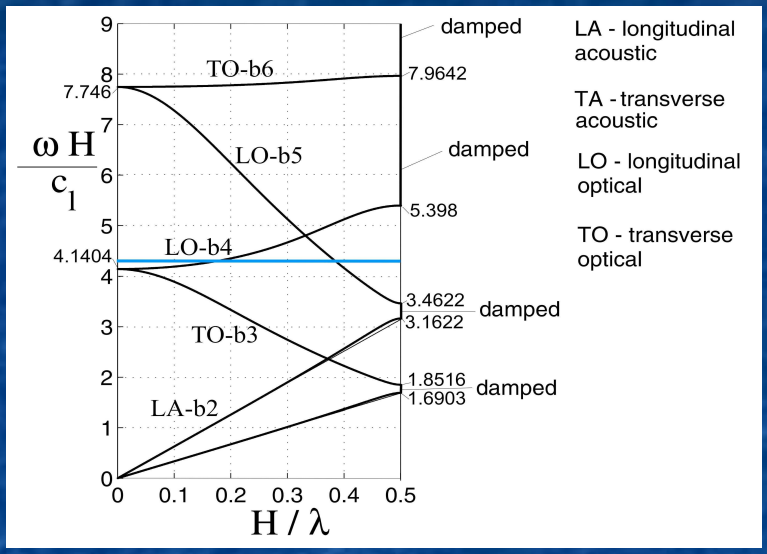
branch b4

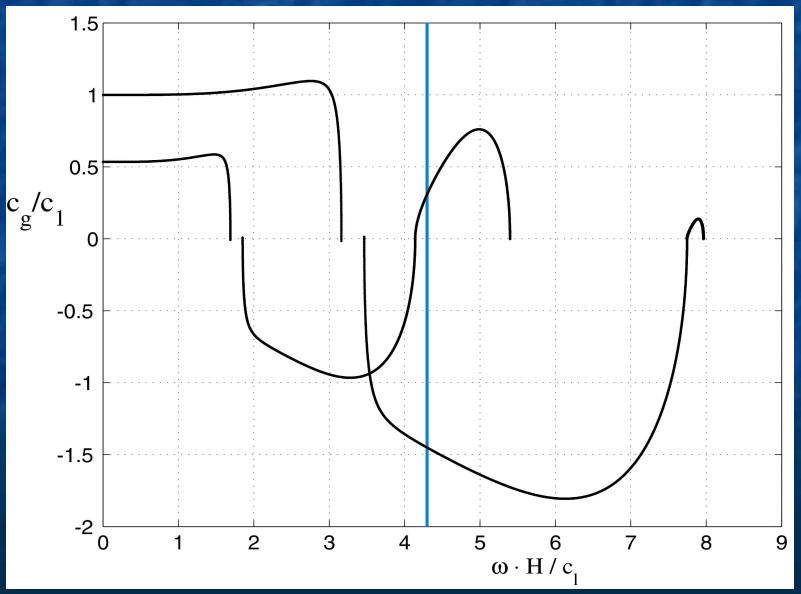


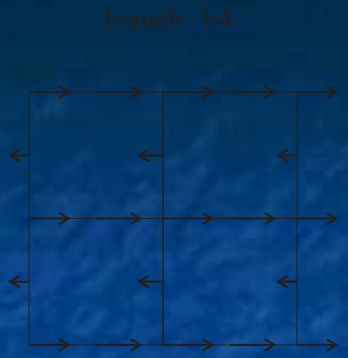
branch b5

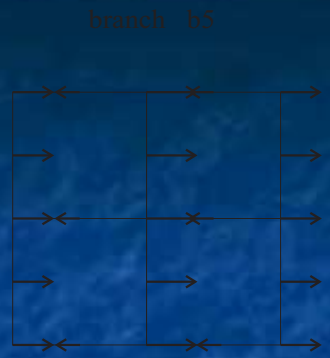
$$\omega H / c_1 = 4.3$$



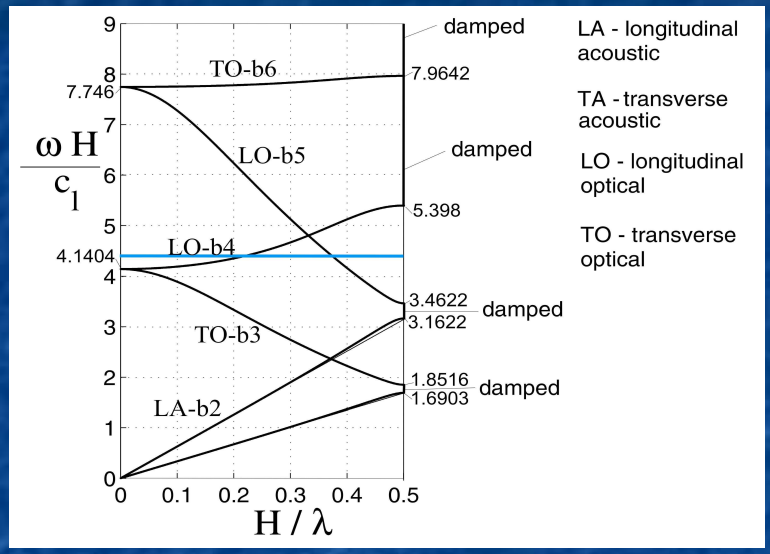


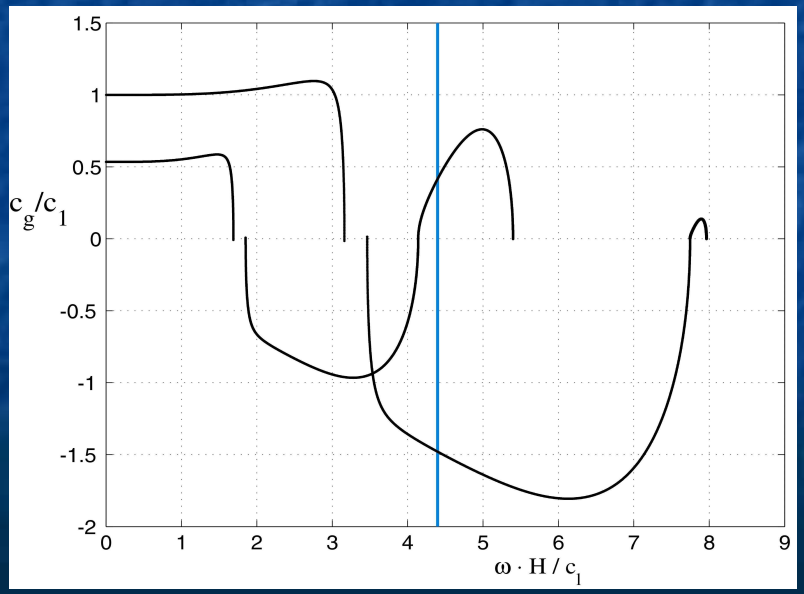



branch b4

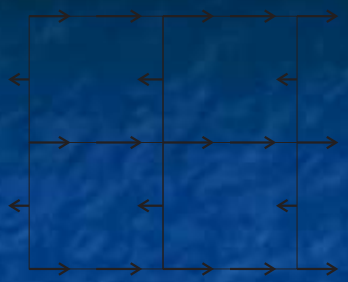

branch b5

$$\omega H / c_1 = 4.4$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

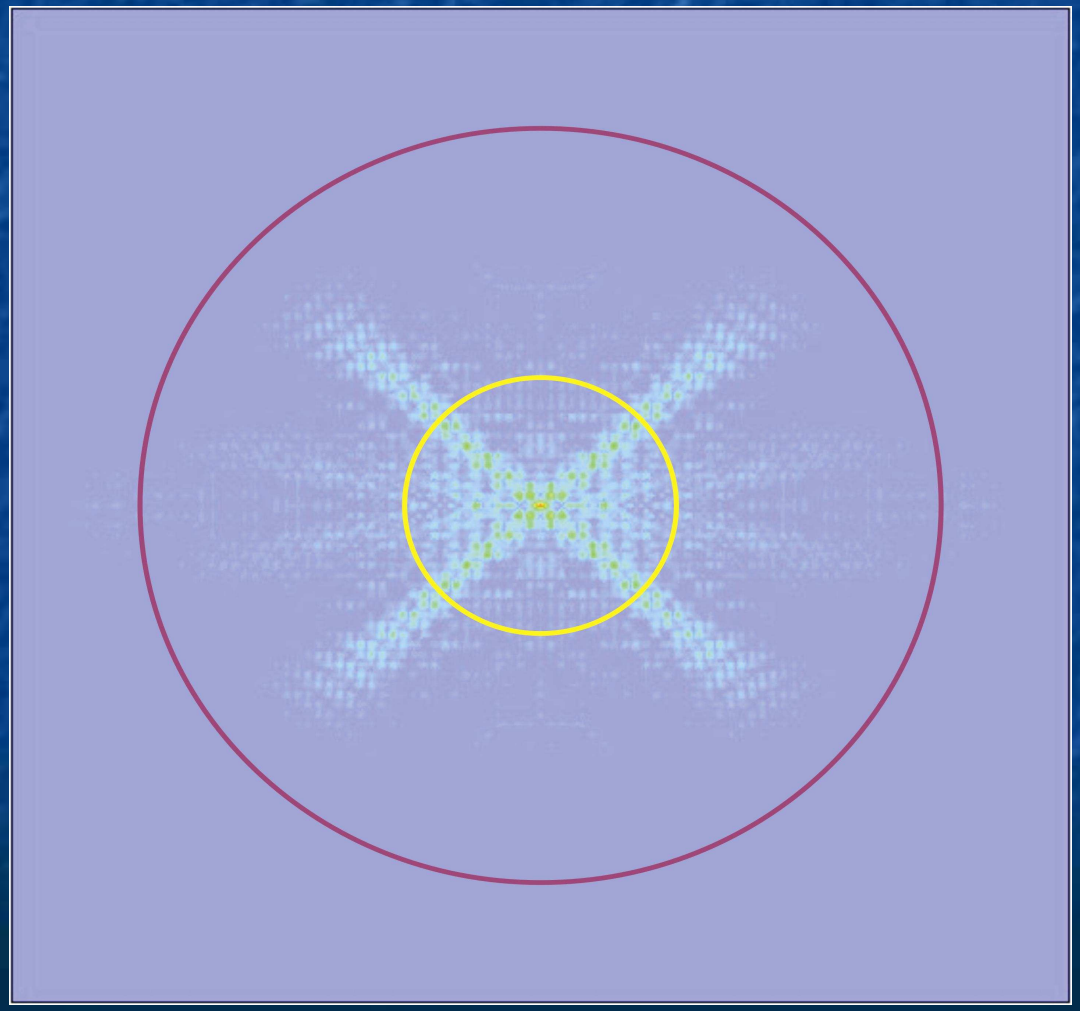

cg /c1
ω · H / c1

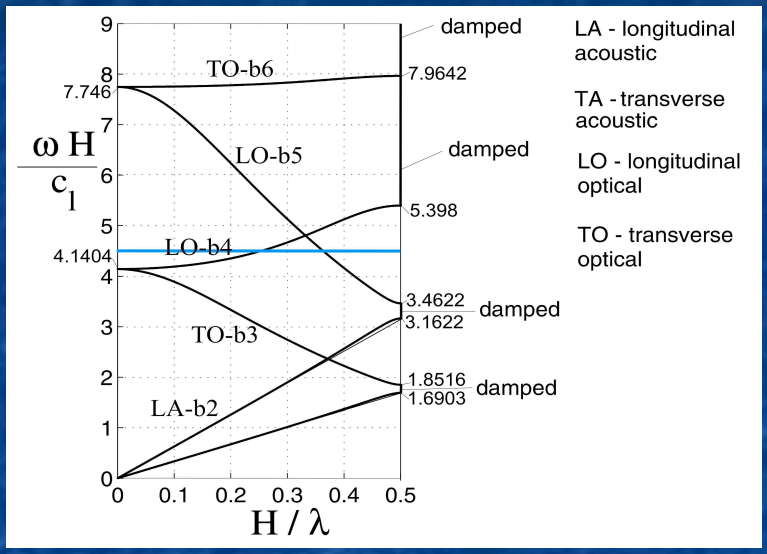
branch b4

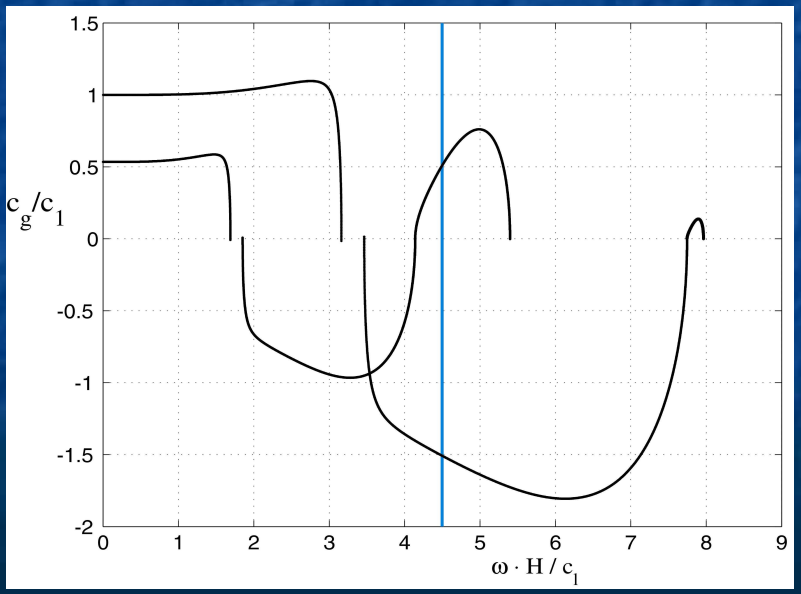


branch b5

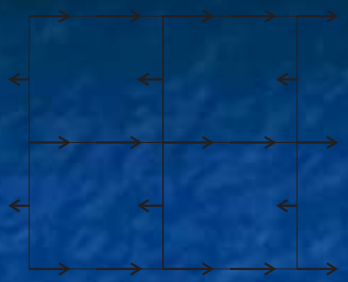
$$\omega H / c_1 = 4.5$$





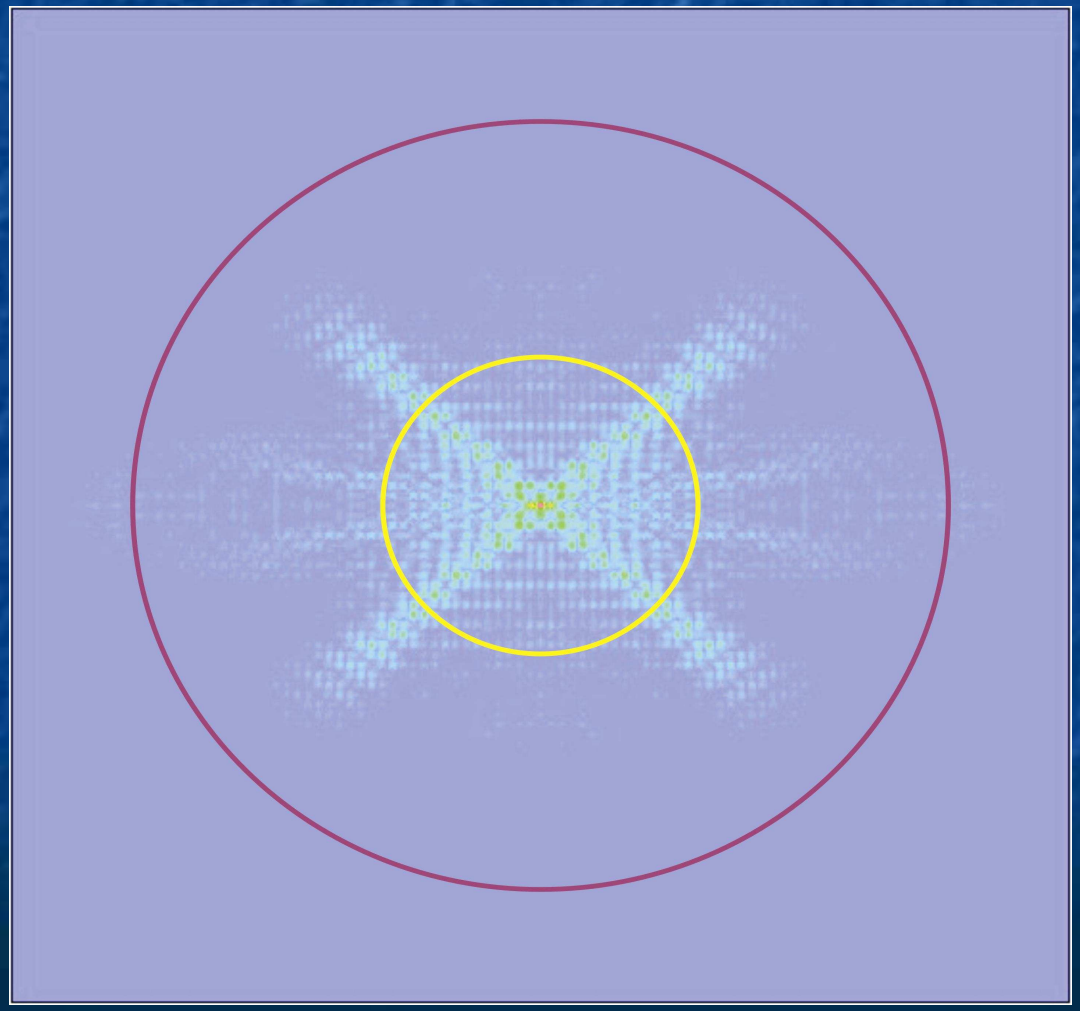


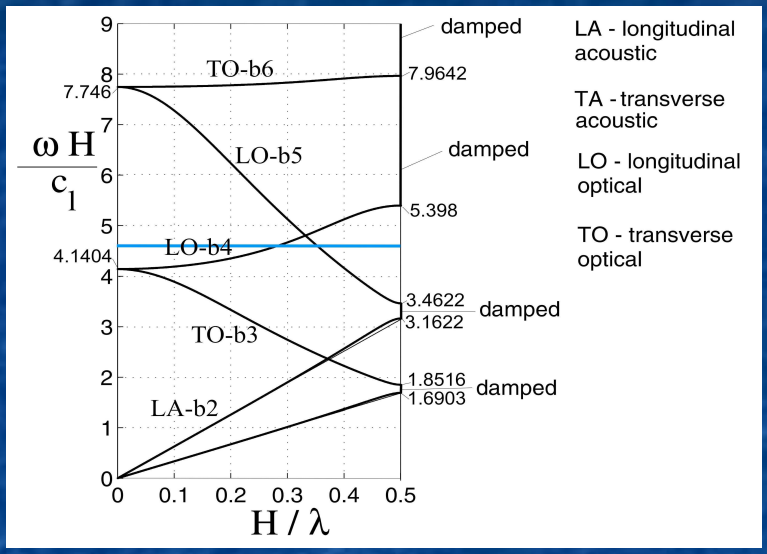
branch b4

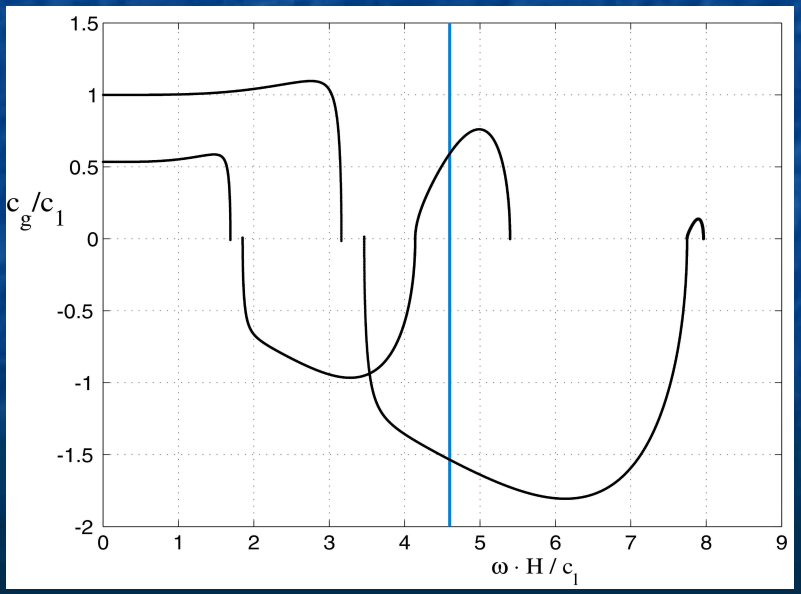


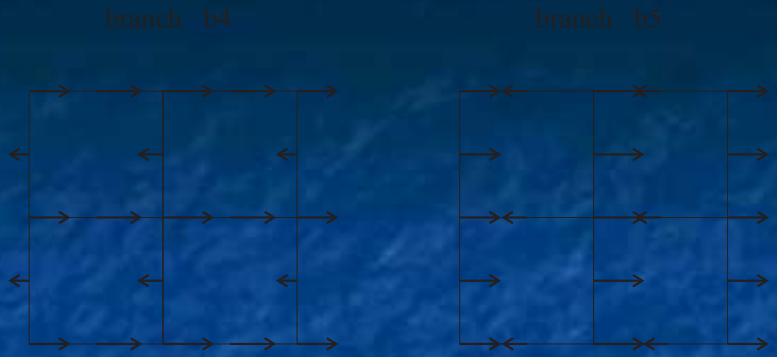
branch b5

$$\omega H / c_1 = 4.6$$

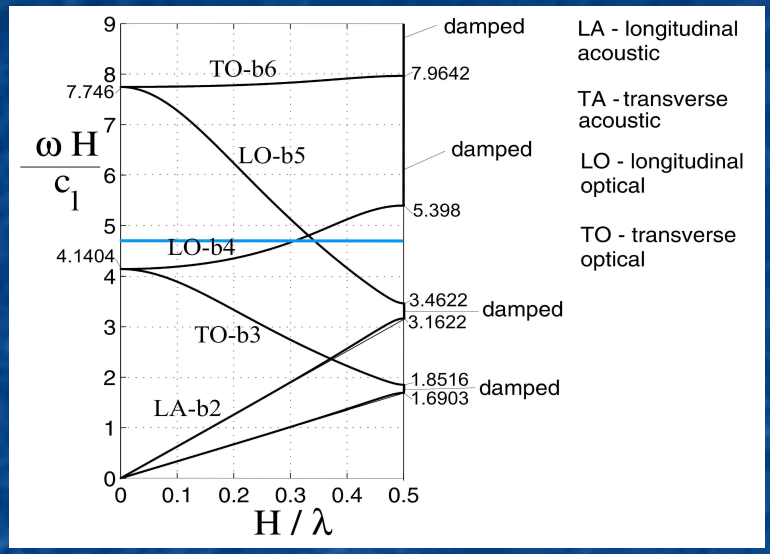


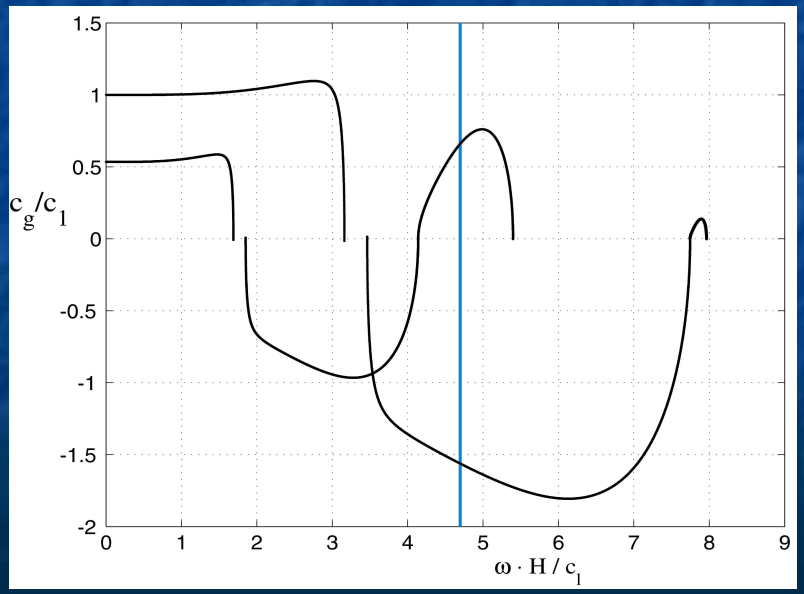


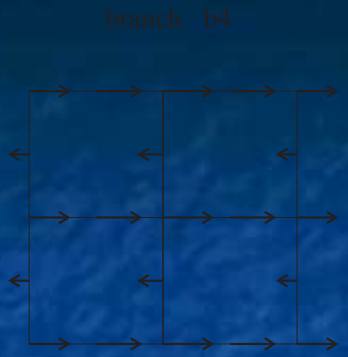



branch b4
branch b5

$$\omega H / c_1 = 4.7$$

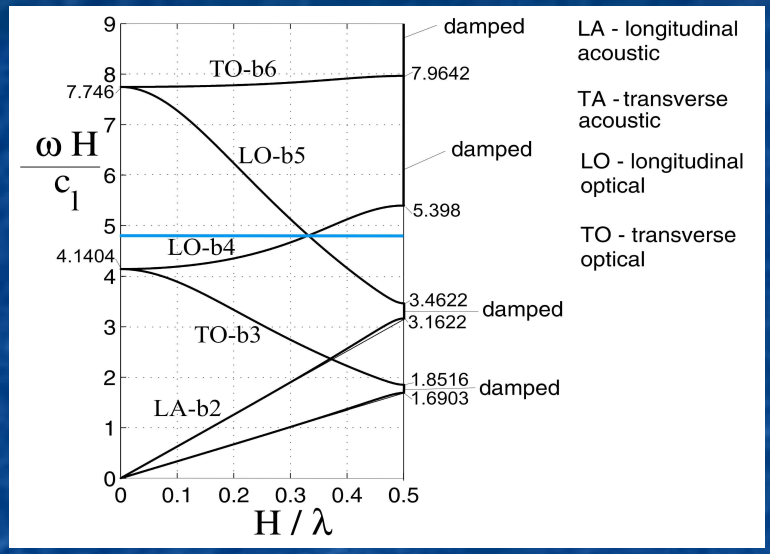

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

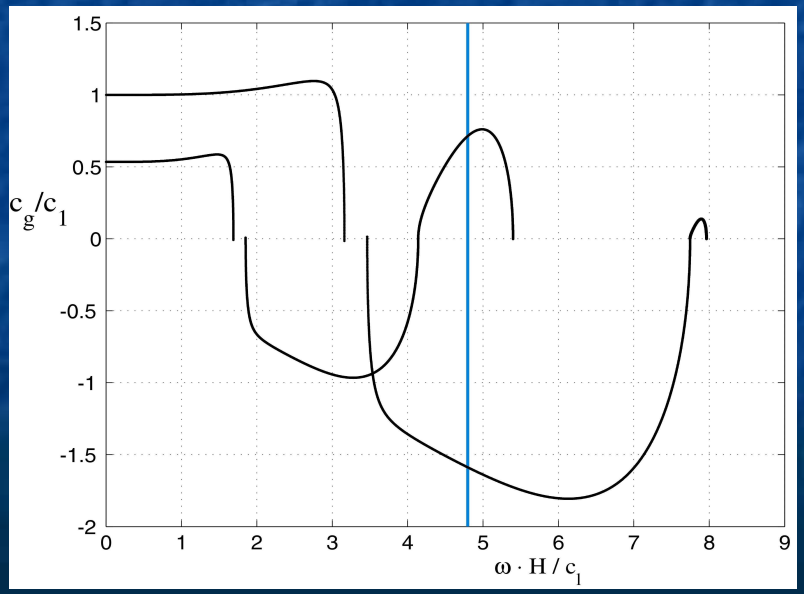

cg /c1
ω · H / c1

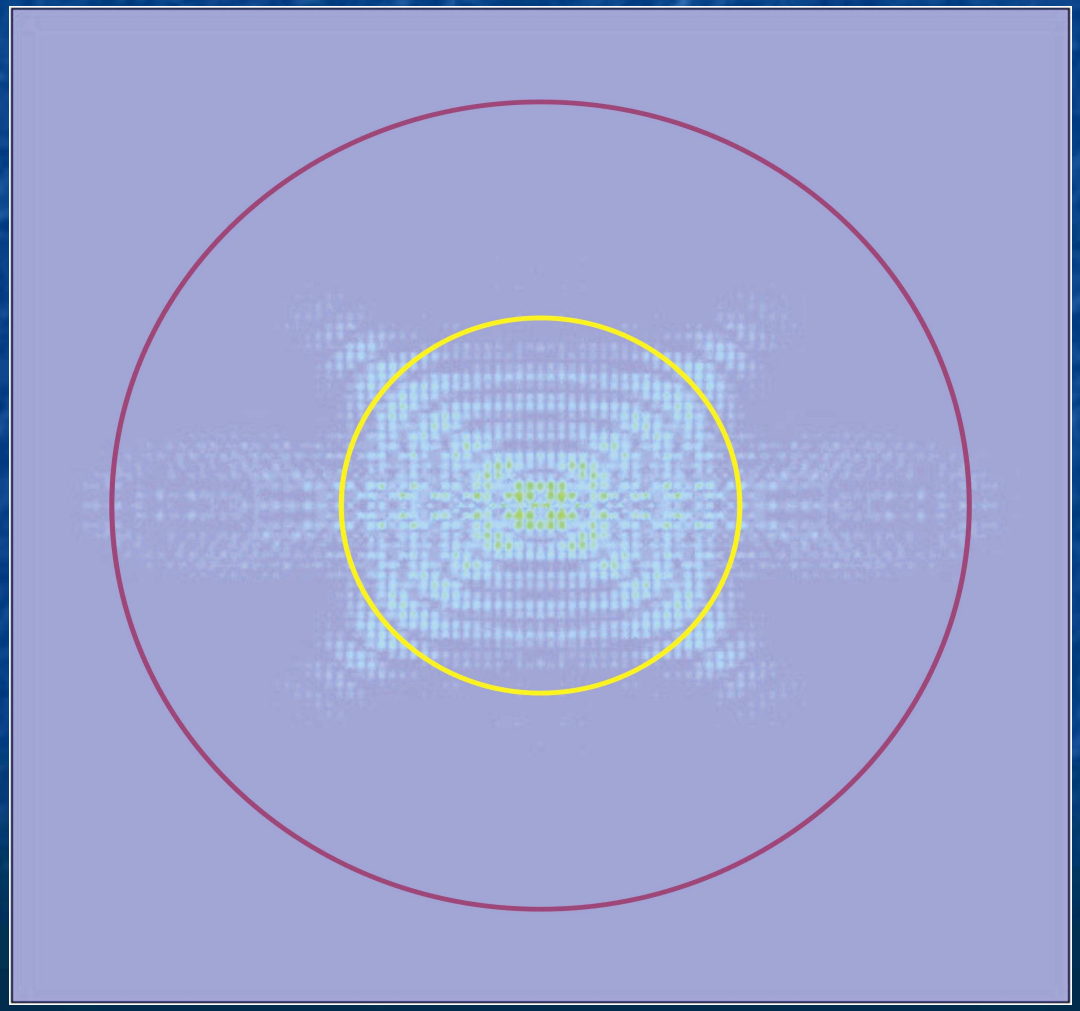

branch b4

branch b5

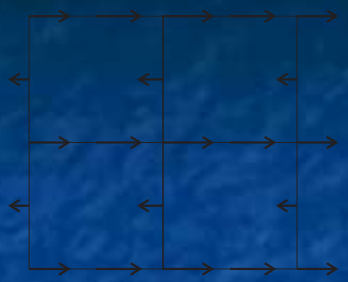
$$\omega H / c_1 = 4.8$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical


cg /c1
ω · H / c1

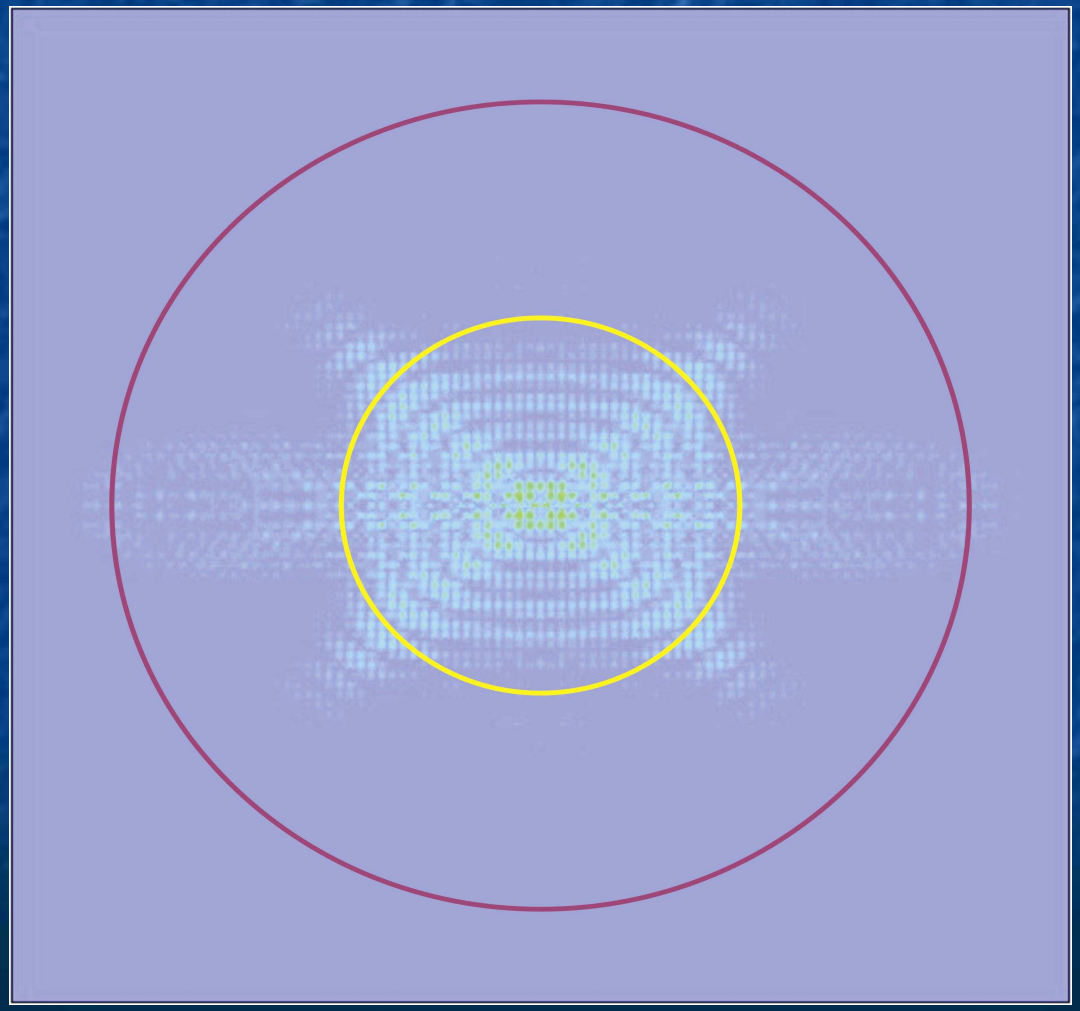


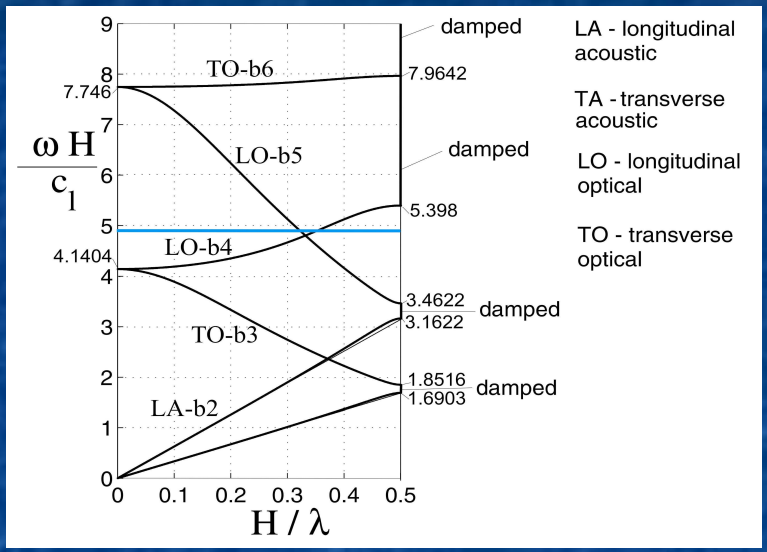
branch b4

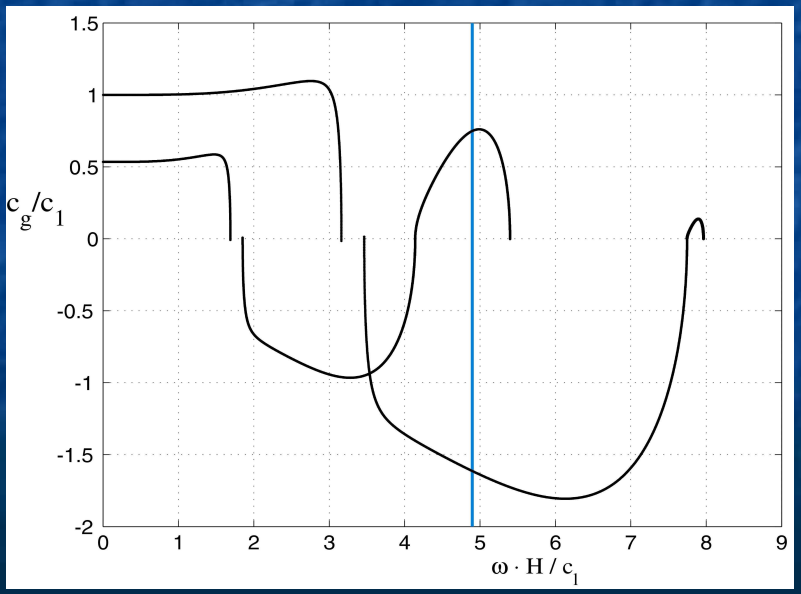


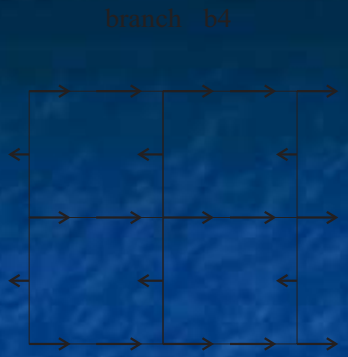
branch b5

$$\omega H / c_1 = 4.9$$



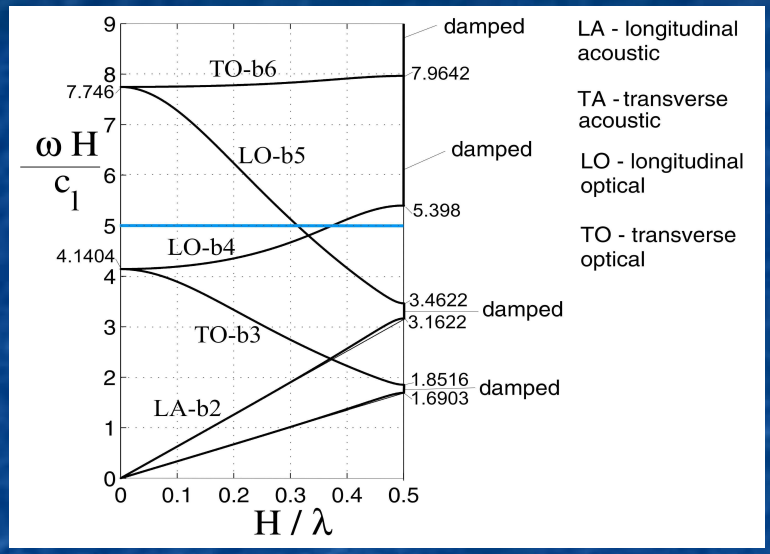


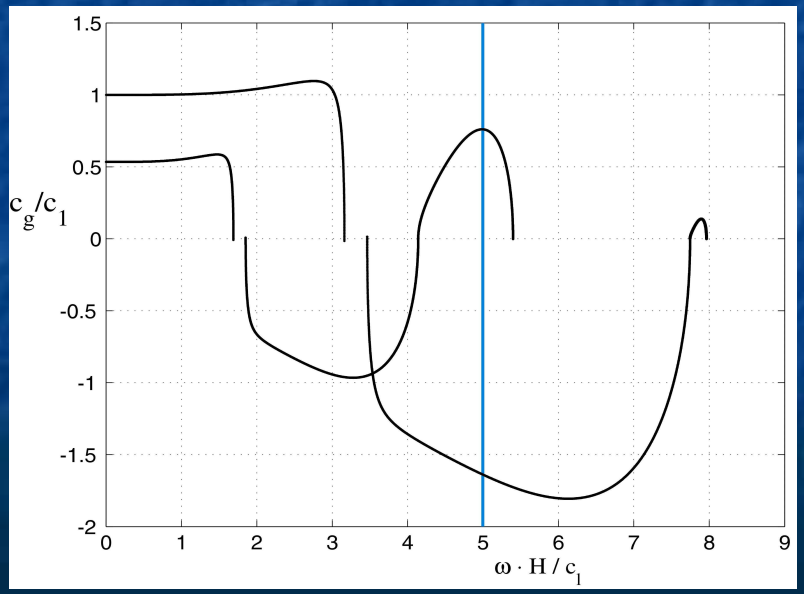


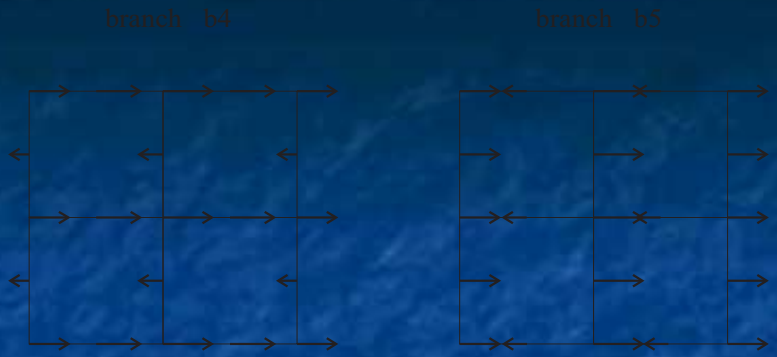

branch b4

branch b5

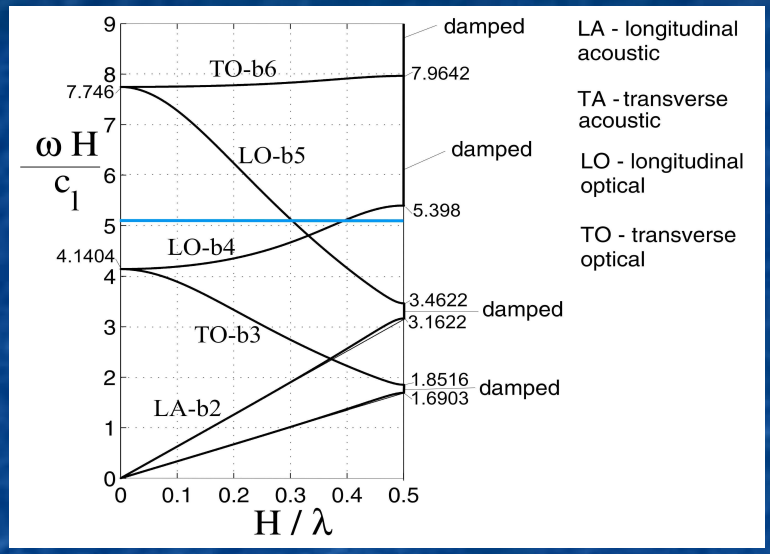
$$\omega H / c_1 = 5.0$$

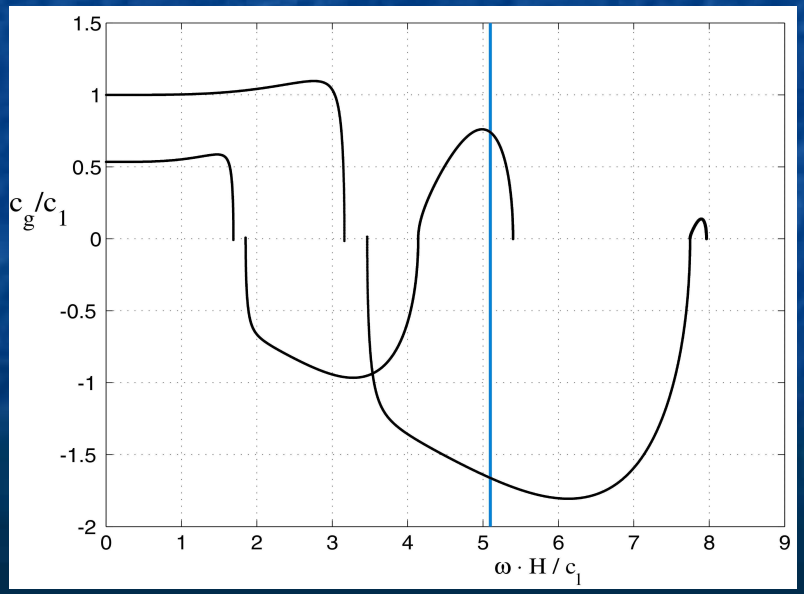

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

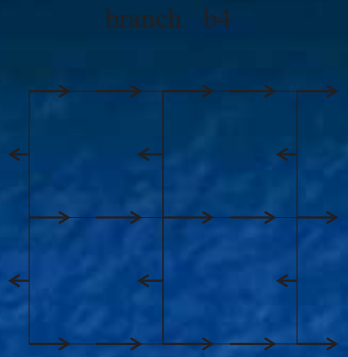

cg/c1
ω · H / c1


branch b4
branch b5

$$\omega H / c_1 = 5.1$$

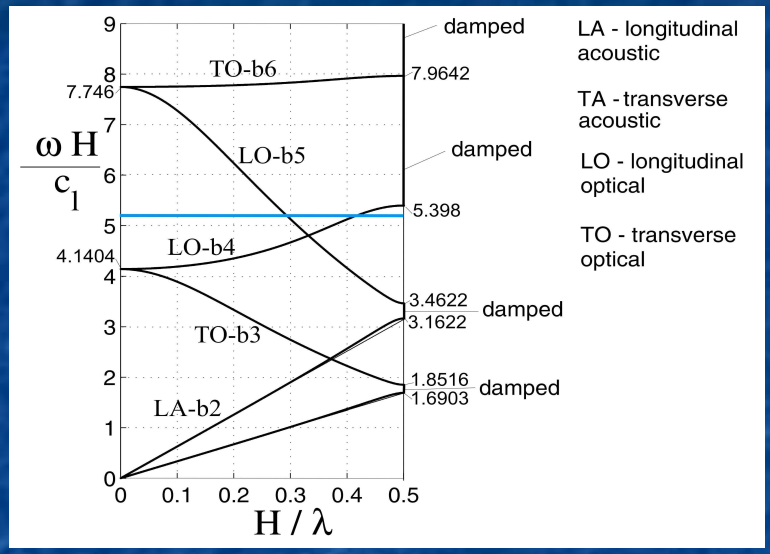

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

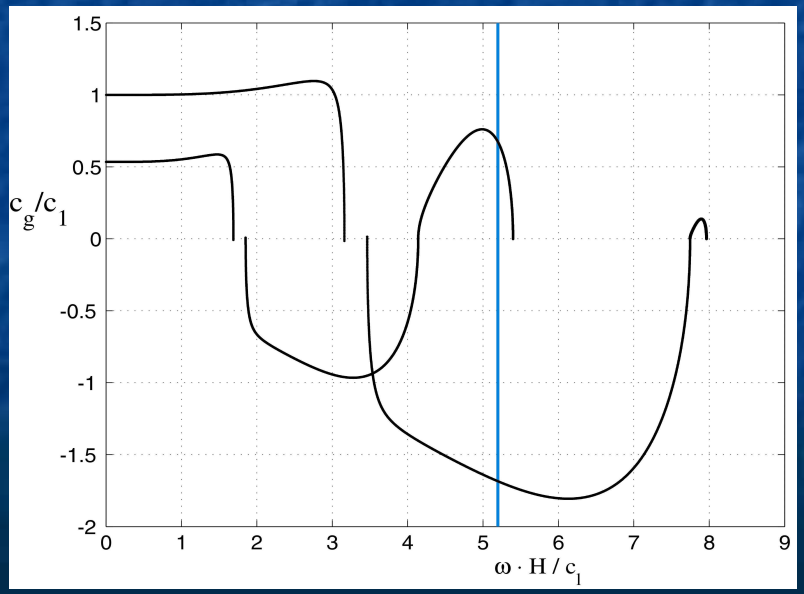

cg /c1
ω · H / c1

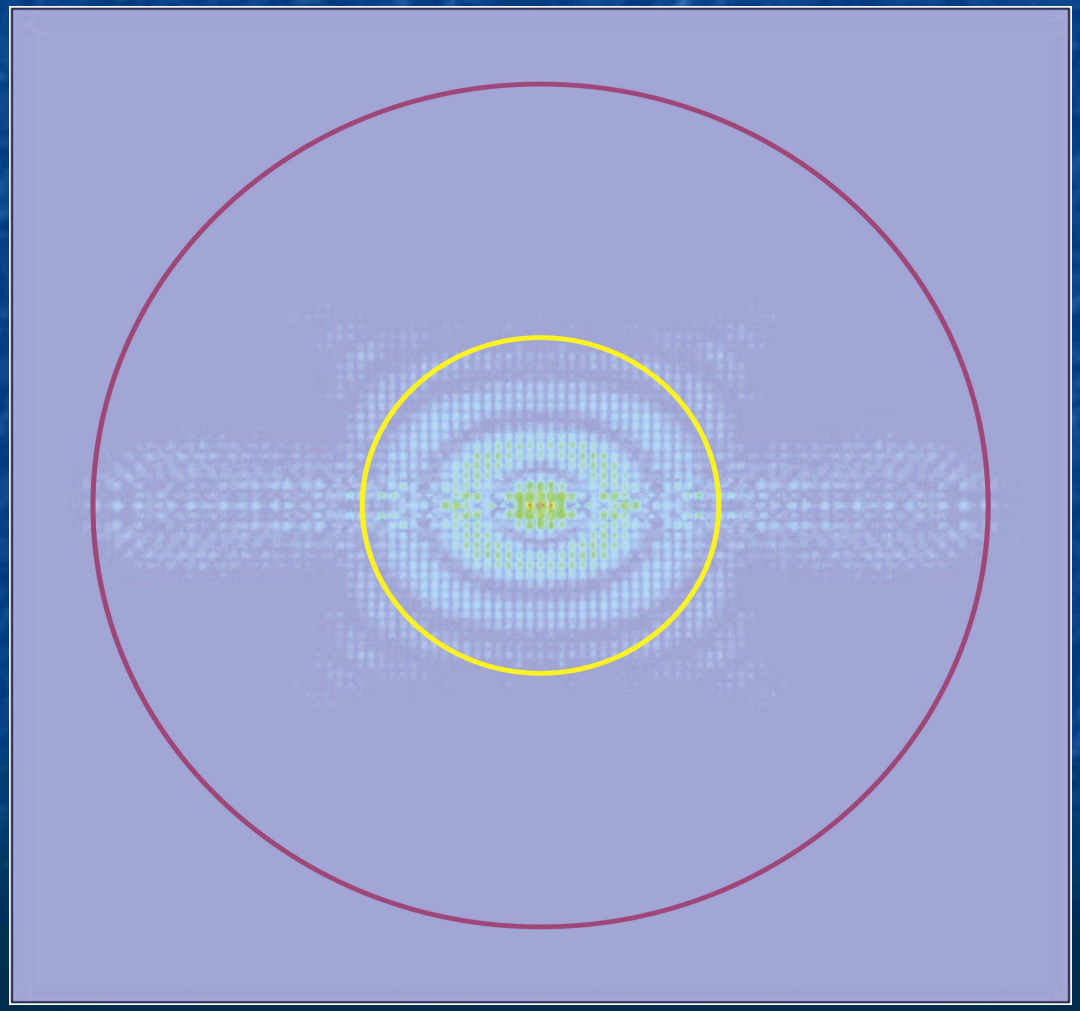

branch b4

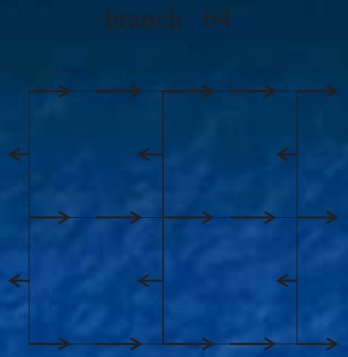
branch b5

$$\omega H / c_1 = 5.2$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

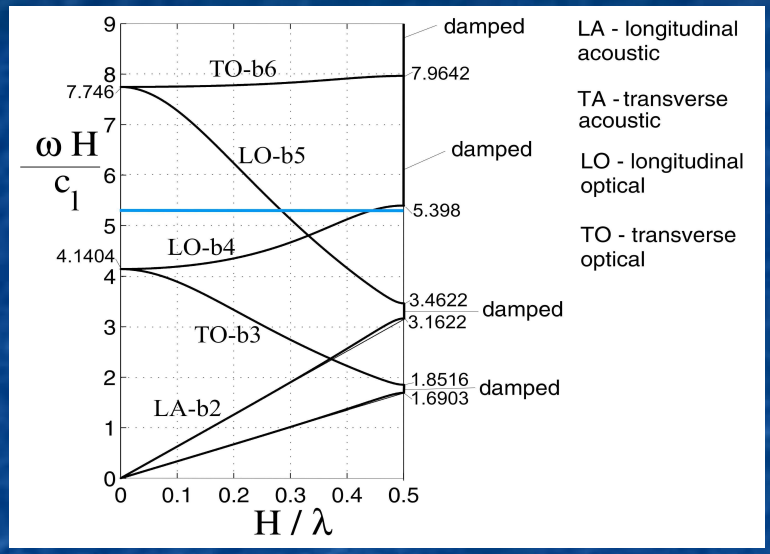

cg/c1
ω · H / c1

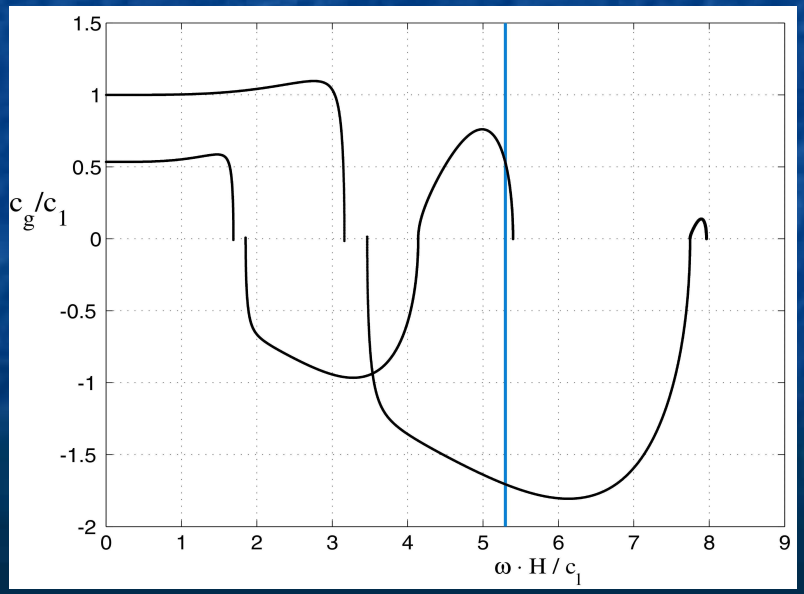


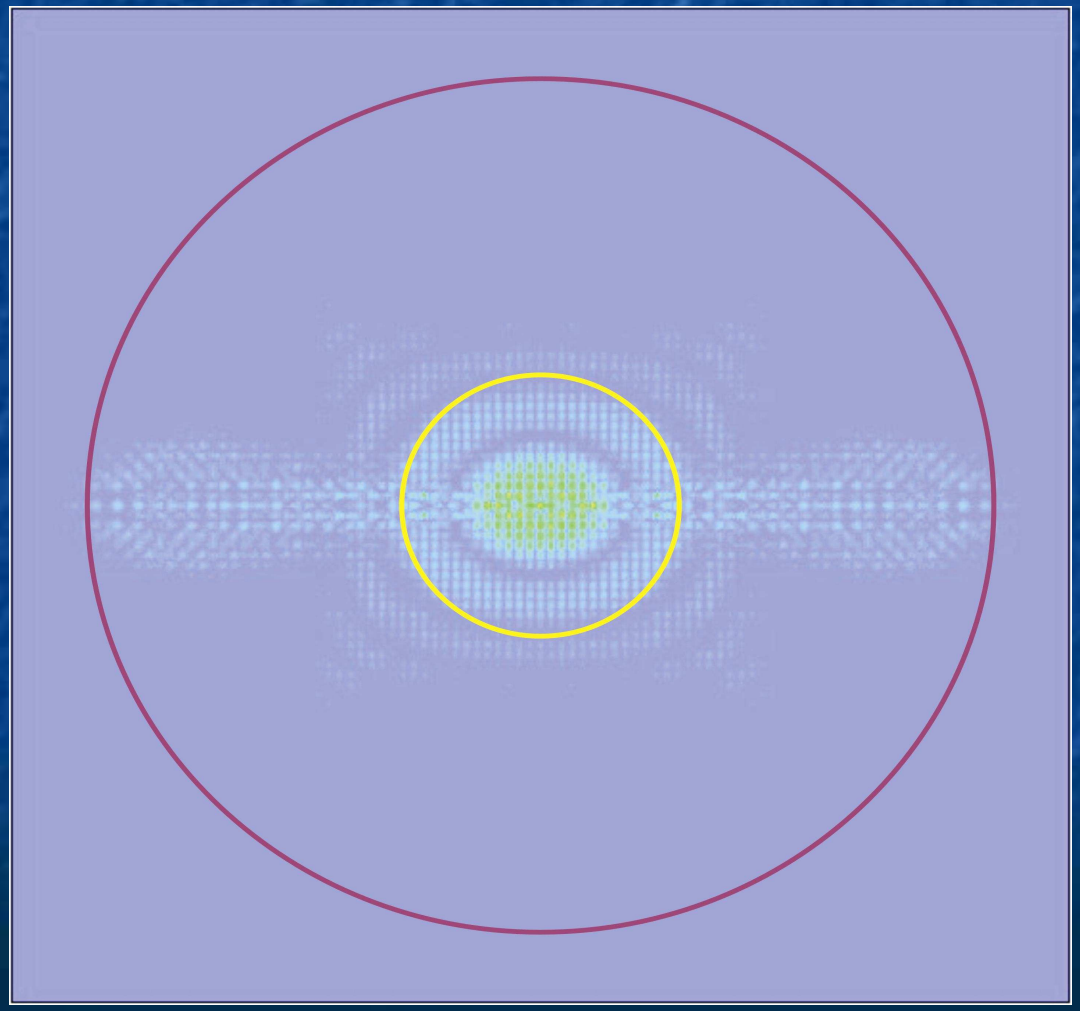

branch b4

branch b5

$$\omega H / c_1 = 5.3$$

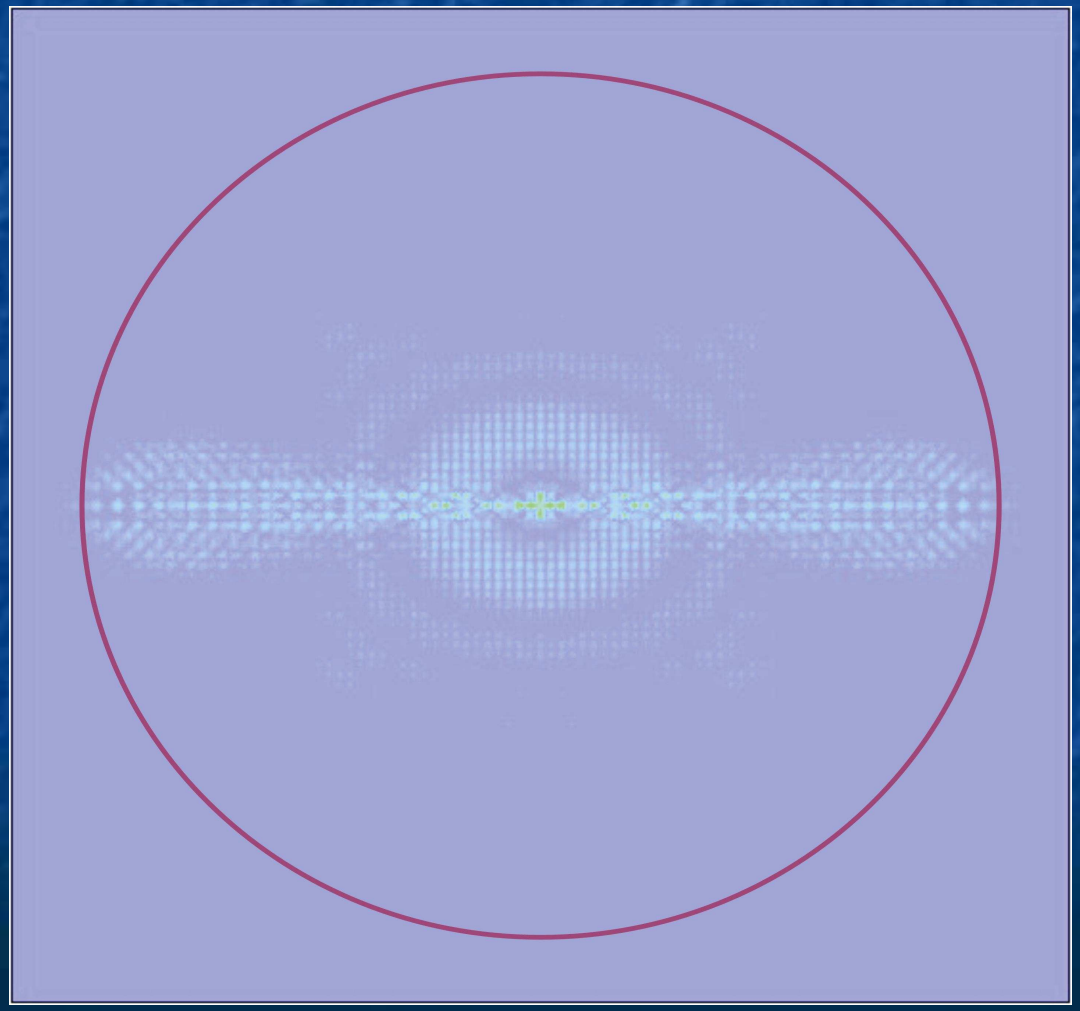

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

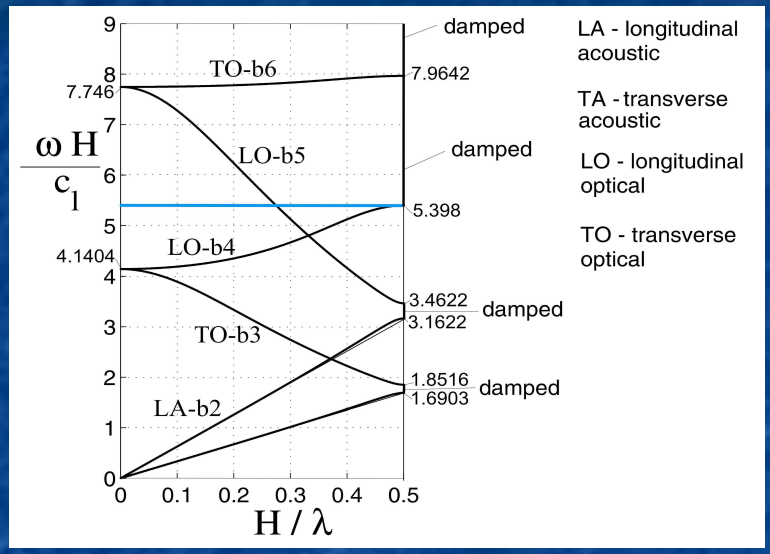

cg/c1
ω · H / c1

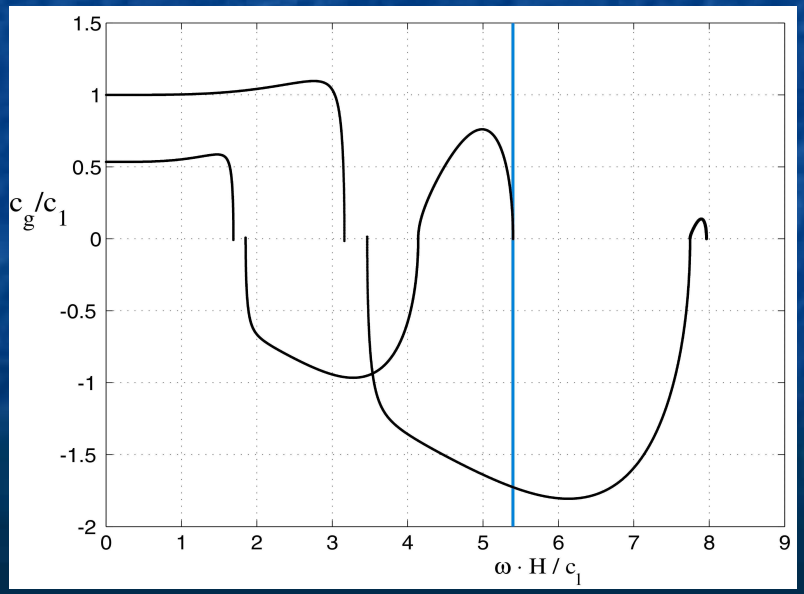


branch b5

$$\omega H / c_1 = 5.4$$

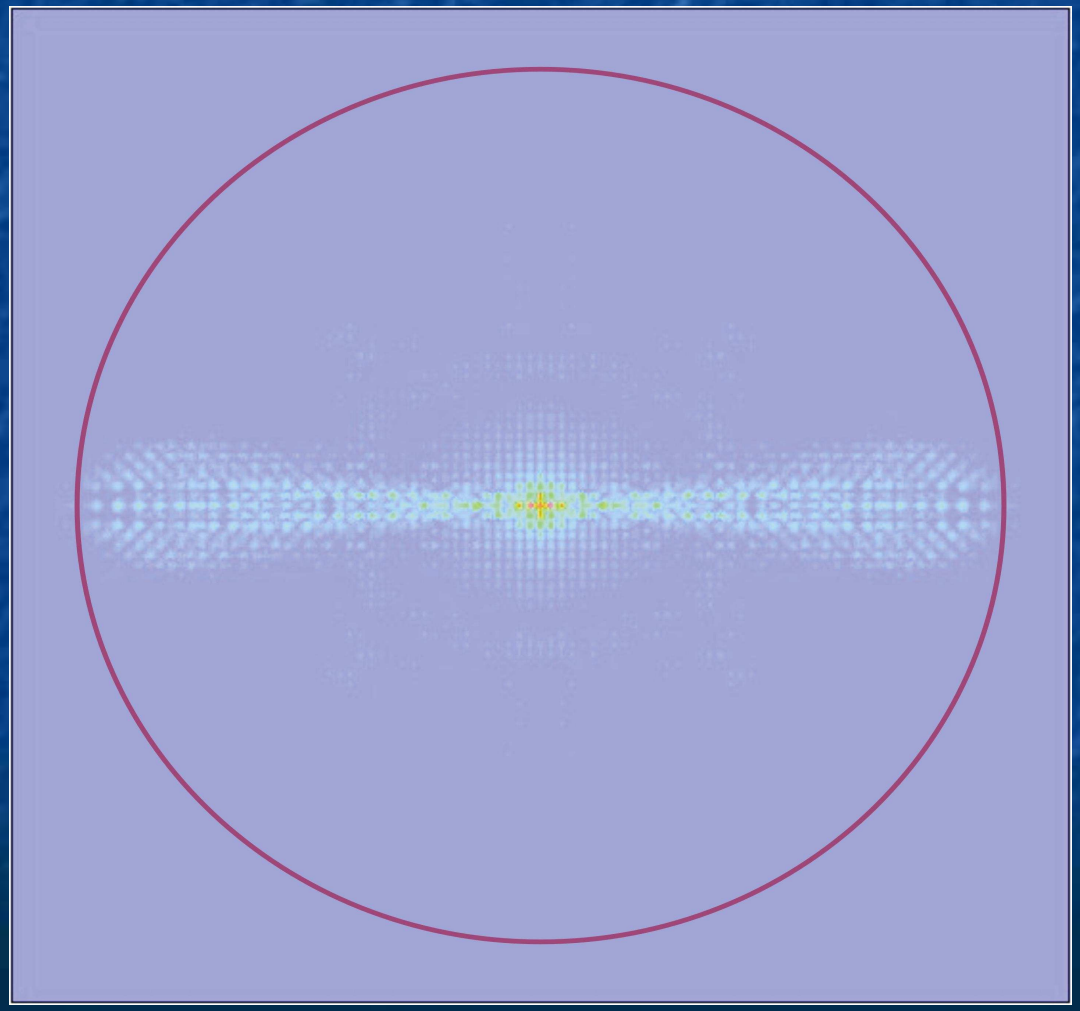


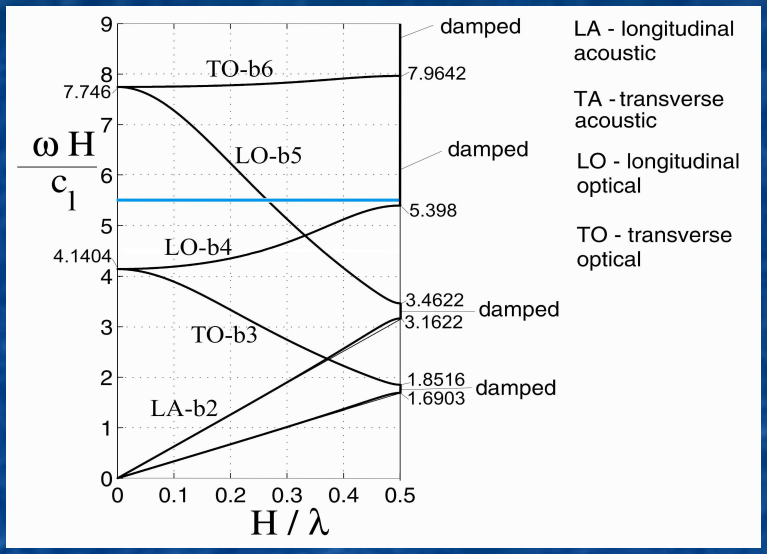


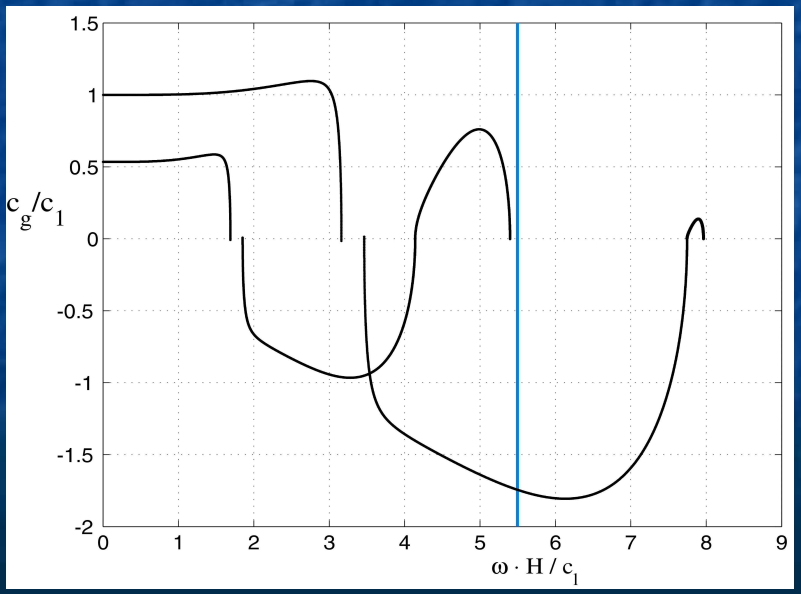


branch b5

$$\omega H / c_1 = 5.5$$

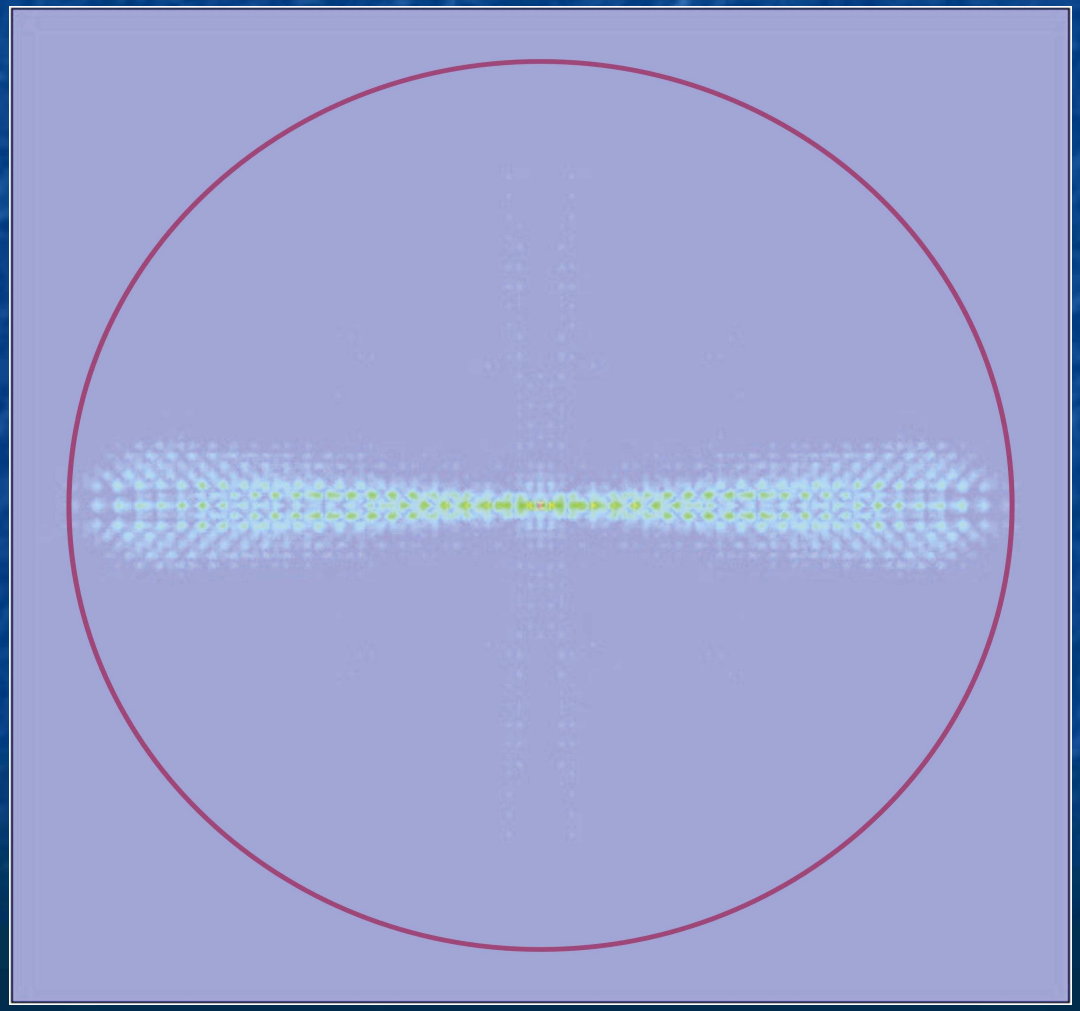


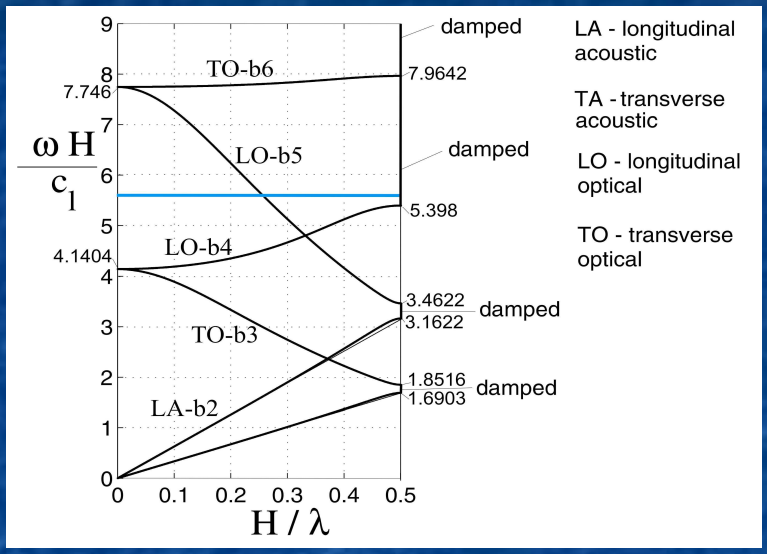


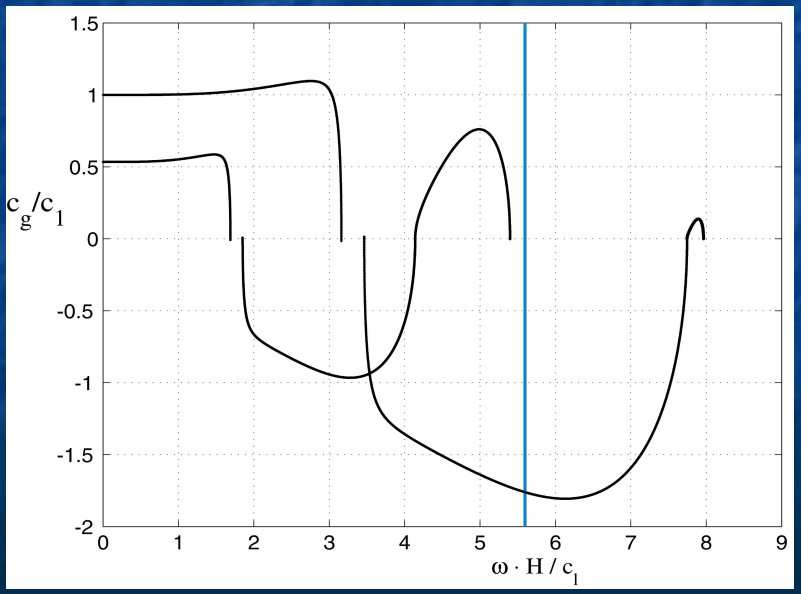


branch b5

$$\omega H / c_1 = 5.6$$

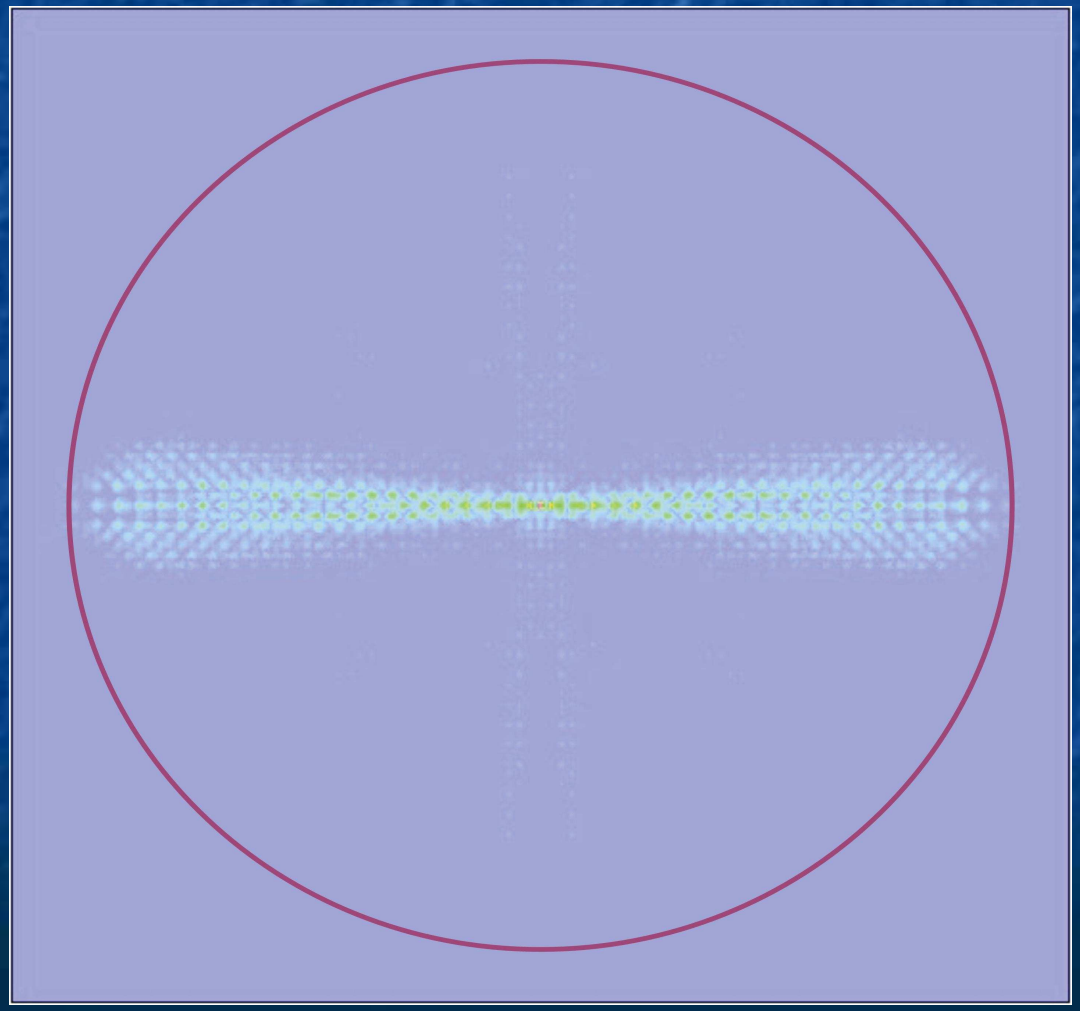


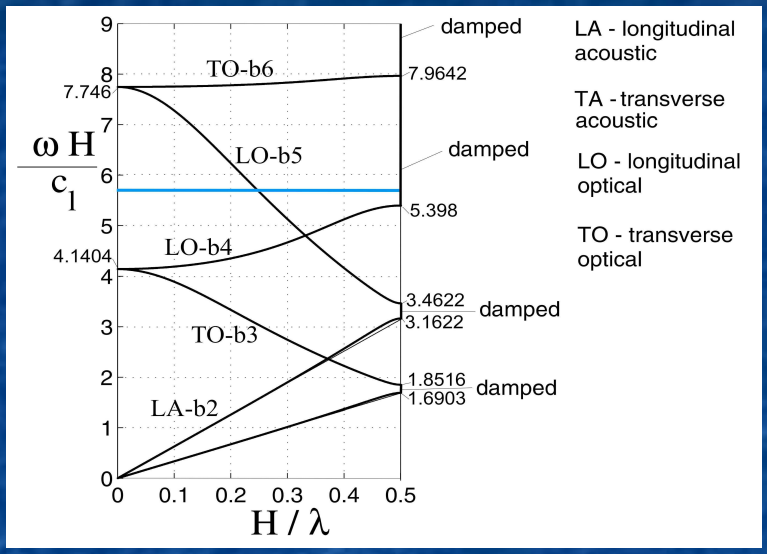


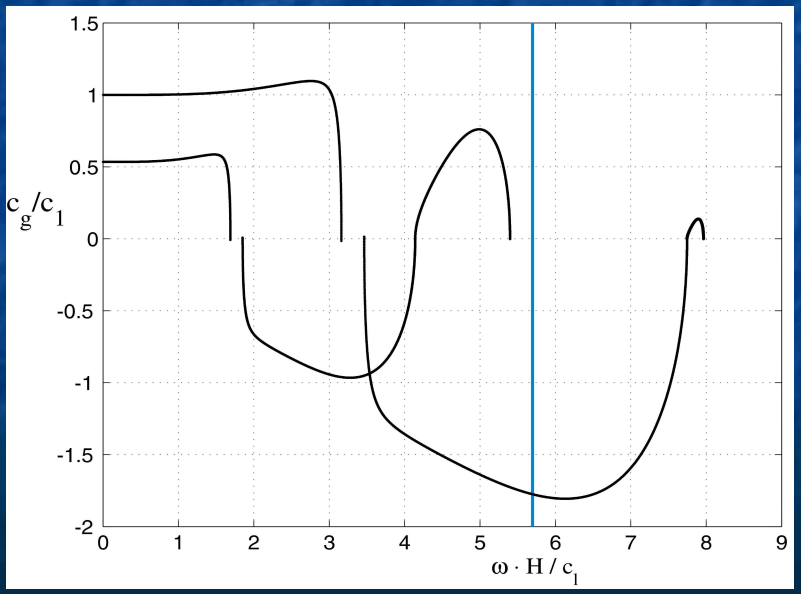


branch b5

$$\omega H / c_1 = 5.7$$

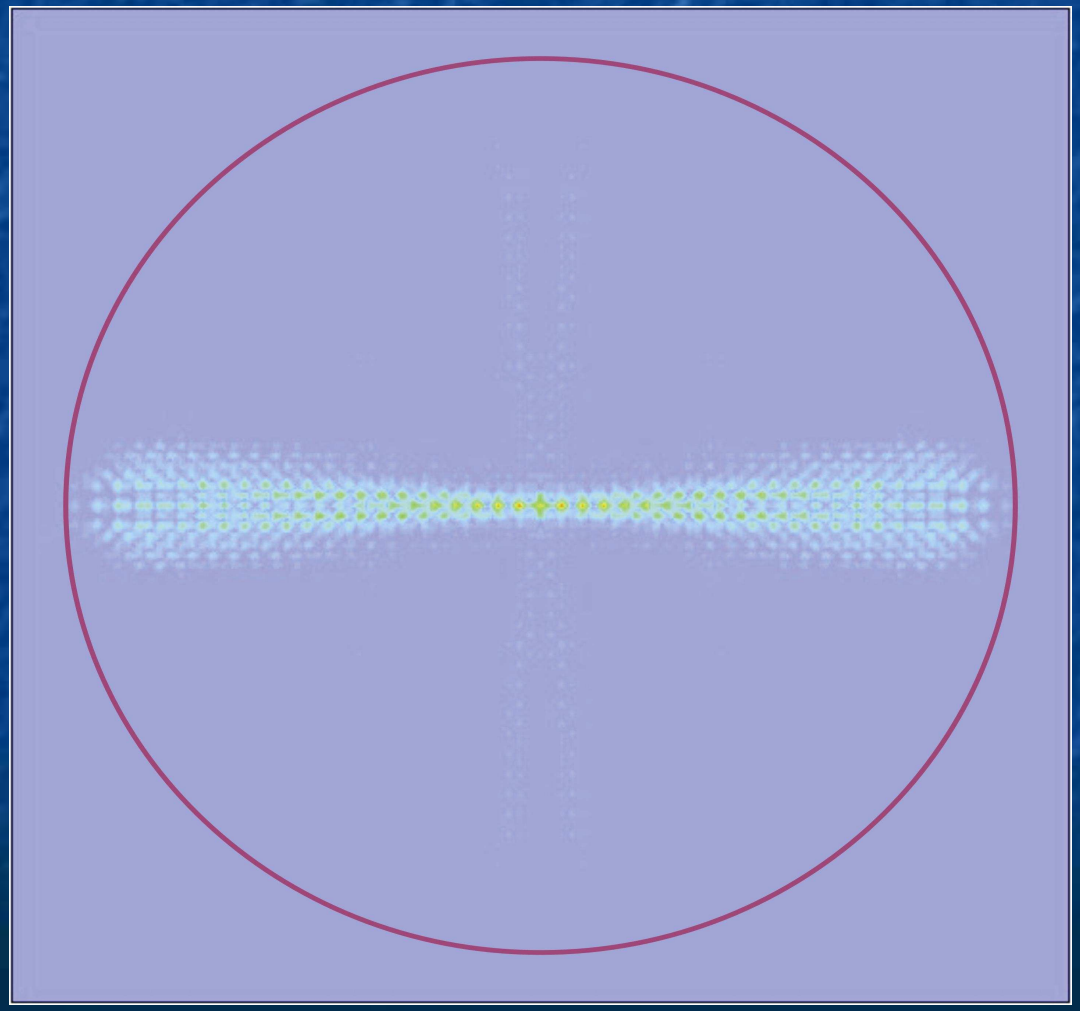


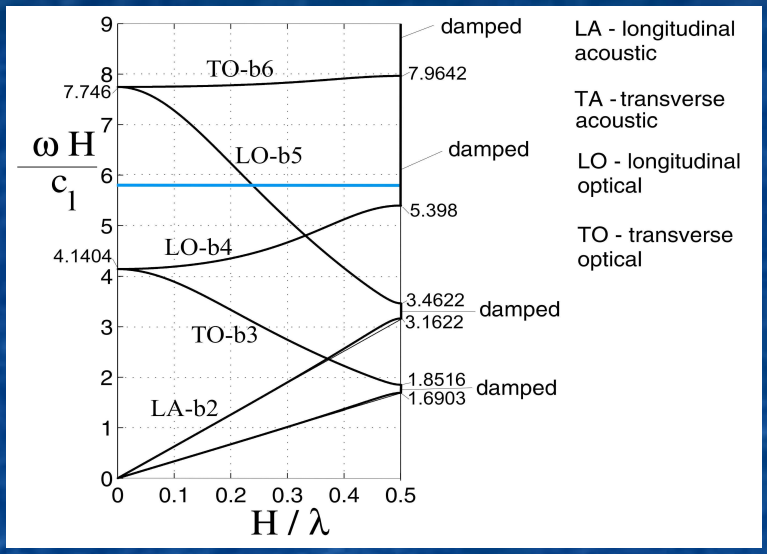


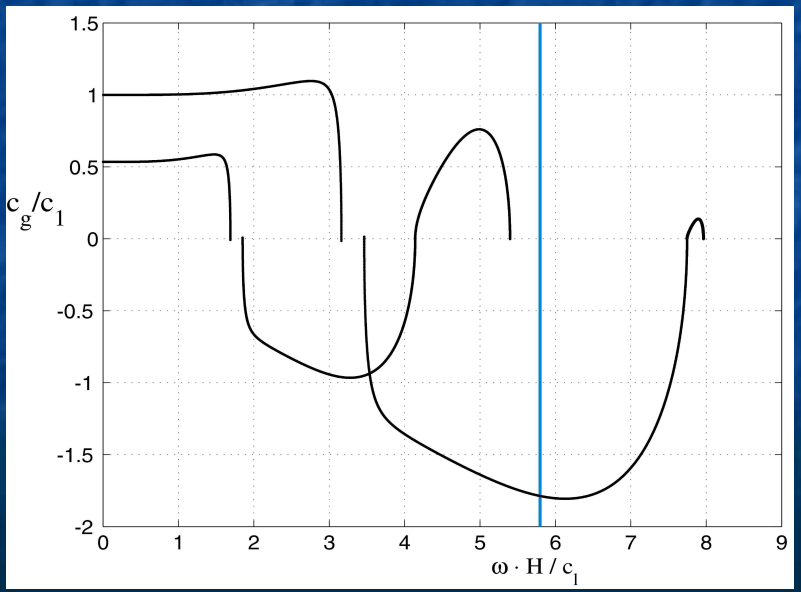


branch b5

$$\omega H / c_1 = 5.8$$

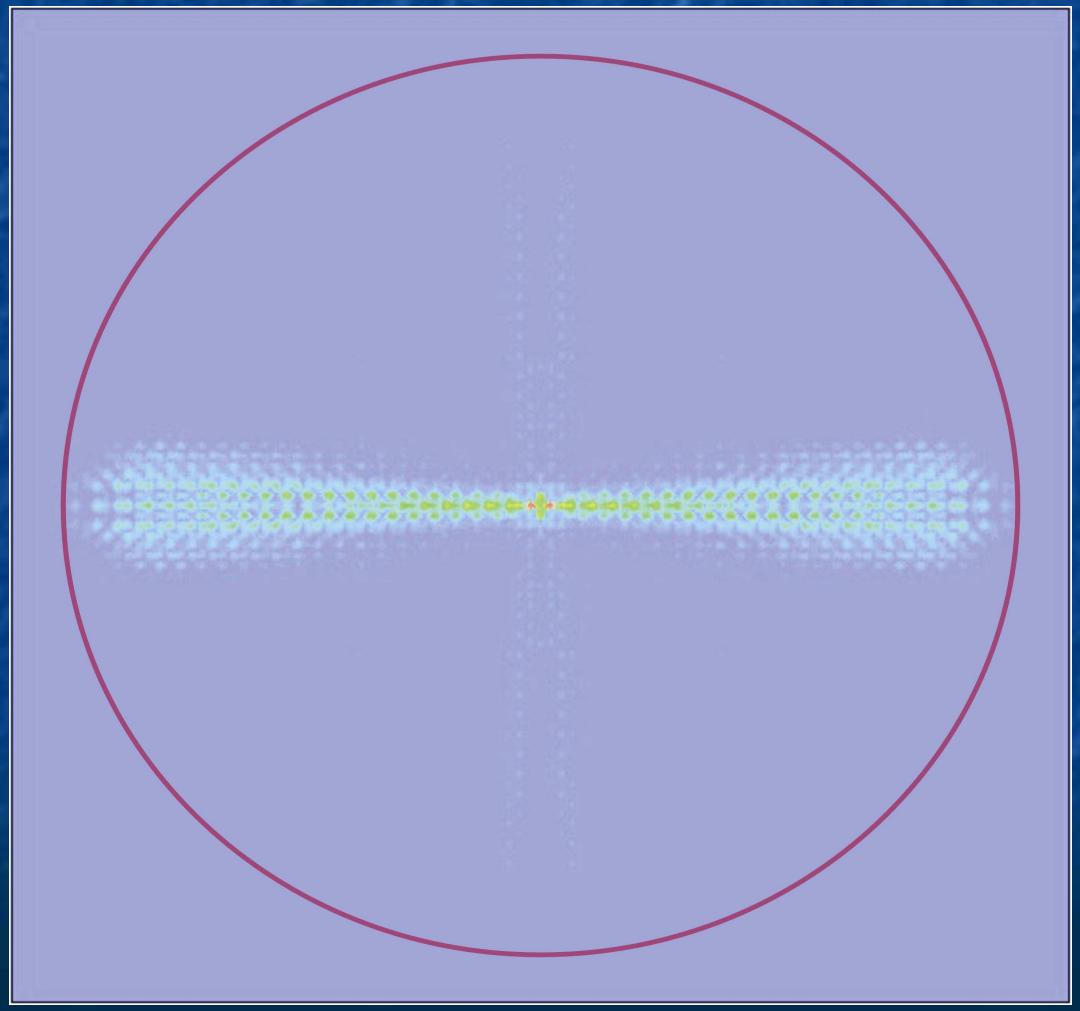


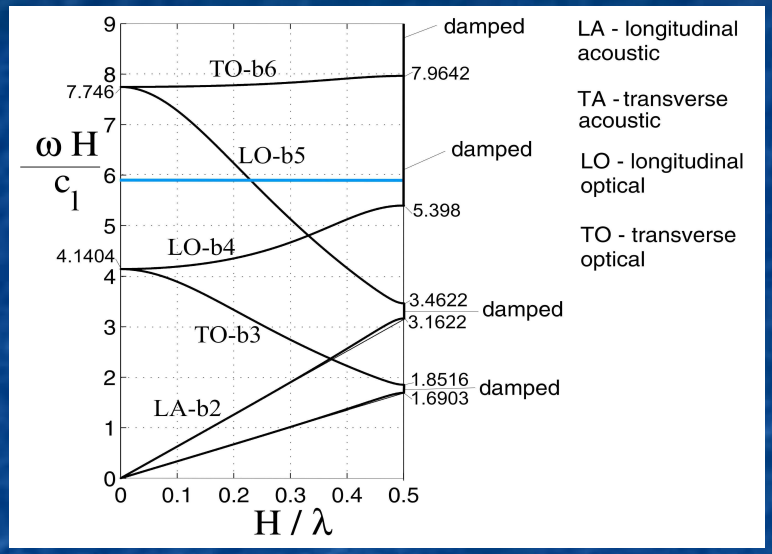


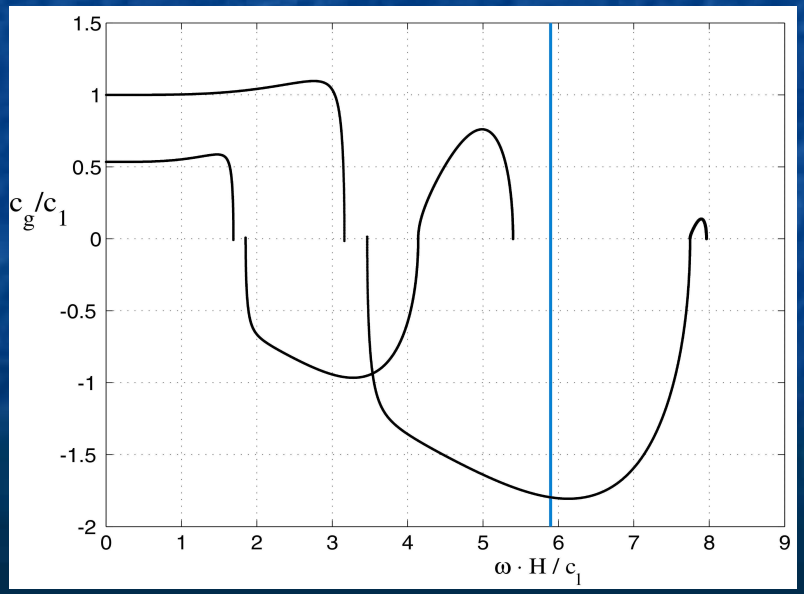


branch b5

$$\omega H / c_1 = 5.9$$

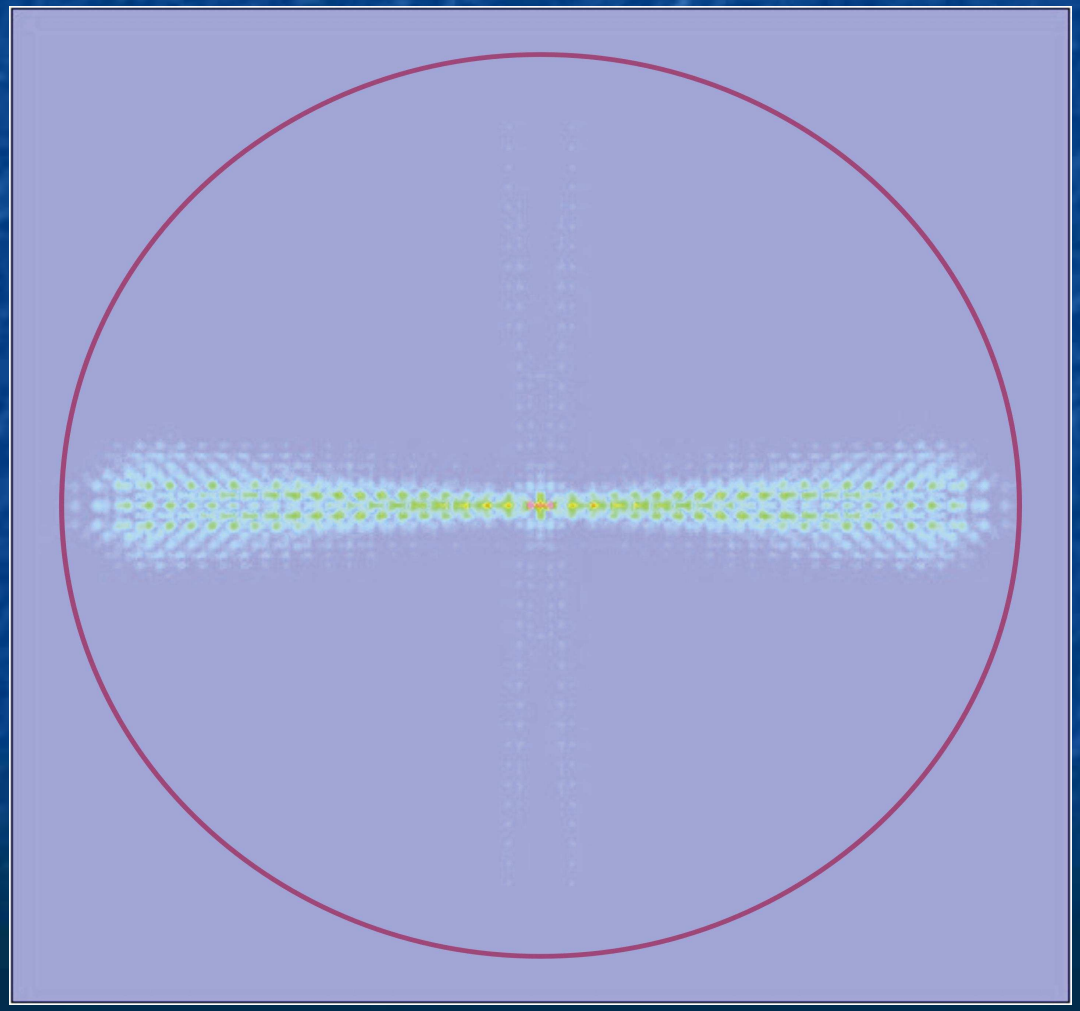


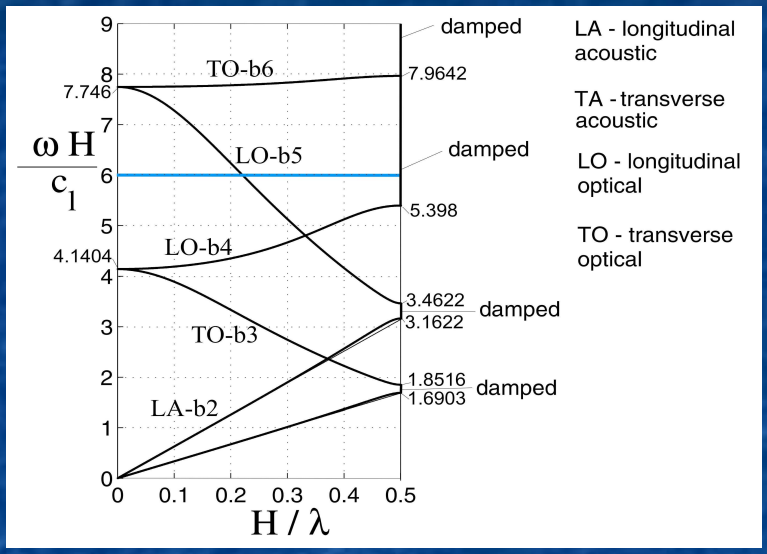


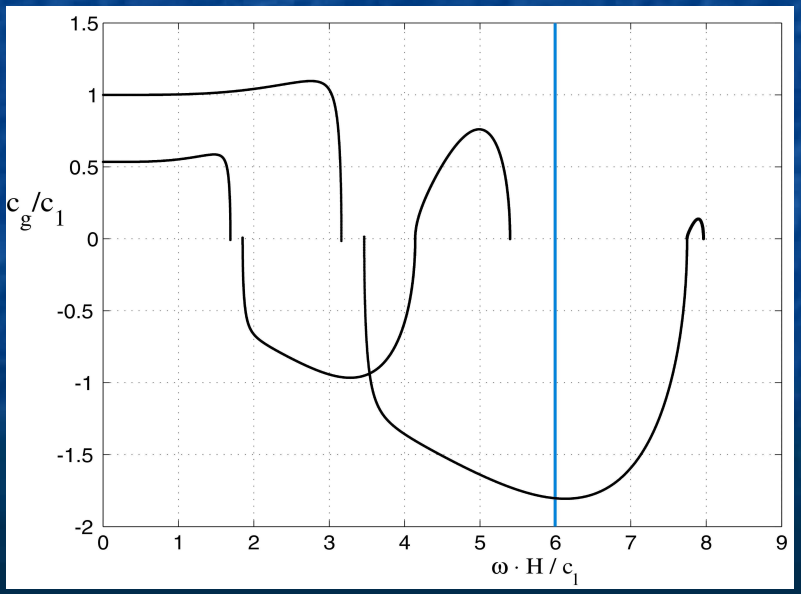


branch b5

$$\omega H / c_1 = 6.0$$

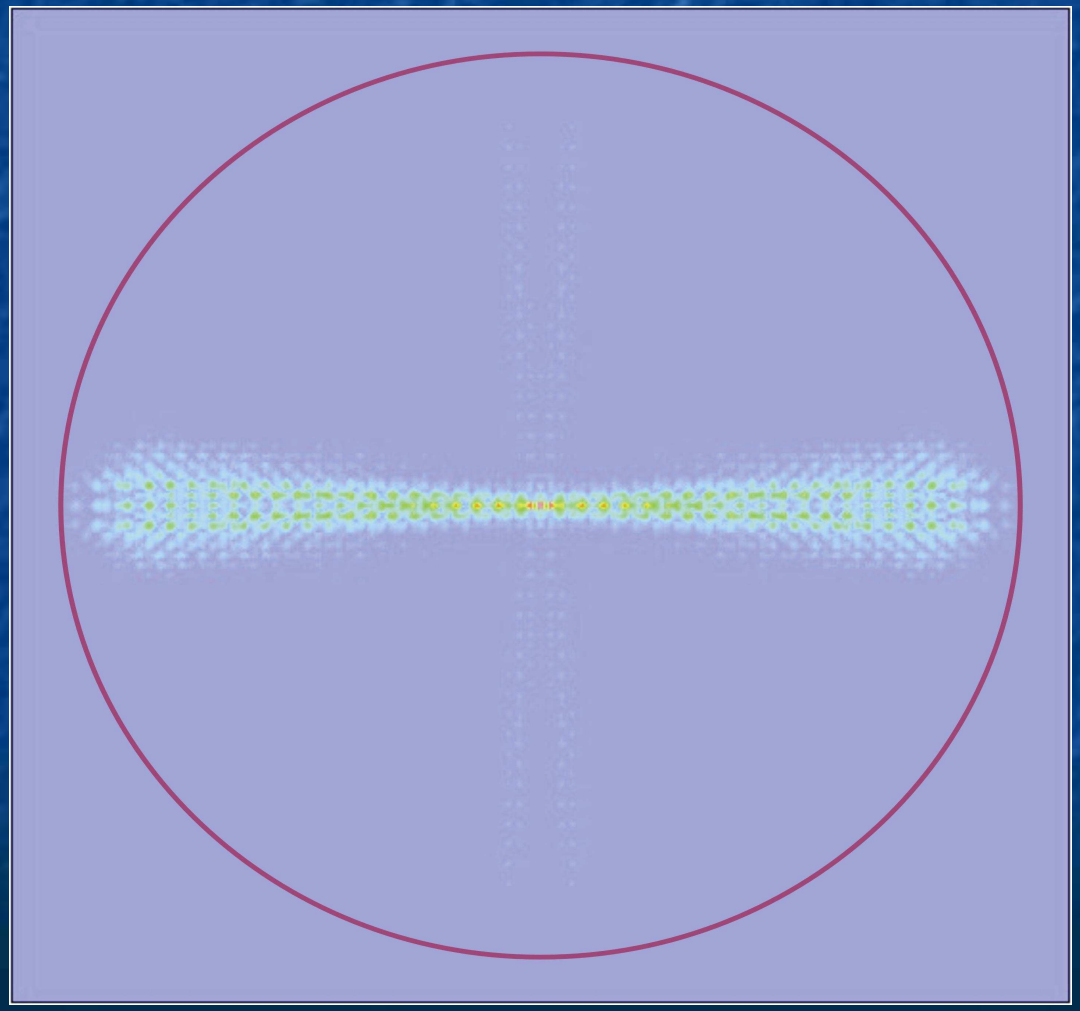


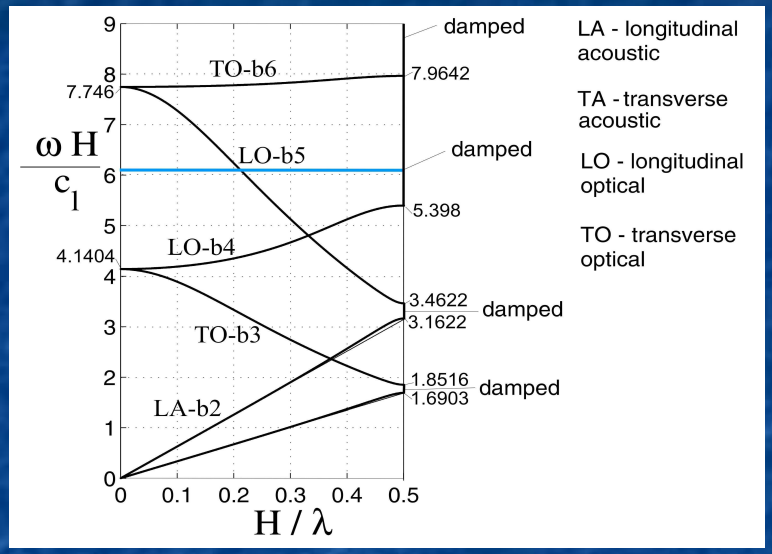


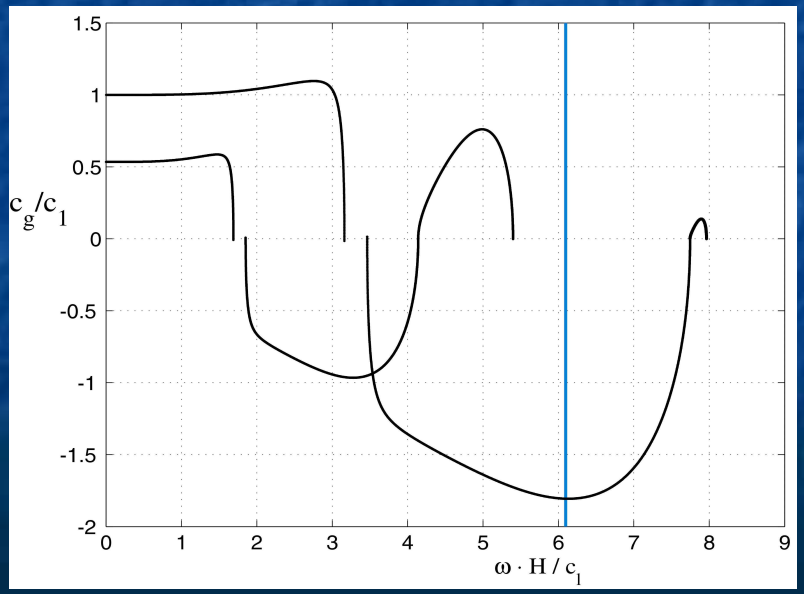


branch b5

$$\omega H / c_1 = 6.1$$

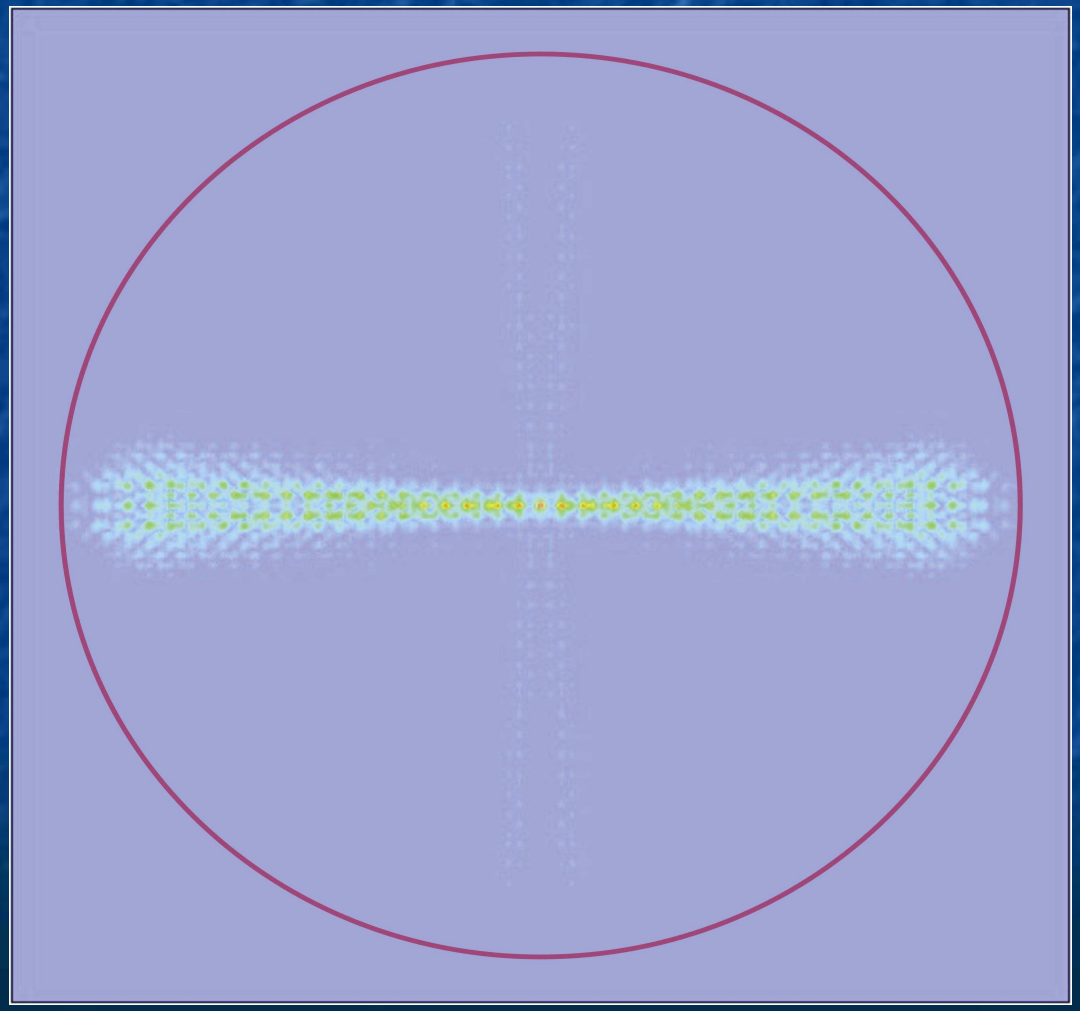


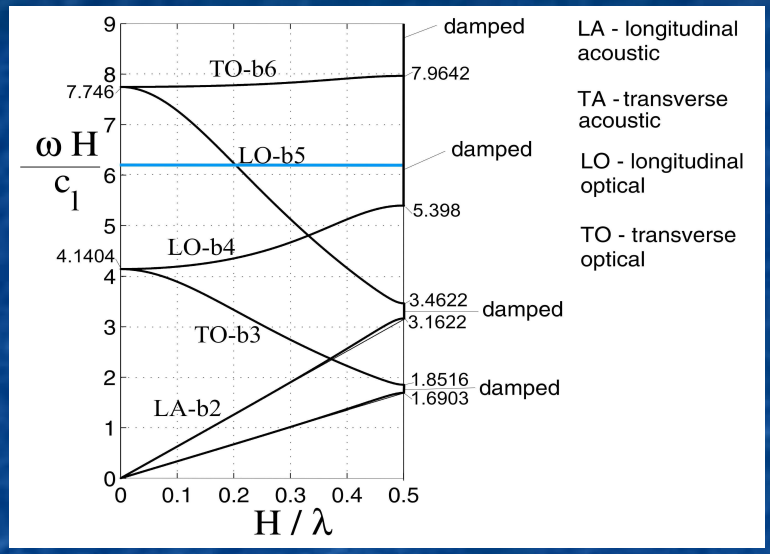


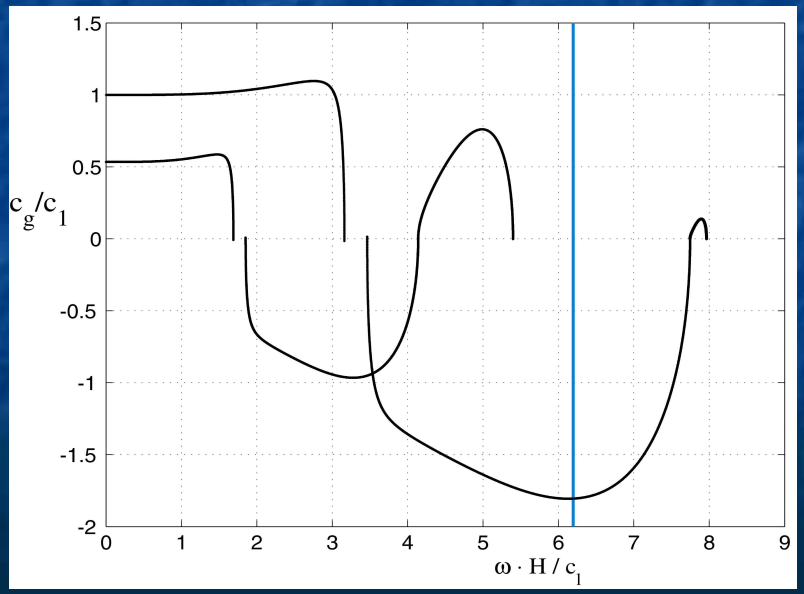


branch b5

$$\omega H / c_1 = 6.2$$

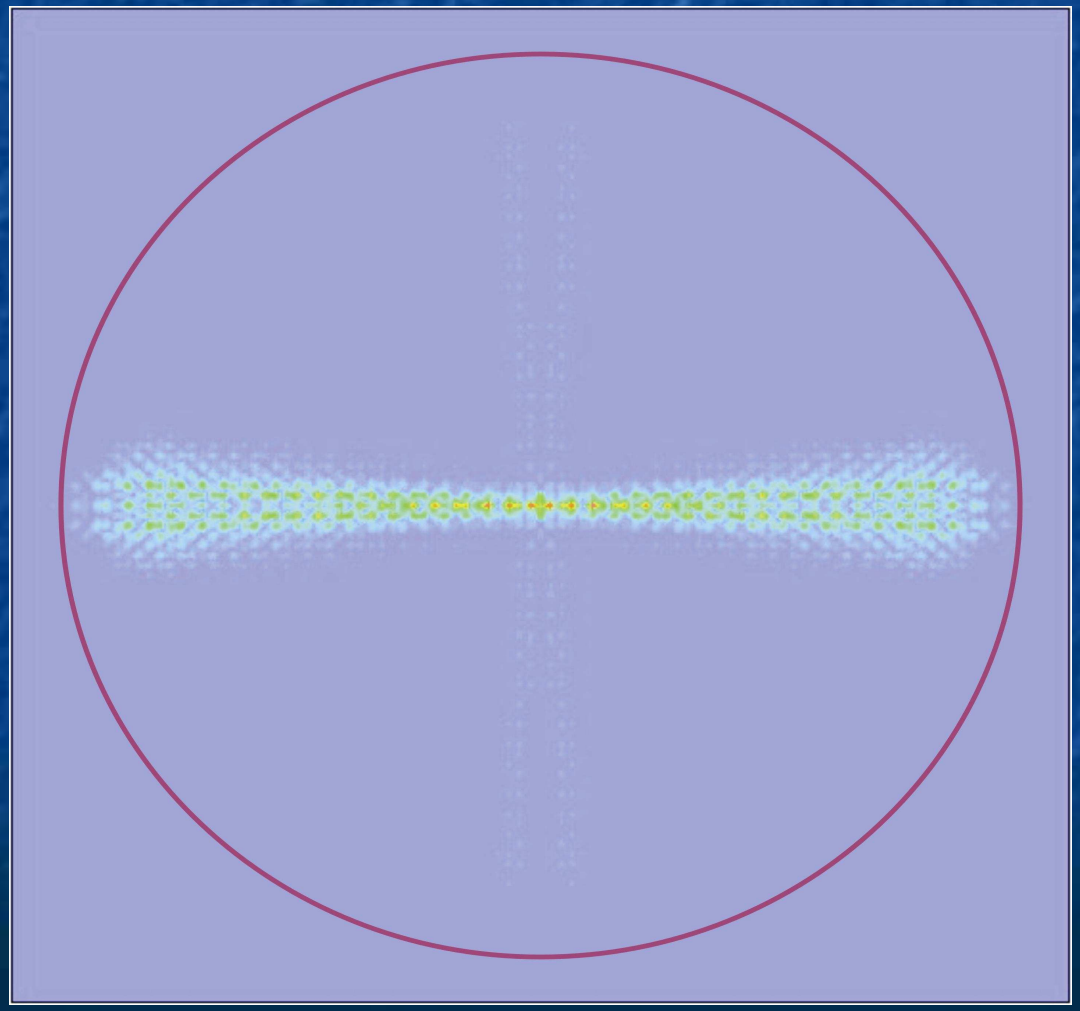


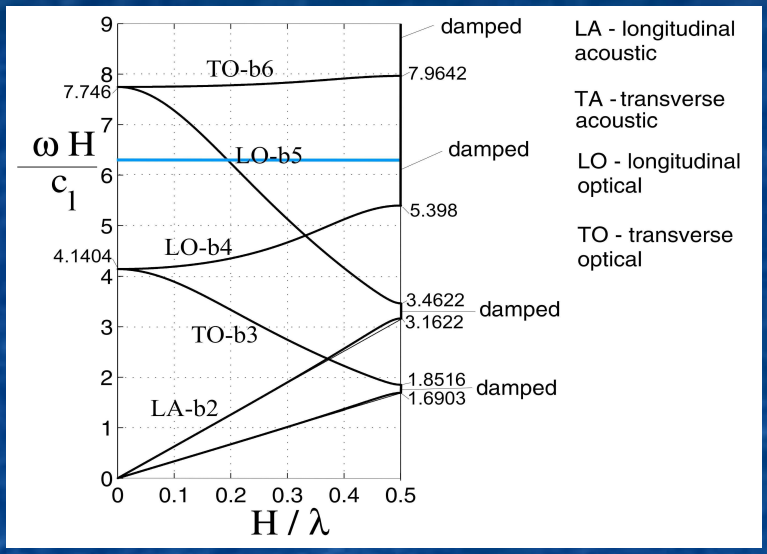


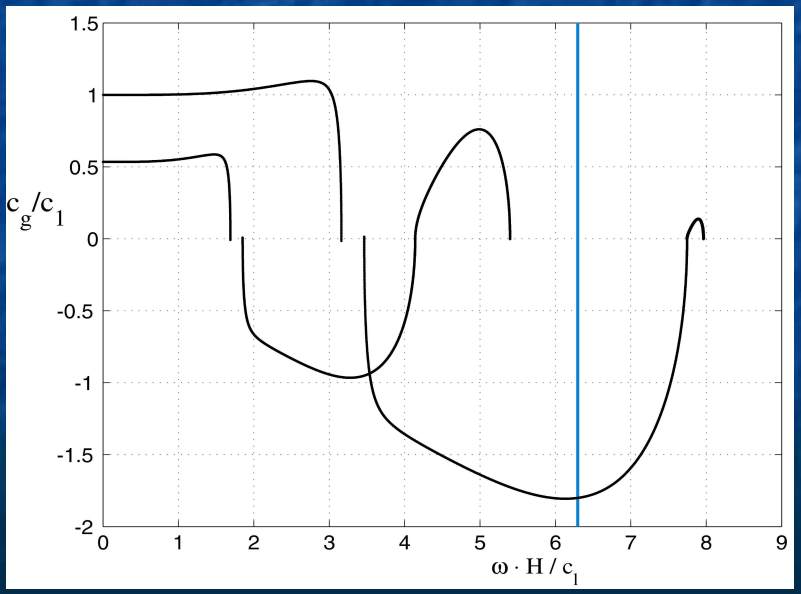


branch b5

$$\omega H / c_1 = 6.3$$

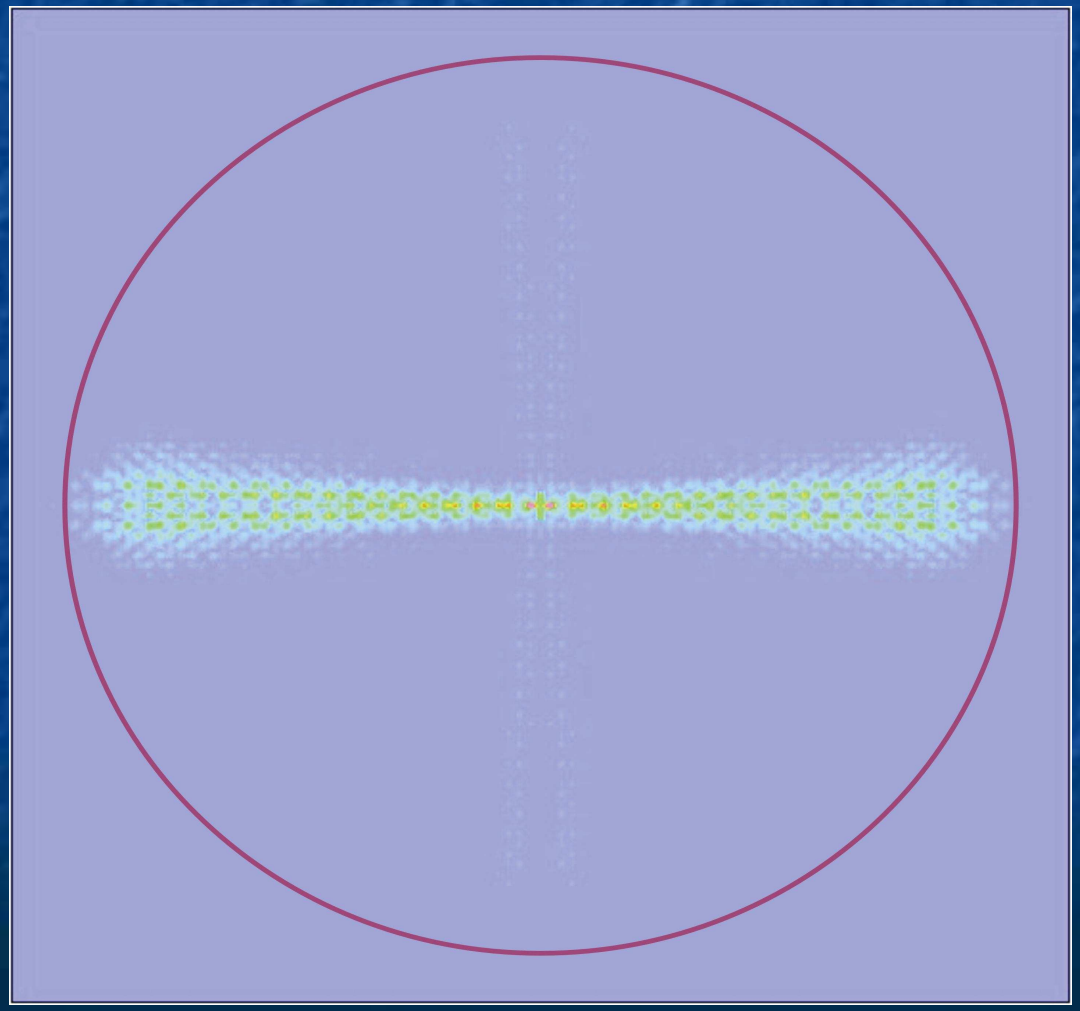


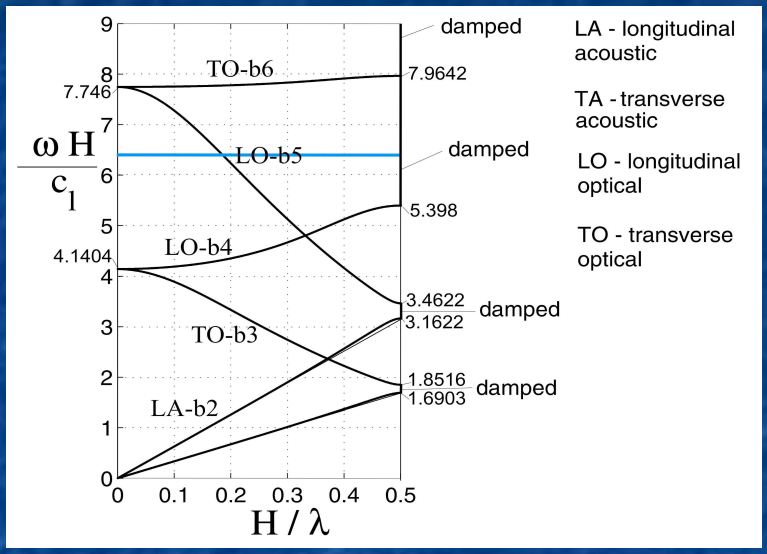


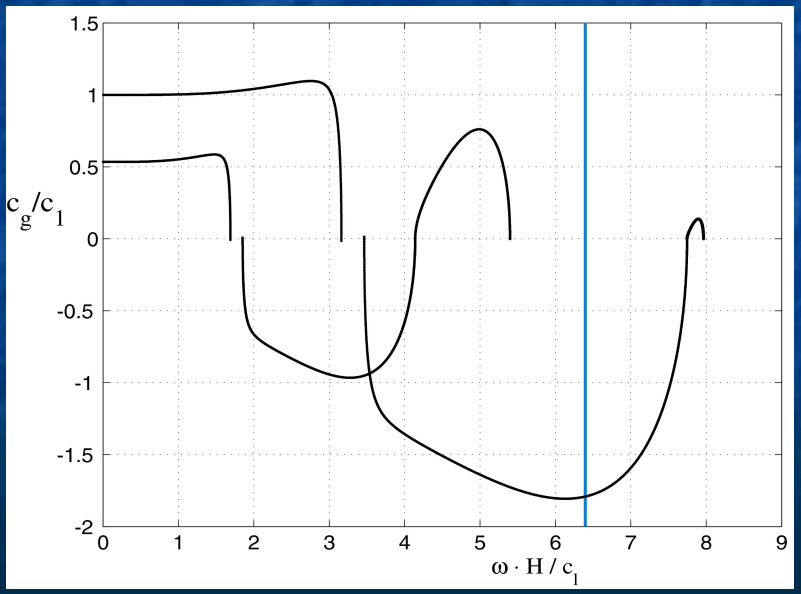


branch b5

$$\omega H / c_1 = 6.4$$

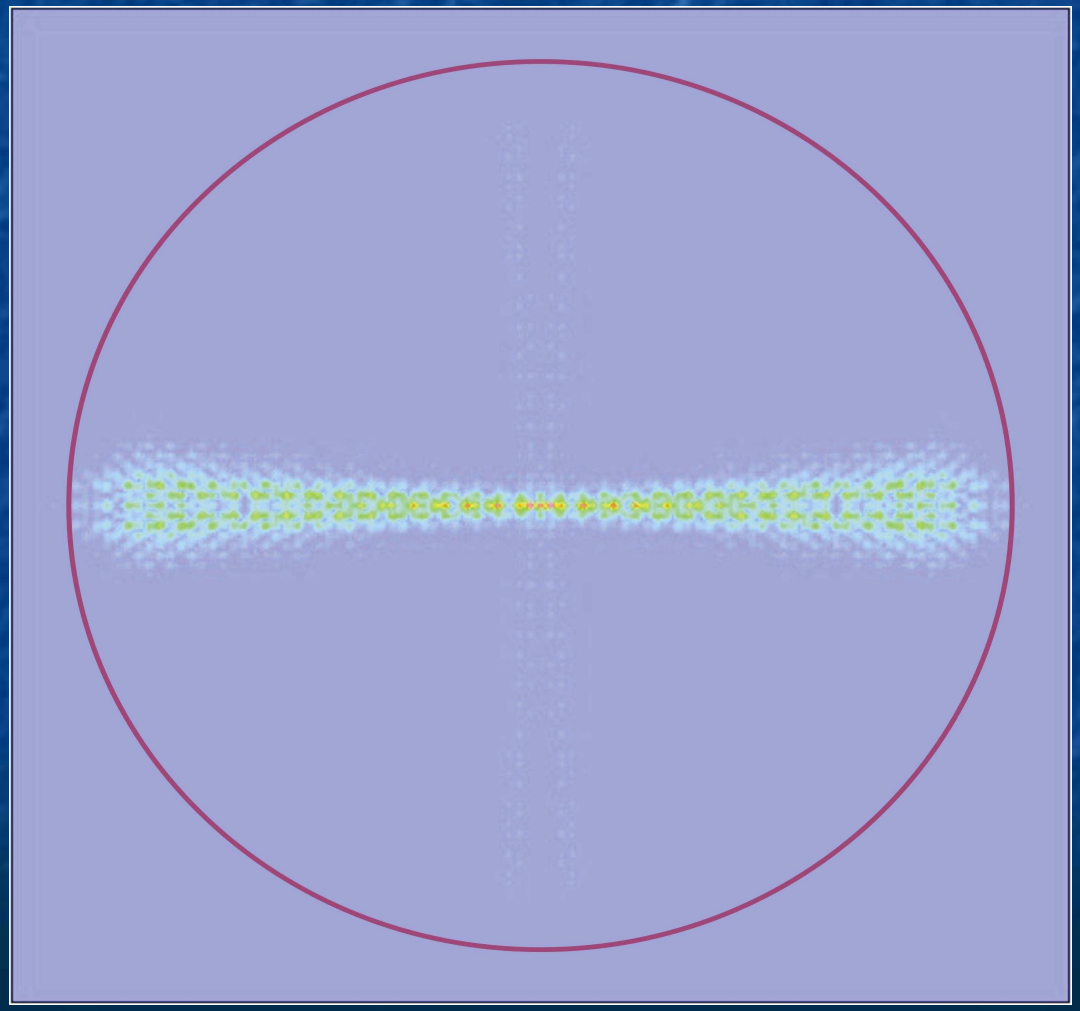


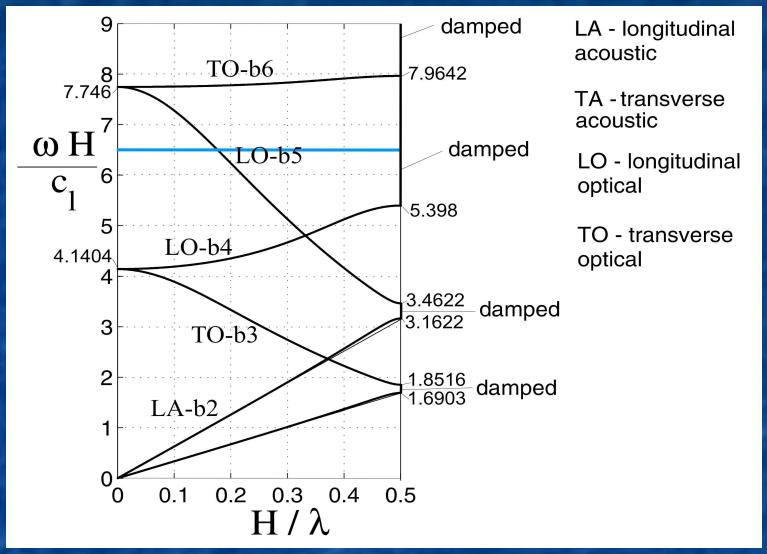


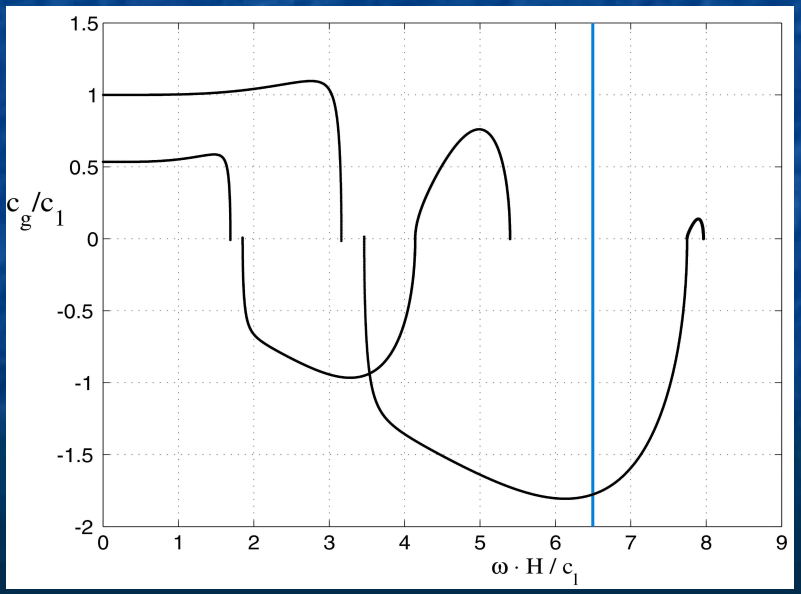


branch b5

$$\omega H / c_1 = 6.5$$

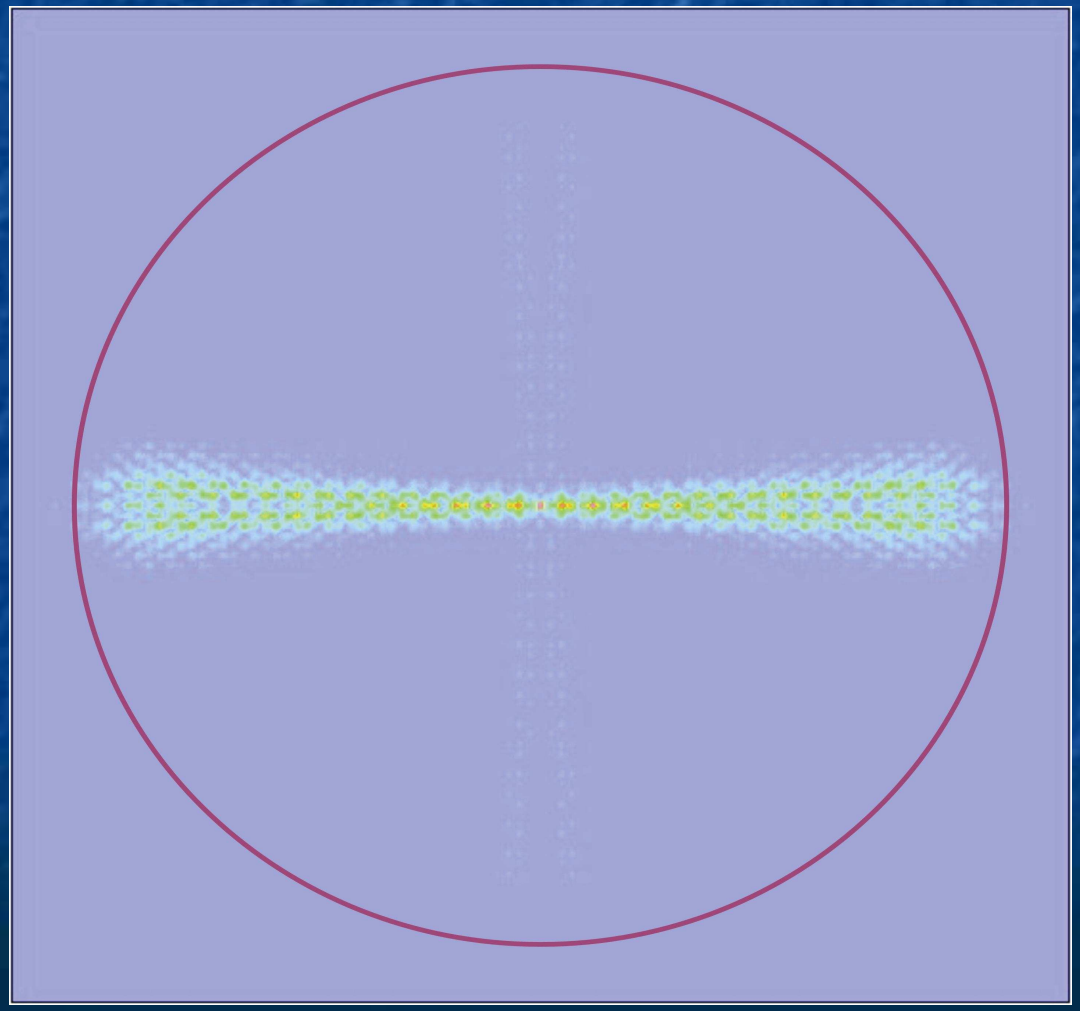


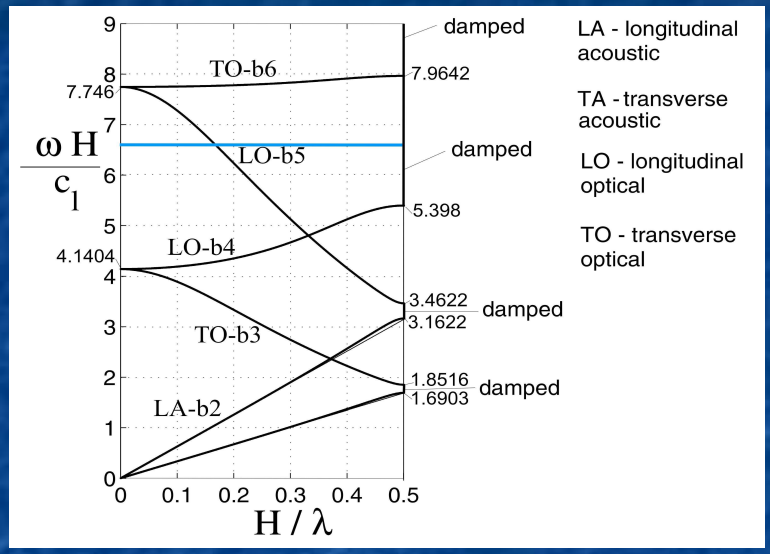


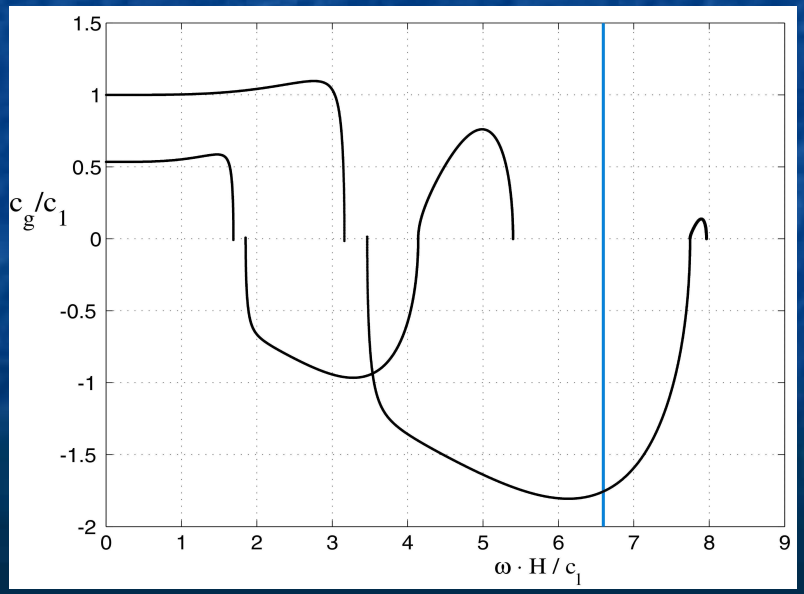


branch b5

$$\omega H / c_1 = 6.6$$

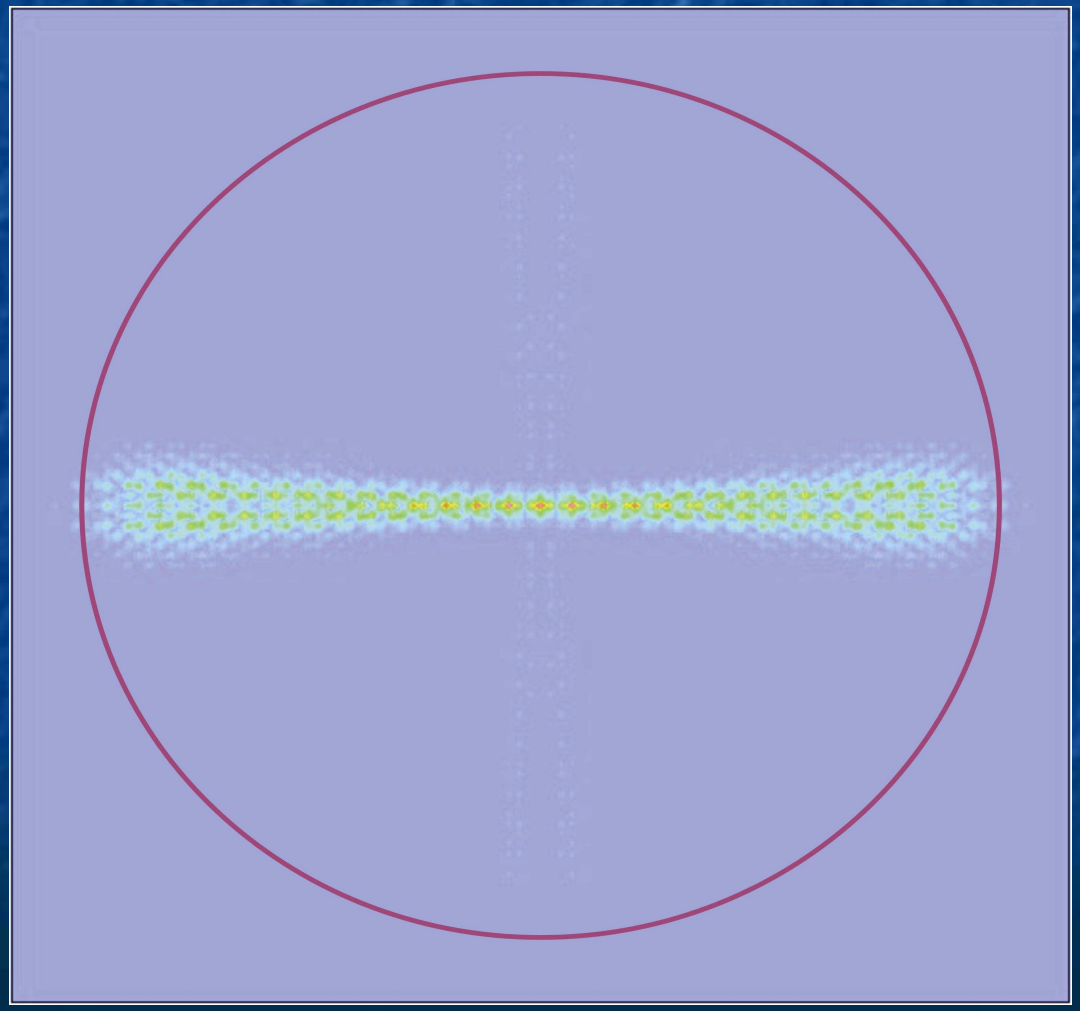


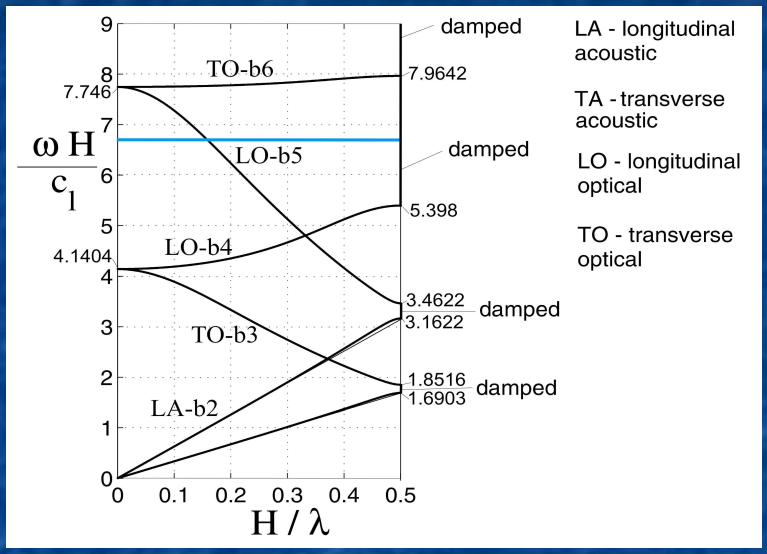


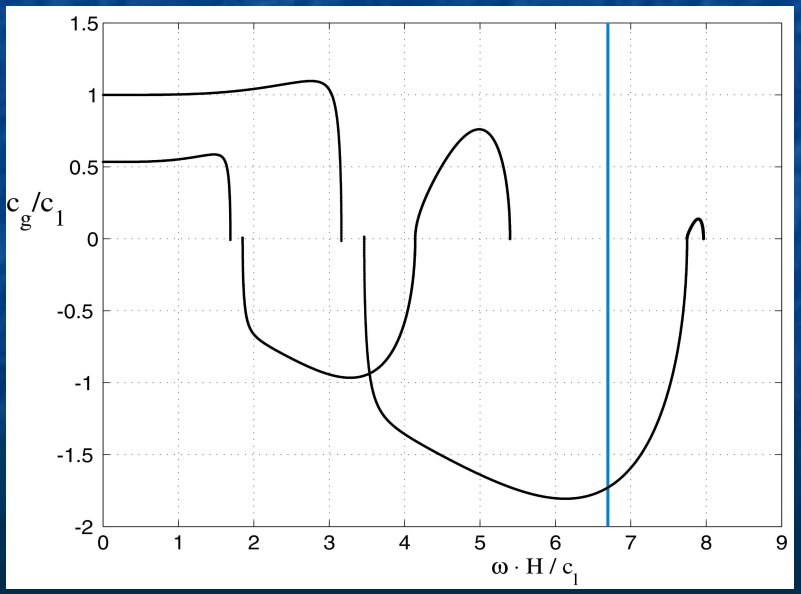


branch b5

$$\omega H / c_1 = 6.7$$

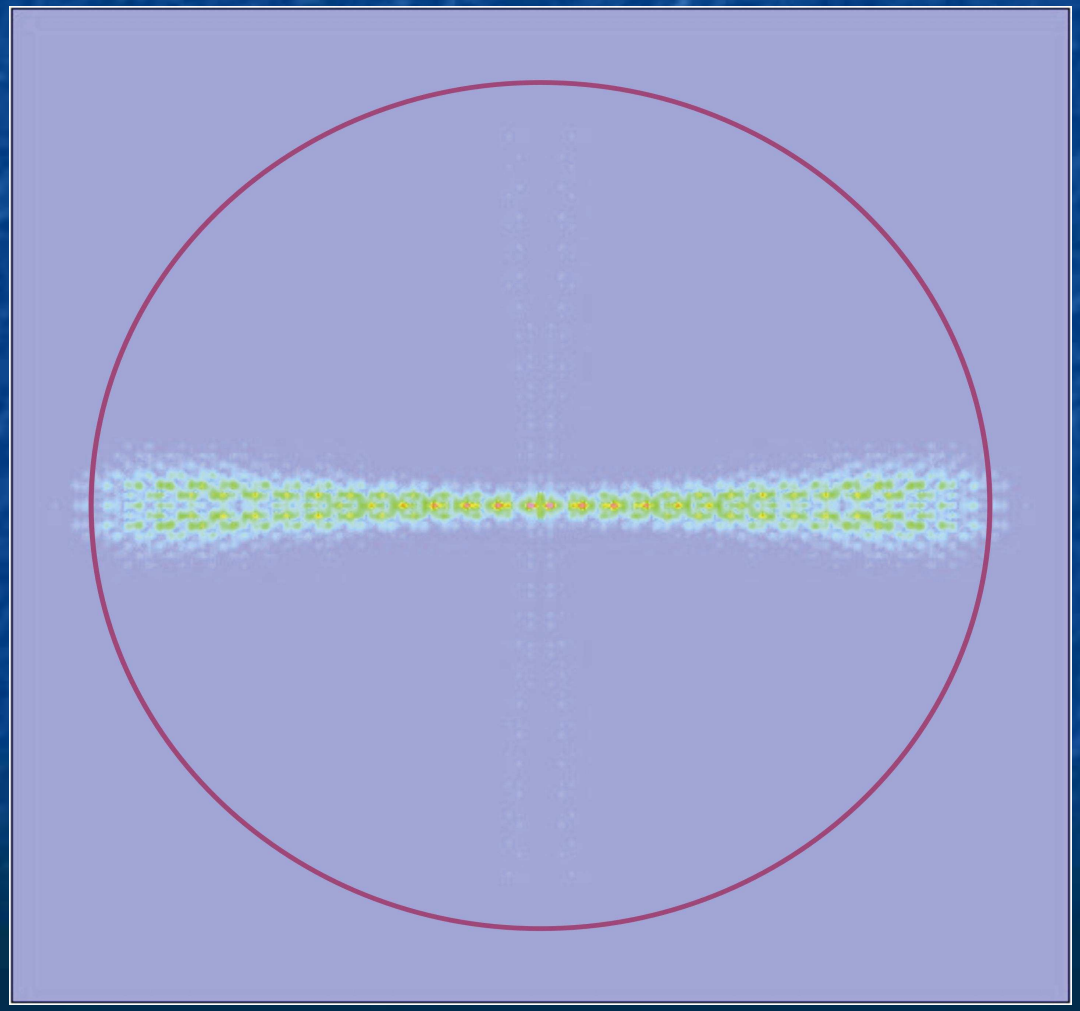


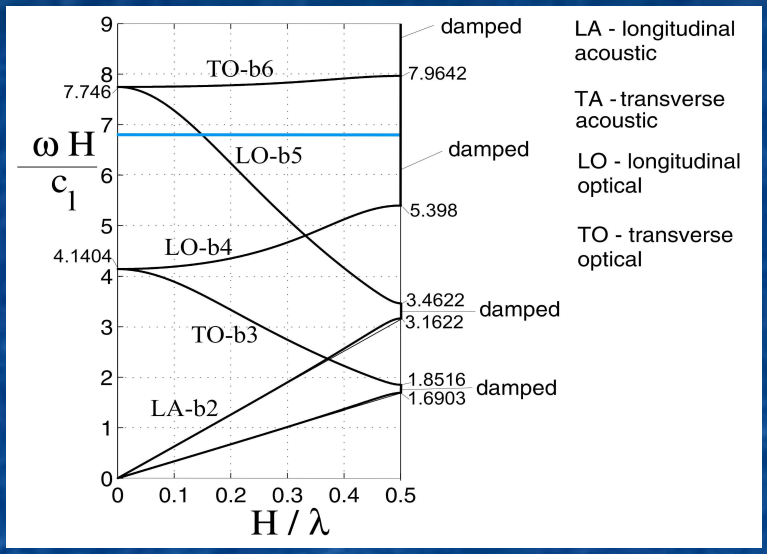


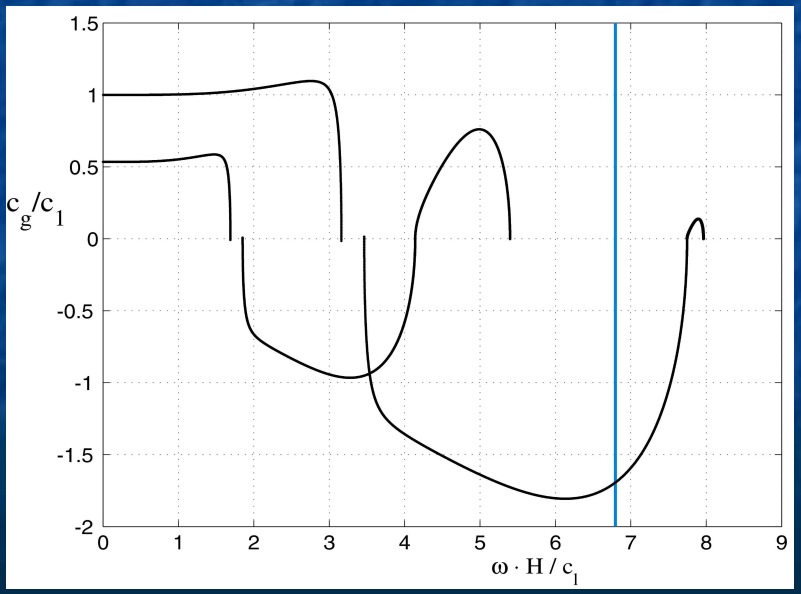


branch b5

$$\omega H / c_1 = 6.8$$

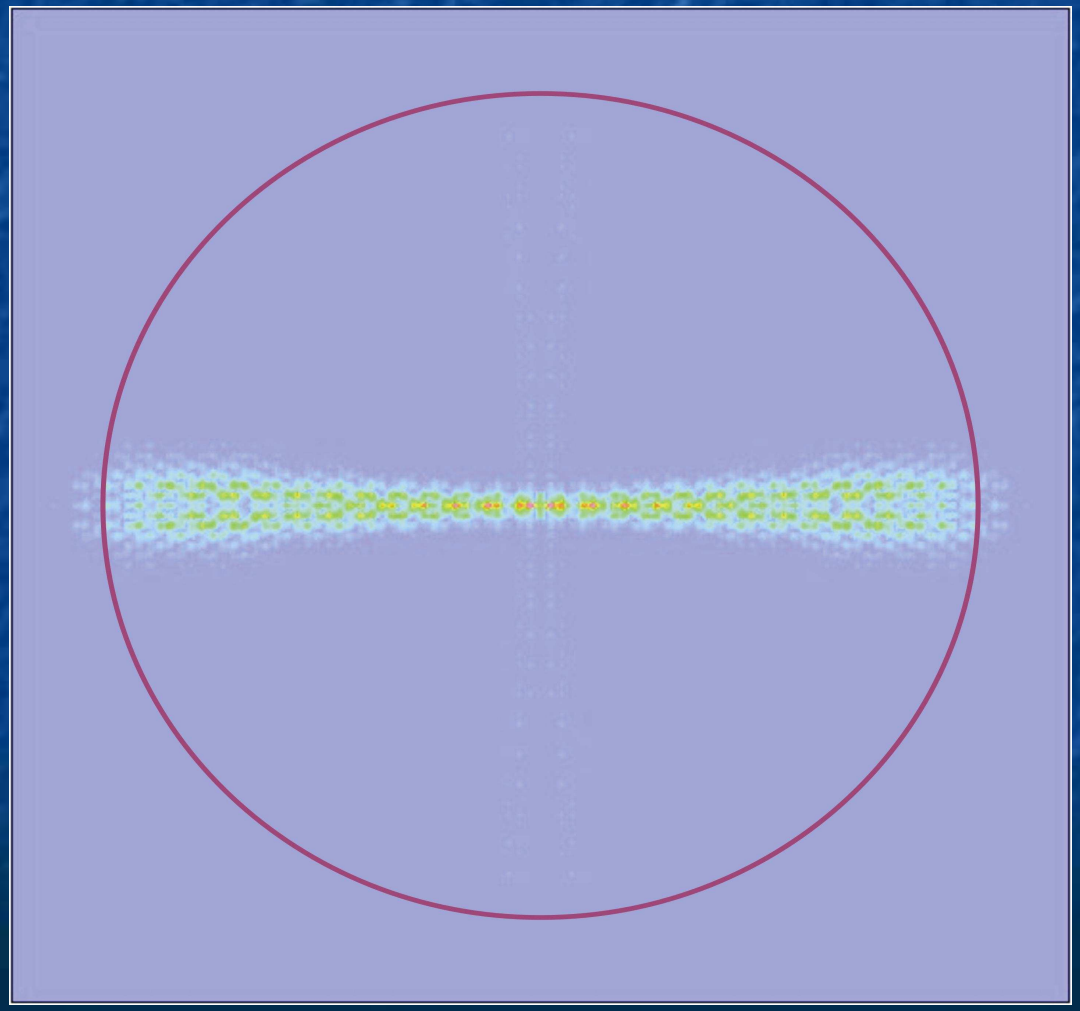


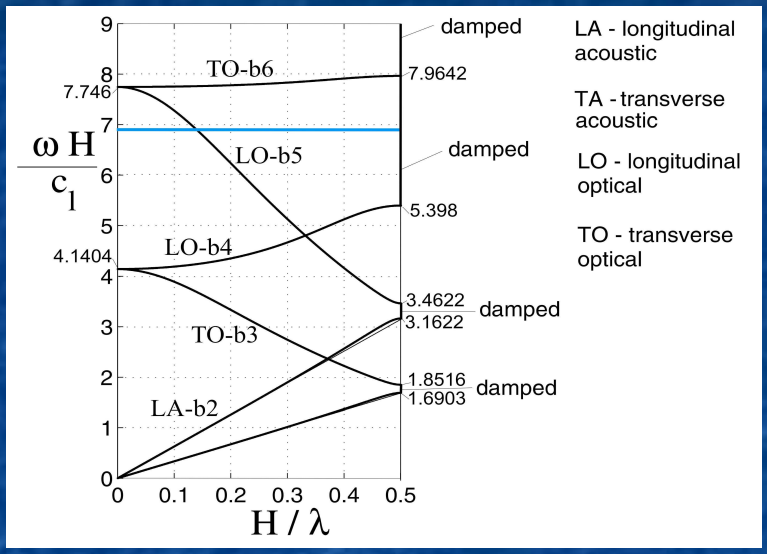


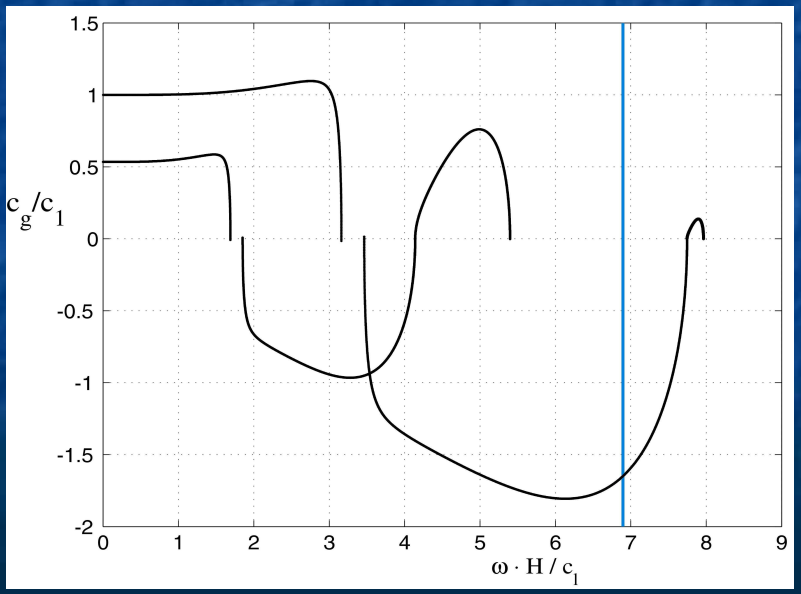


branch b5

$$\omega H / c_1 = 6.9$$

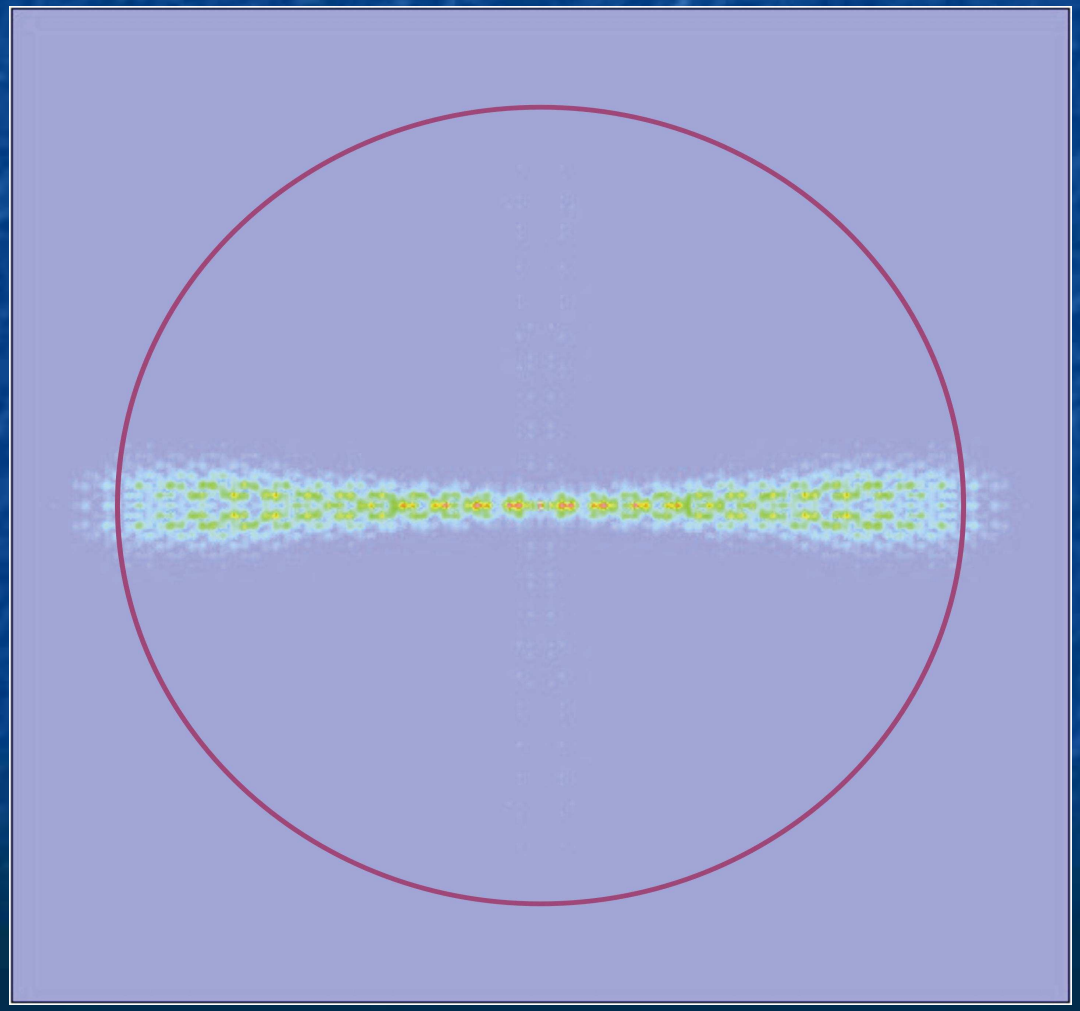


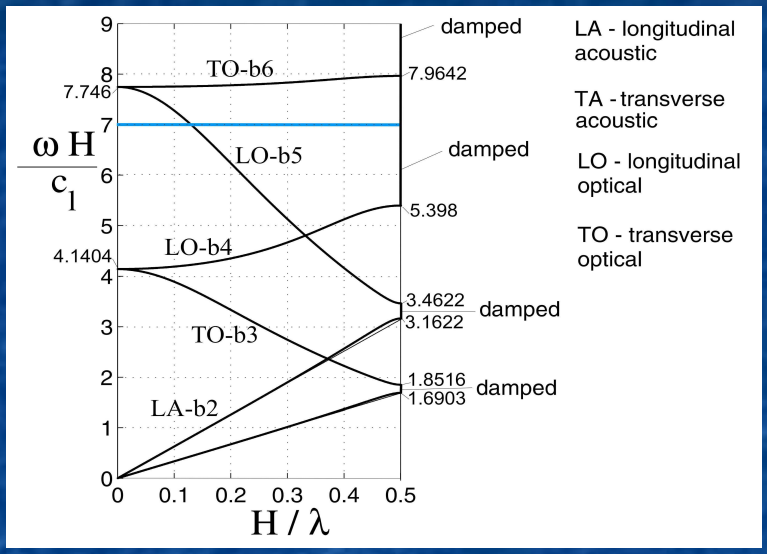


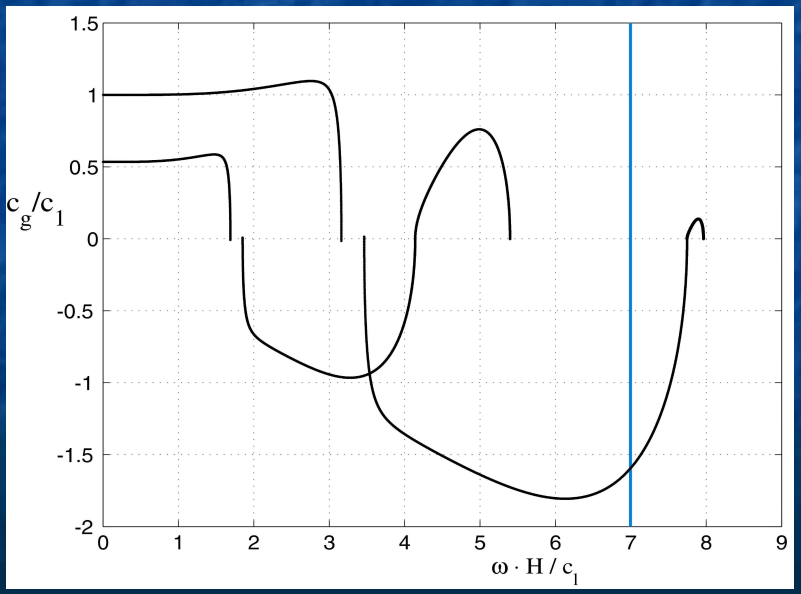


branch b5

$$\omega H / c_1 = 7.0$$

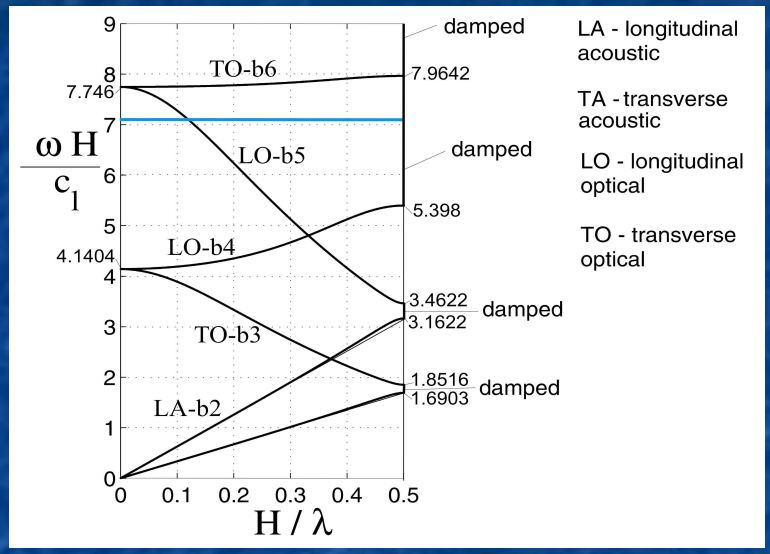


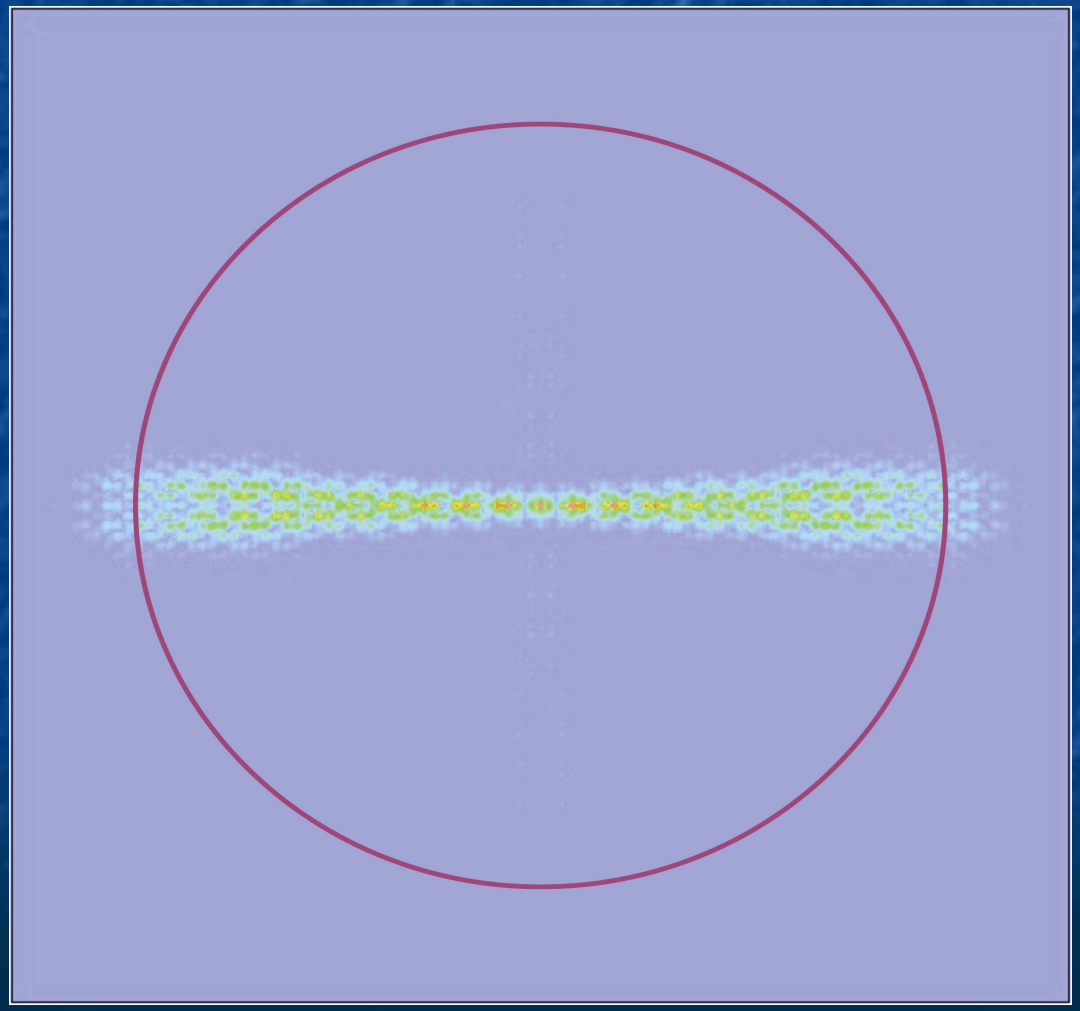


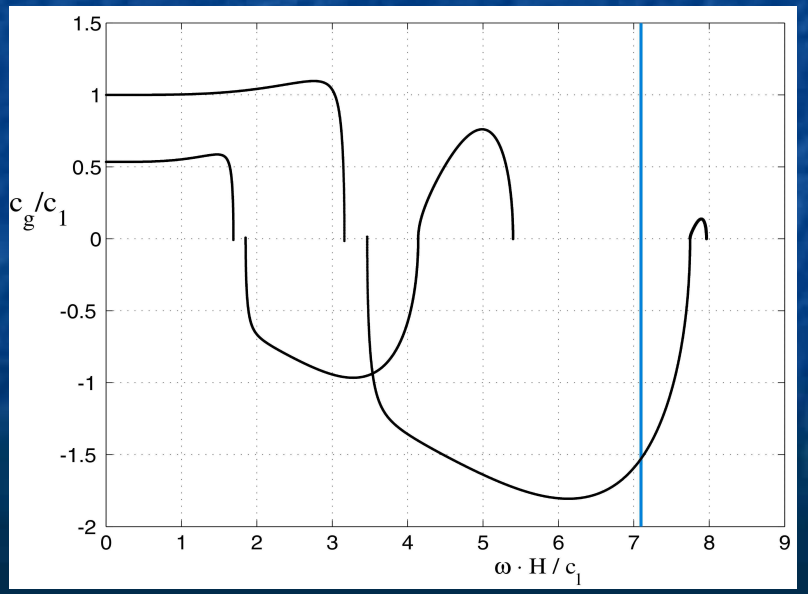


branch b5

$$\omega H / c_1 = 7.1$$

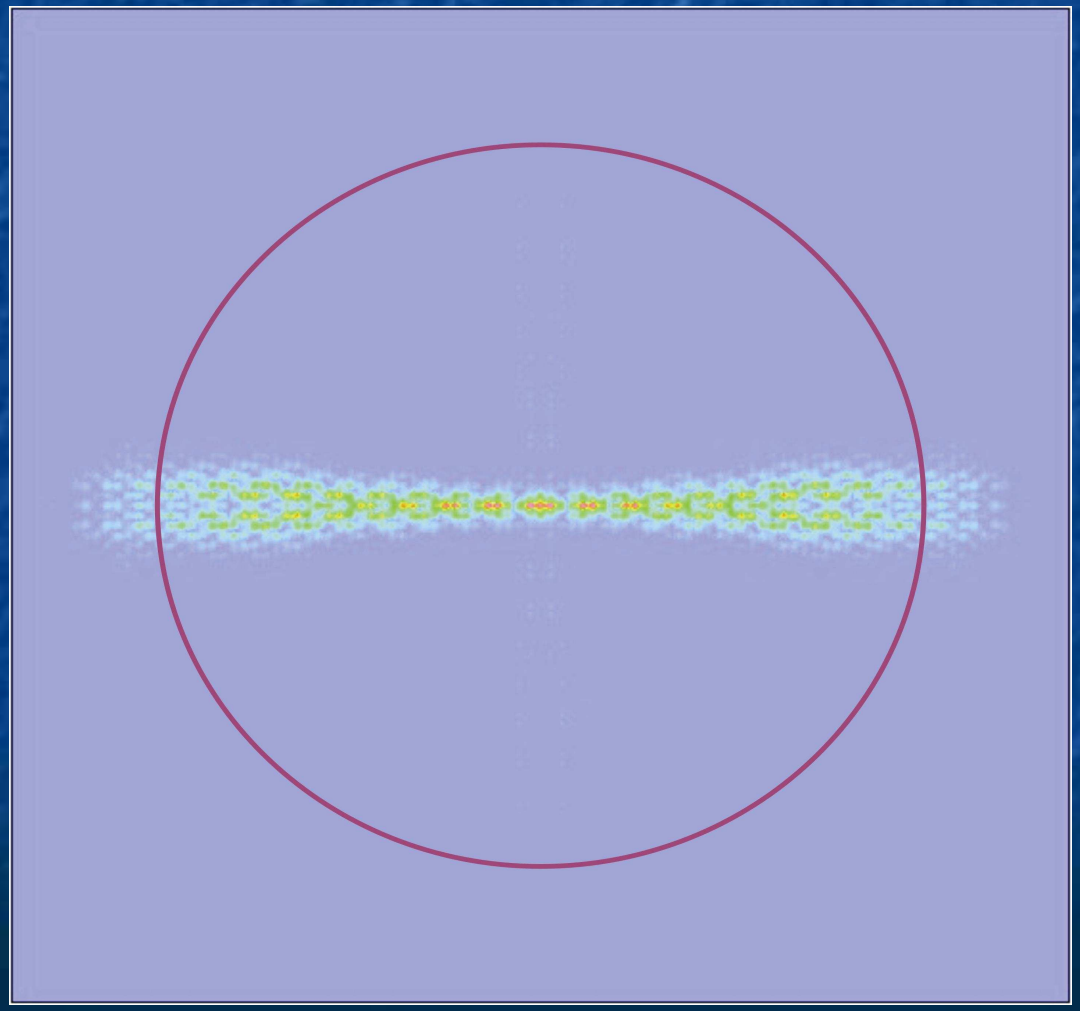


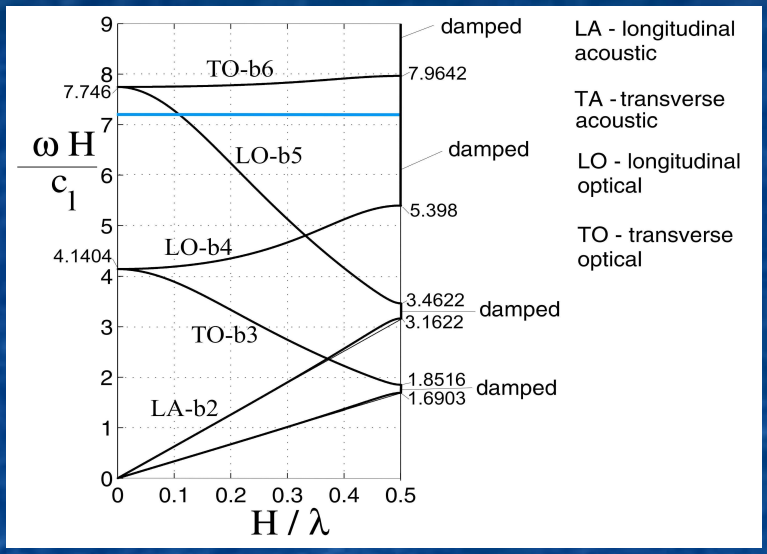


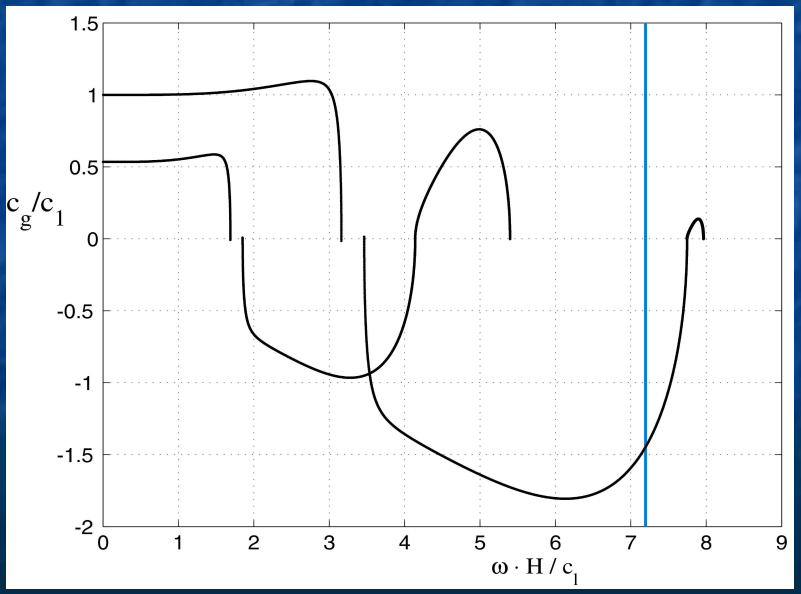


branch b5

$$\omega H / c_1 = 7.2$$

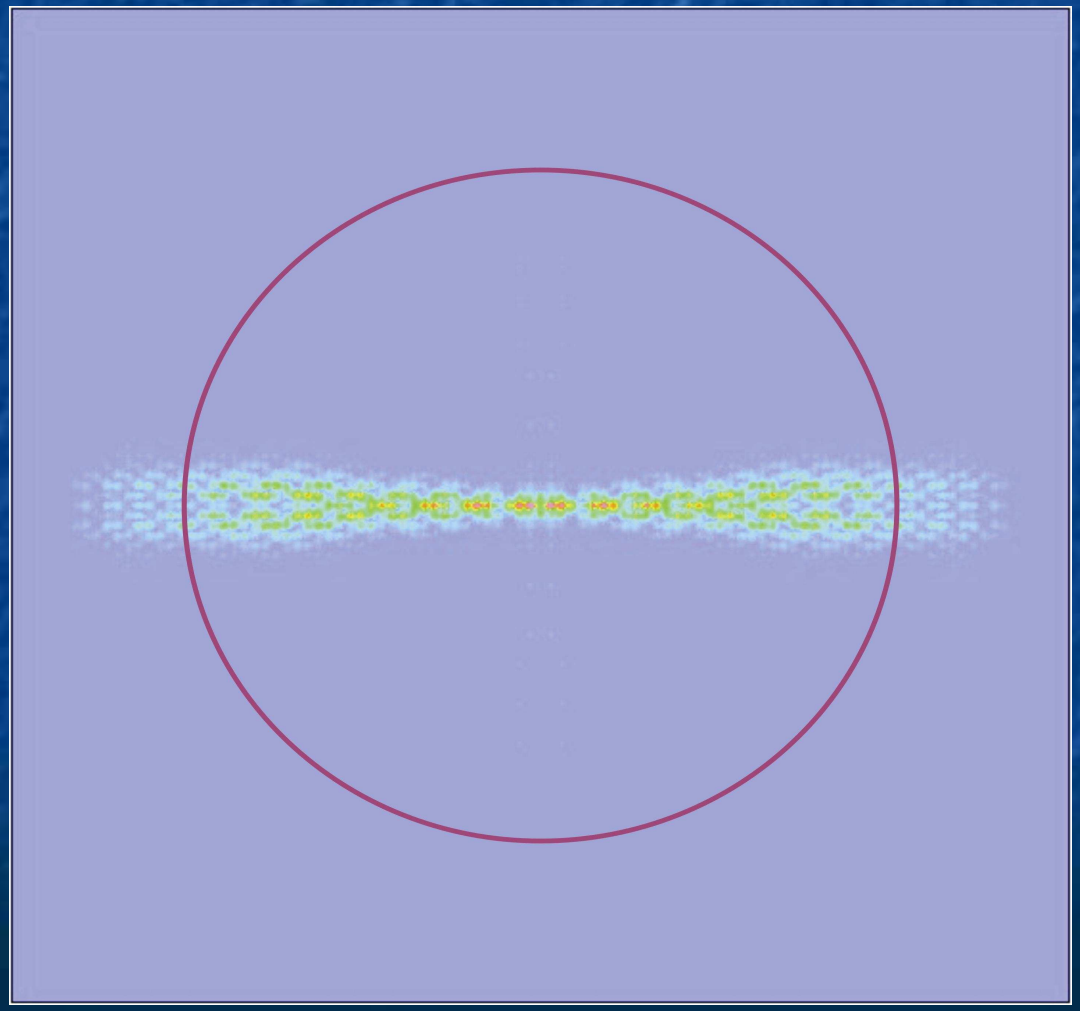


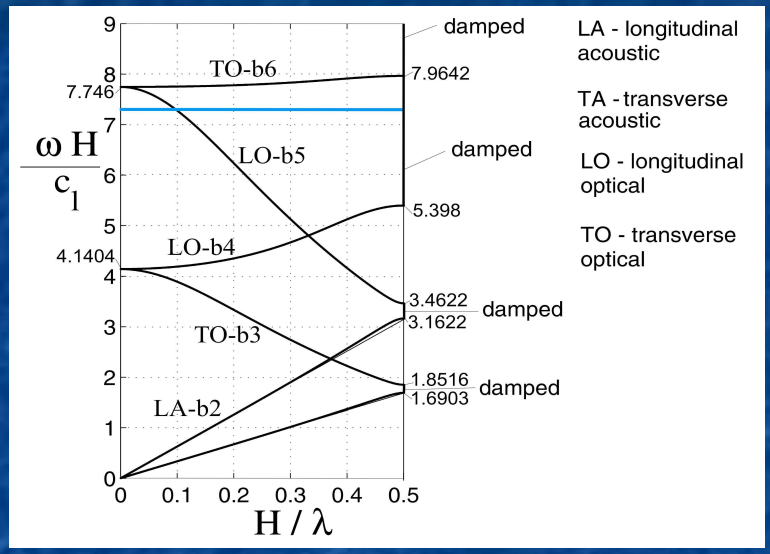


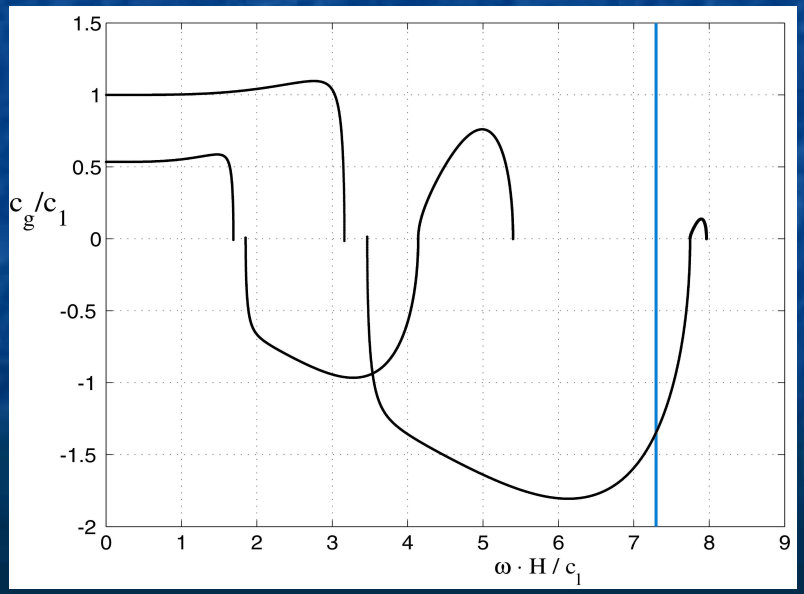


branch b5

$$\omega H / c_1 = 7.3$$

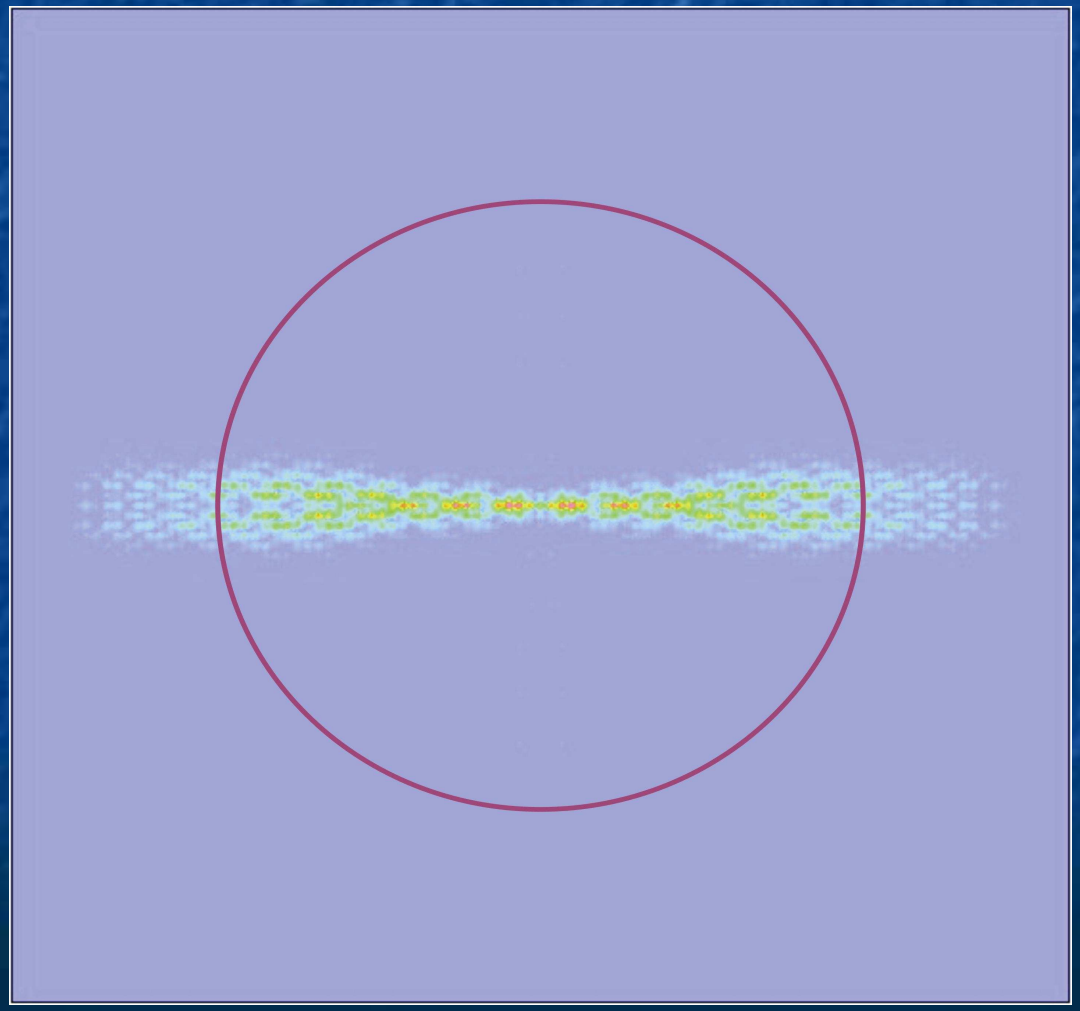


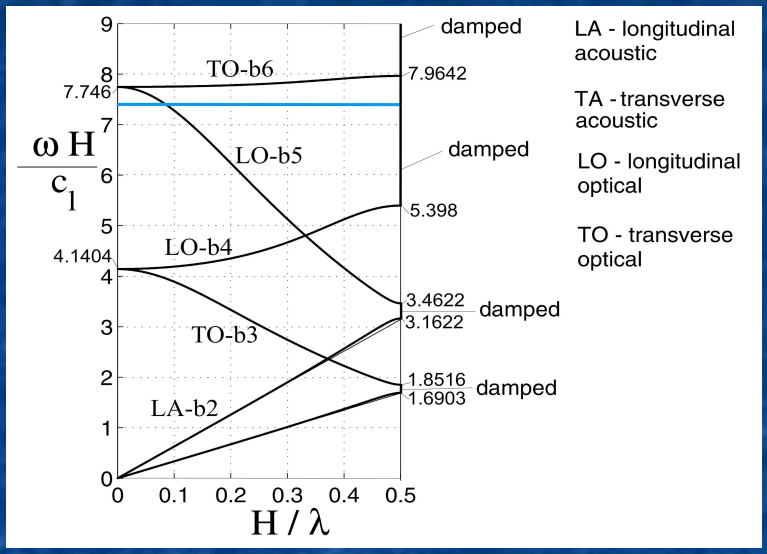


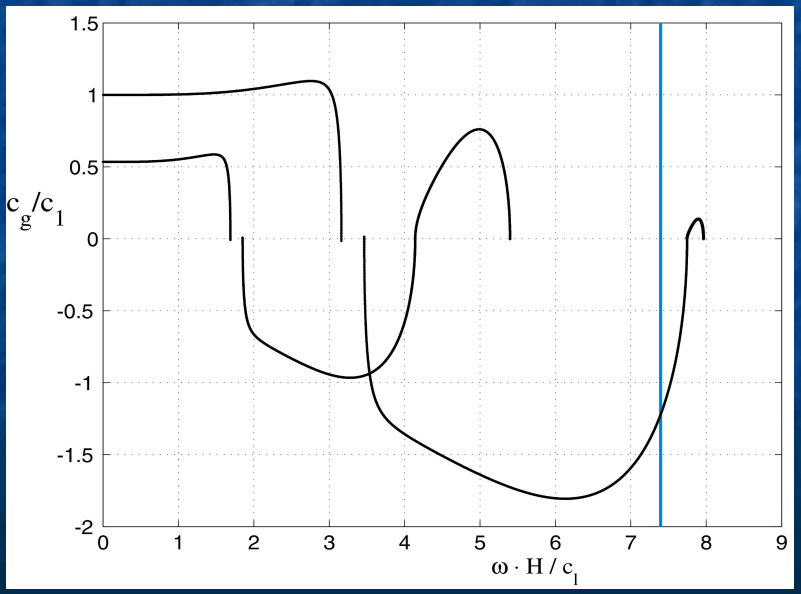


branch b5

$$\omega H / c_1 = 7.4$$

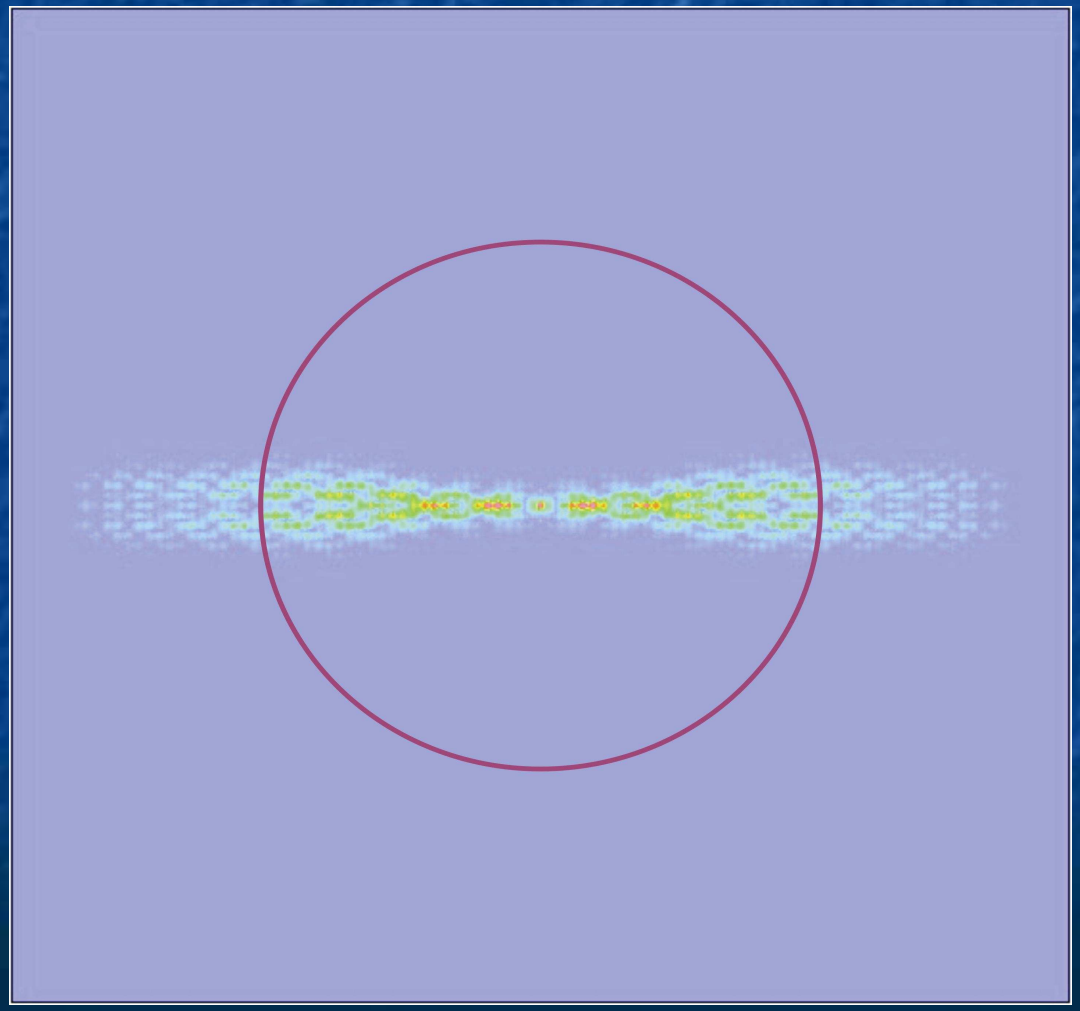


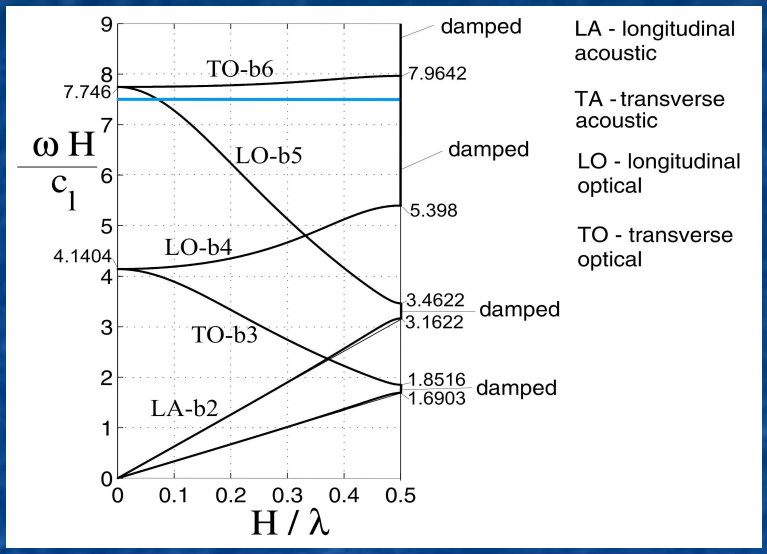


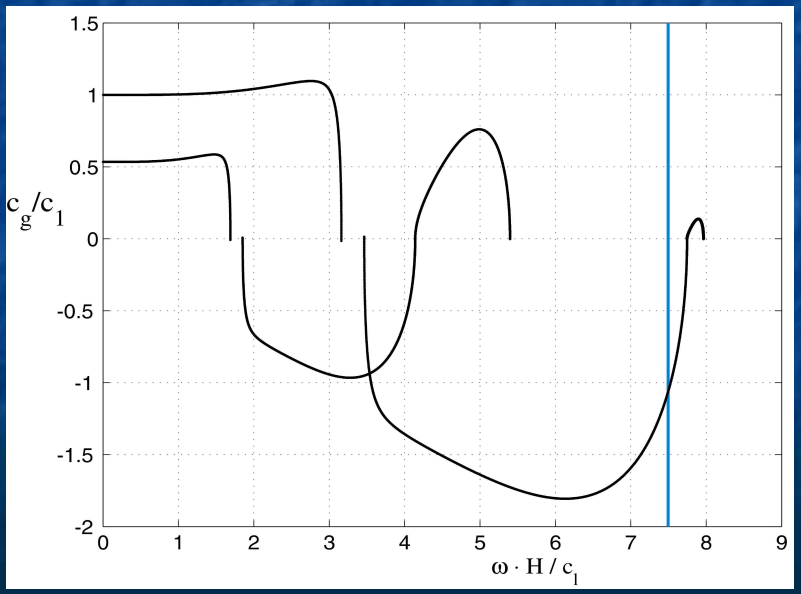


branch b5

$$\omega H / c_1 = 7.5$$

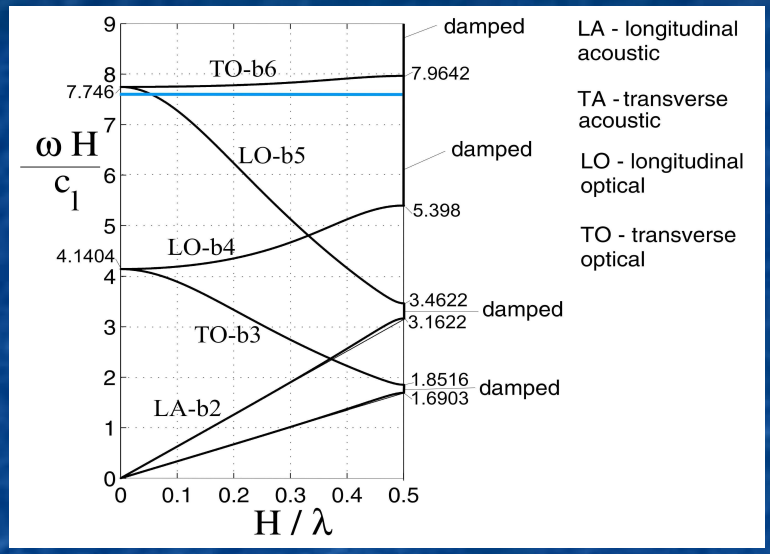


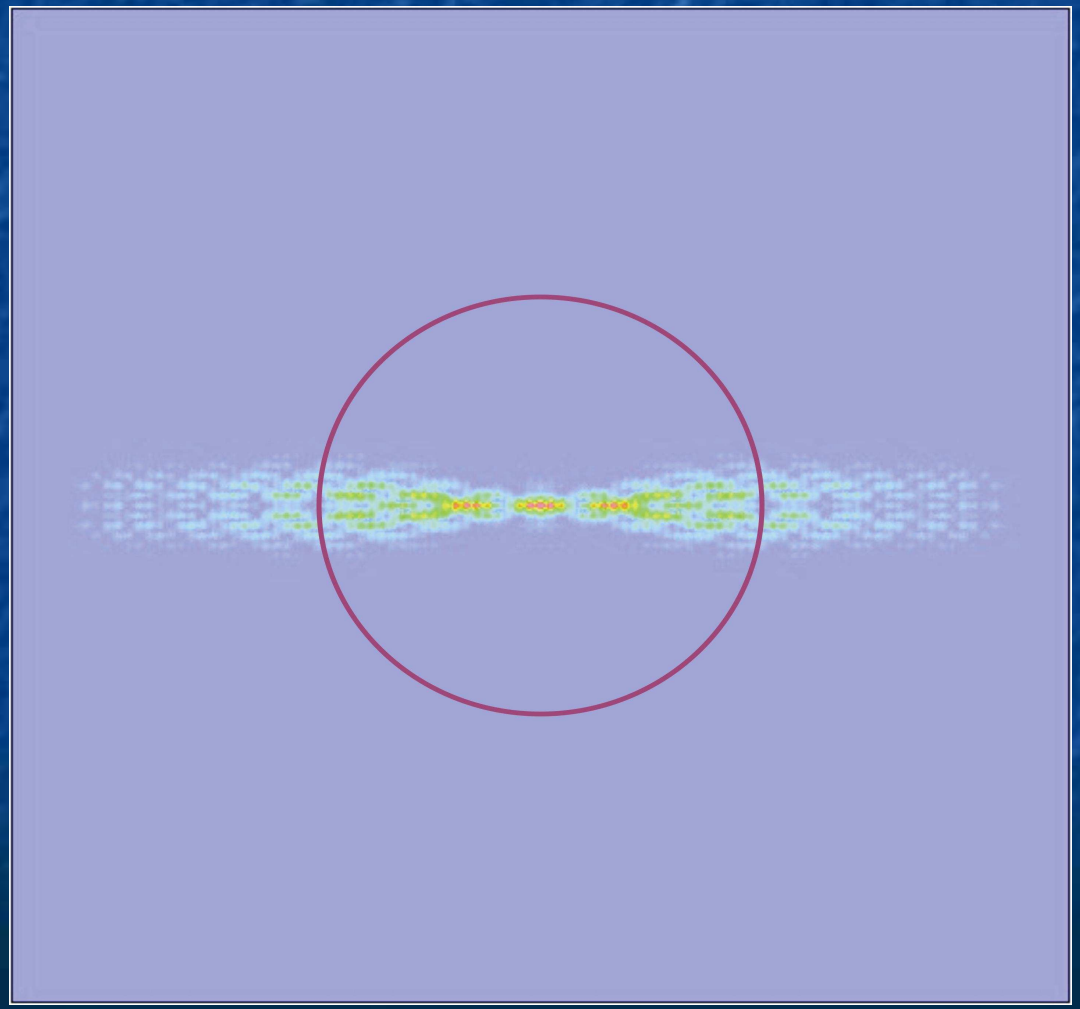


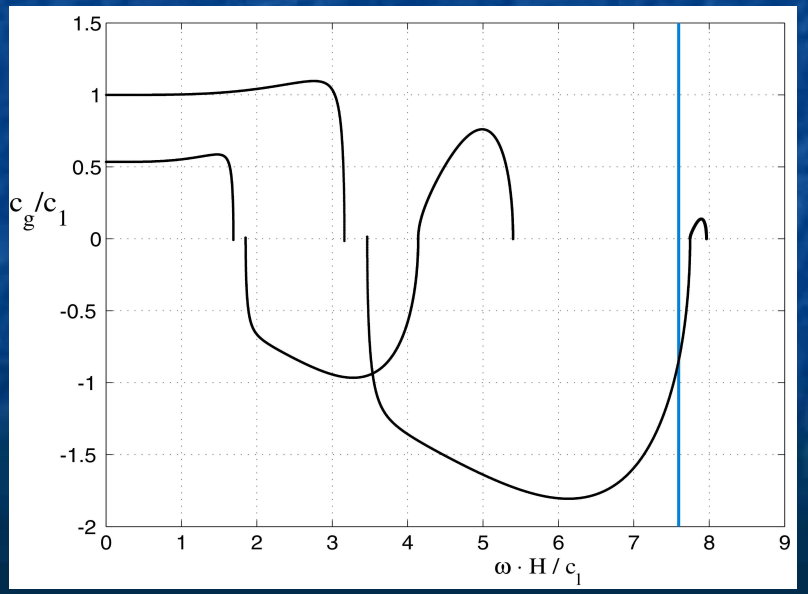


branch b5

$$\omega H / c_1 = 7.6$$

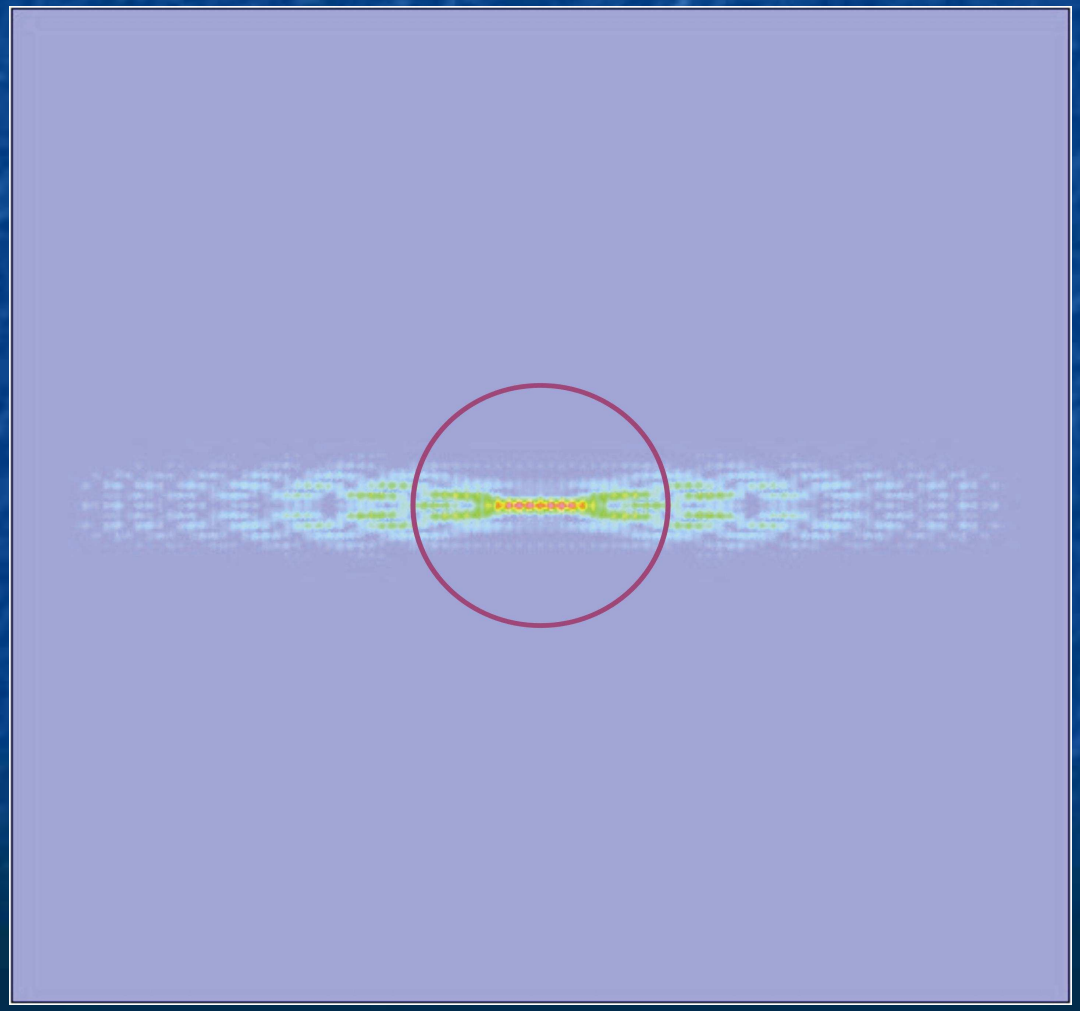


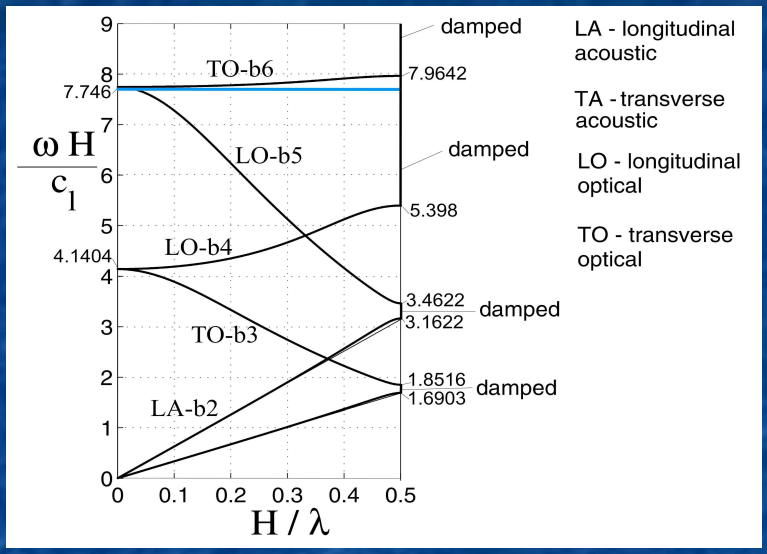


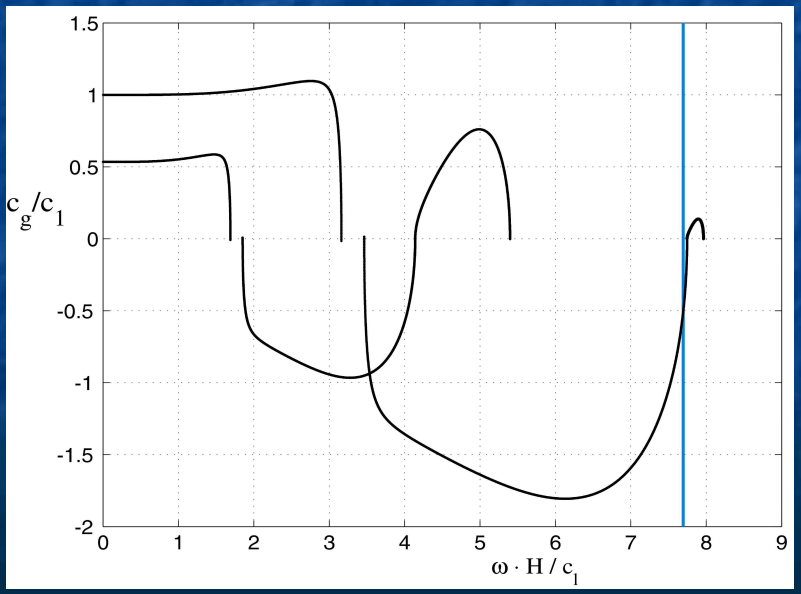


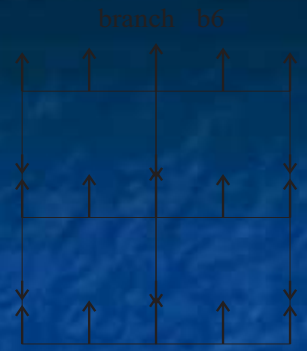
branch b5

$$\omega H / c_1 = 7.7$$

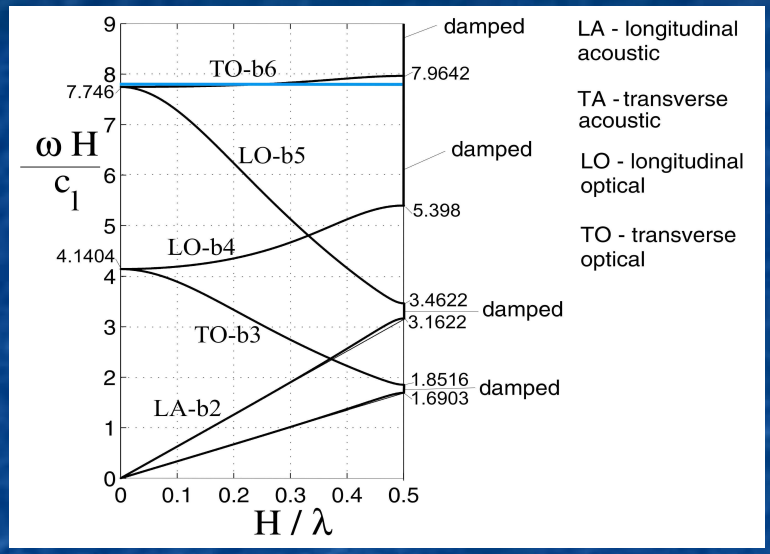


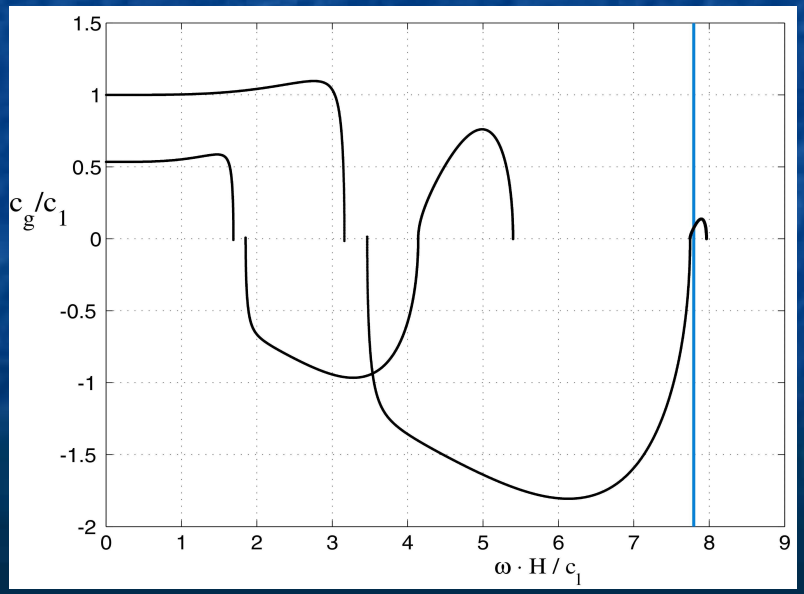


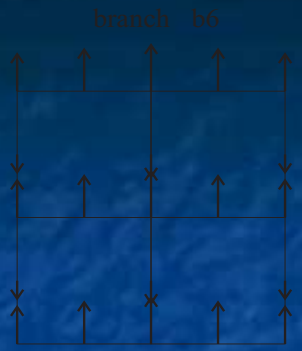



branch b6

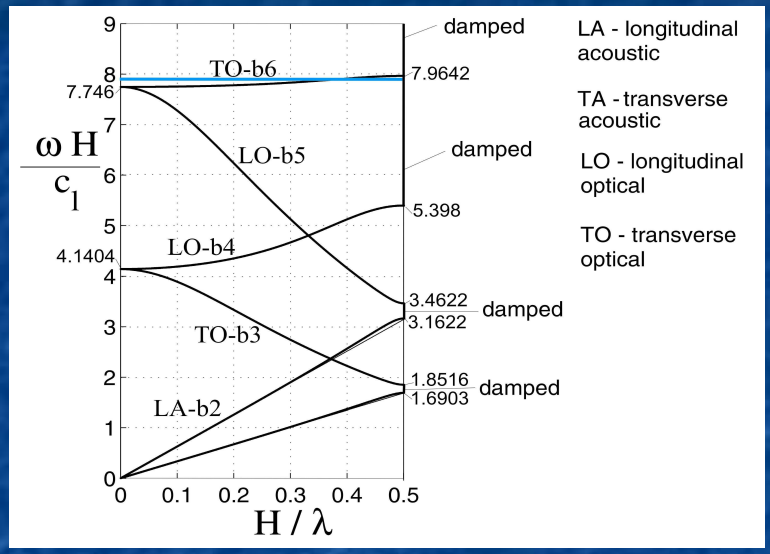
$$\omega H / c_1 = 7.8$$

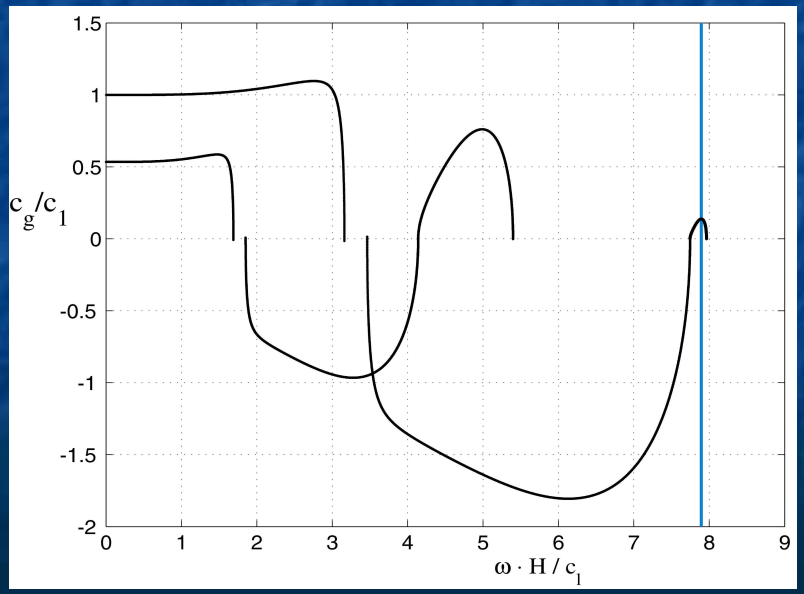

ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
7.9642
5.398
4.1404
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical


cg /c1
ω · H / c1

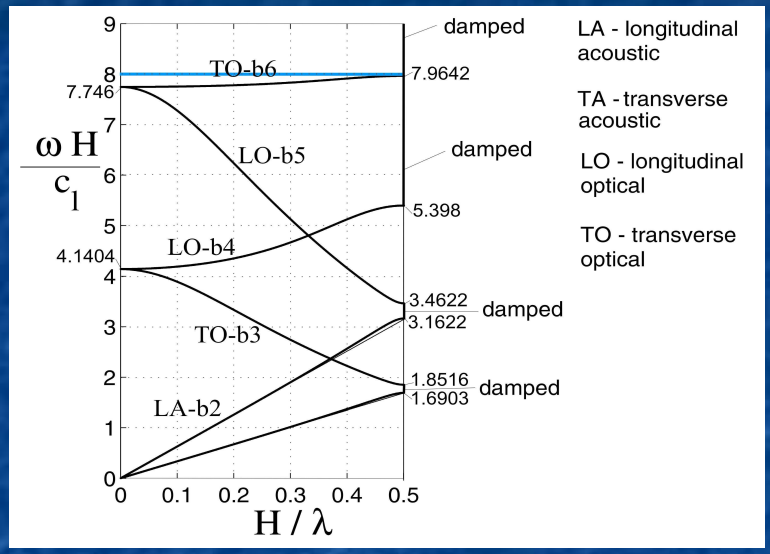

branch b6

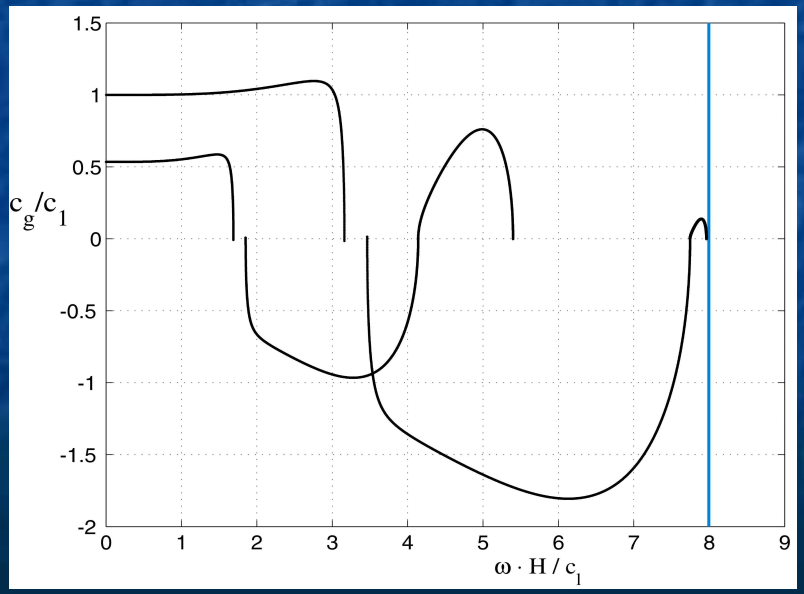
$$\omega H / c_1 = 7.9$$


ω H / c1
H / λ
TO-b6
LO-b5
LO-b4
TO-b3
LA-b2
7.746
4.1404
7.9642
5.398
3.4622
3.1622
1.8516
1.6903
damped
damped
damped
damped
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

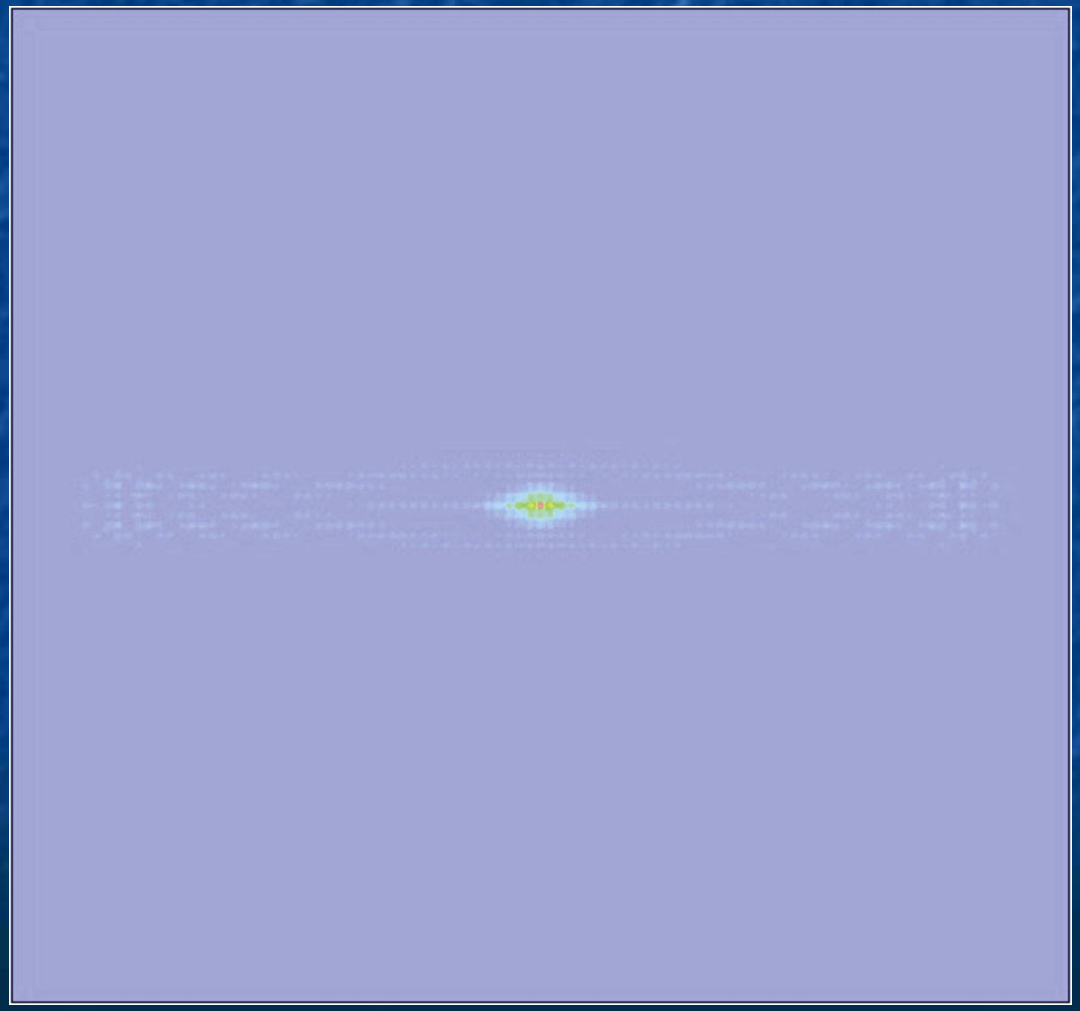

cg /c1
ω · H / c1

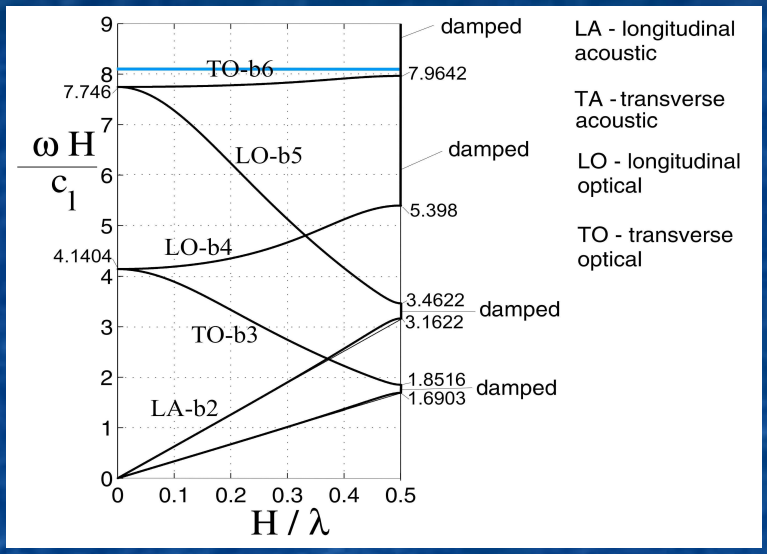
$$\omega H / c_1 = 8.0$$

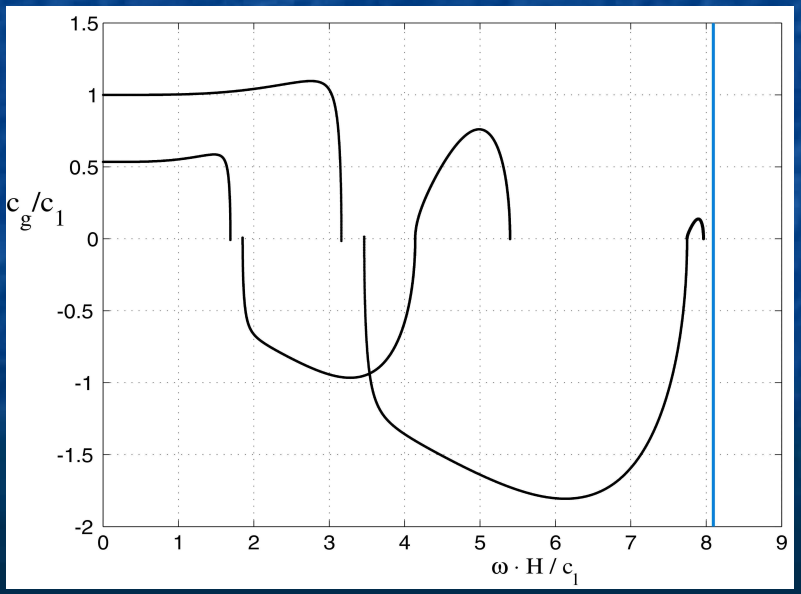

damped
TO-b6
7.9642
7.746
LO-b5
damped
5.398
LO-b4
4.1404
3.4622
3.1622
damped
TO-b3
1.8516
1.6903
damped
LA-b2
ω H / c1
H / λ
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical


cg/c1
ω · H / c1

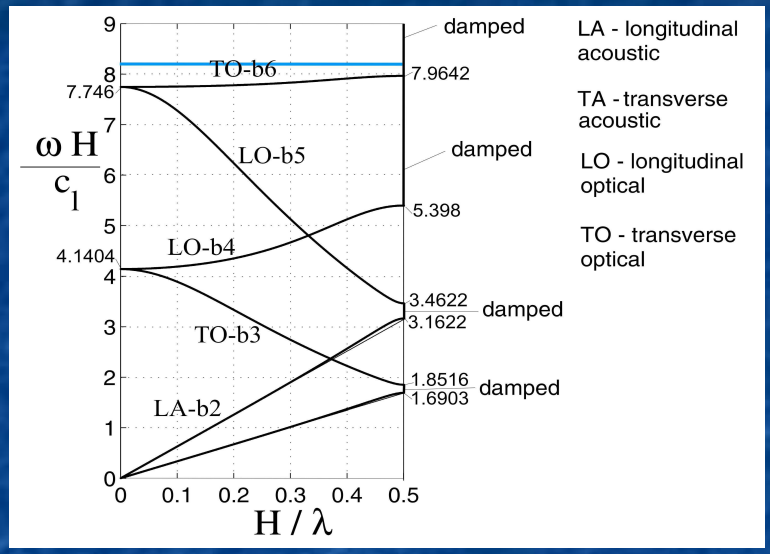
$$\omega H / c_1 = 8.1$$

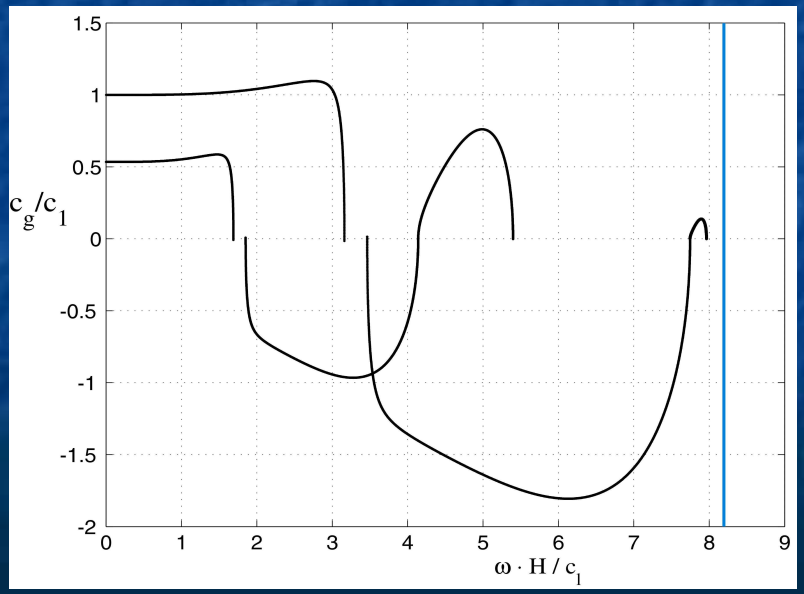



damped
TO-b6
7.9642
7.746
LO-b5
damped
5.398
LO-b4
4.1404
3.4622
3.1622
damped
TO-b3
1.8516
1.6903
damped
LA-b2
ω H / c1
H / λ
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical

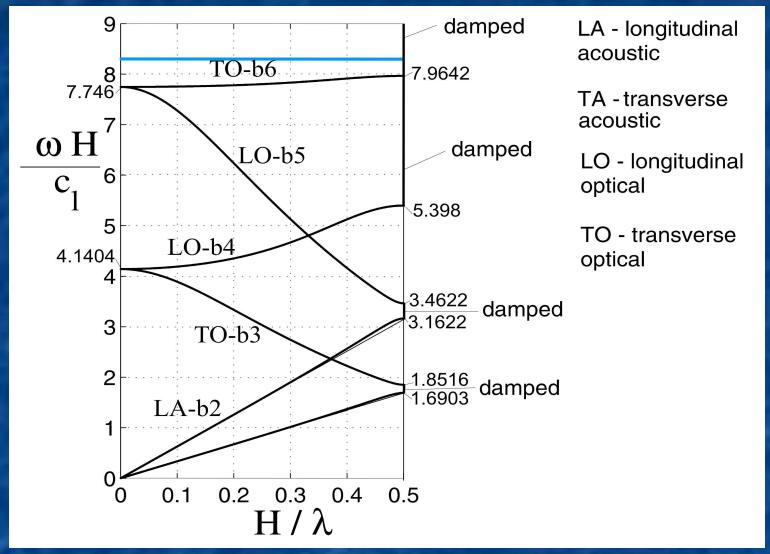

cg/c1
ω · H / c1

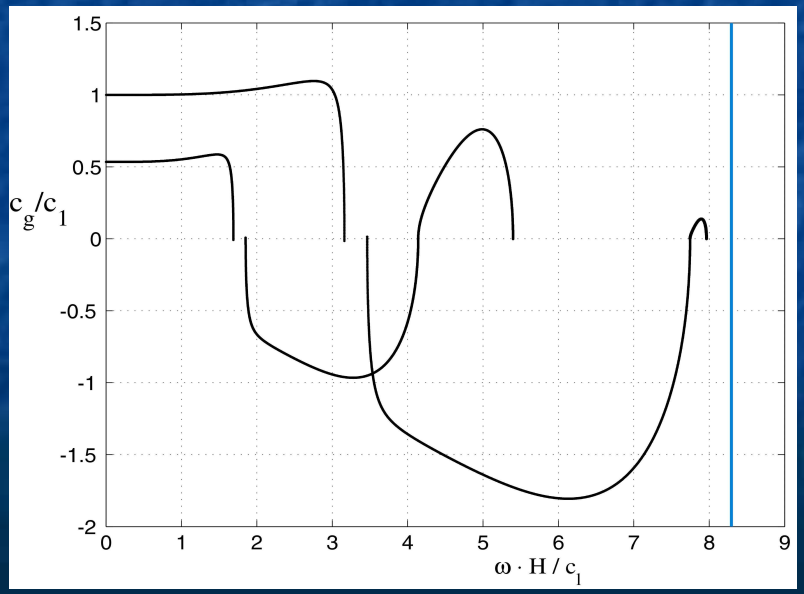
$$\omega H / c_1 = 8.2$$


damped
TO-b6
7.9642
7.746
LO-b5
damped
ω H / c1
5.398
LO-b4
4.1404
3.4622
damped
3.1622
TO-b3
1.8516
damped
1.6903
LA-b2
H / λ
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical


cg/c1
ω · H / c1

$$\omega H / c_1 = 8.3$$


damped
TO-b6
7.9642
7.746
LO-b5
damped
5.398
LO-b4
4.1404
3.4622
3.1622
damped
TO-b3
1.8516
1.6903
damped
LA-b2
ω H / c1
H / λ
LA - longitudinal acoustic
TA - transverse acoustic
LO - longitudinal optical
TO - transverse optical


cg /c1
ω · H / c1

Závěr

Na základě numerických testů odezvy rozlehlé stěny na proměnnou frekvenci buzení se podařilo ověřit platnost teoretických dispersních závislostí pro rovinné čtvercové kvadratické konečné prvky.

Děkuji za pozornost.

Tato práce byla podporována GA ČR 101/06/0914.