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Increasing Veno-arterial Extracorporeal Membrane Oxygenation Flow Reduces Electrical

Impedance of the Lung Regions in Porcine Acute Heart Failure

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Short title: VA ECMO Flow Reduces Electrical Impedance of Lungs

Summary

Veno-arterial extracorporeal membrane oxygenation (VA ECMO) is a technique used in patients with severe heart failure. The aim of this study was to evaluate its effects on left ventricular afterload and fluid accumulation in lungs with electrical impedance tomography (EIT). In eight swine, incremental increases of extracorporeal blood flow (EBF) were applied before and after the induction of ischemic heart failure. Hemodynamic parameters were continuously recorded and computational analysis of EIT was used to determine lung fluid accumulation. With an increase in EBF from 1 to 4 l/min in acute heart failure the associated increase of arterial pressure (raised by 44%) was accompanied with significant decrease of electrical impedance of lung regions. Increasing EBF in healthy circulation did not cause lung impedance changes. Our findings indicate that in severe heart failure EIT may reflect fluid accumulation in lungs due to increasing EBF.

Key words

Extracorporeal membrane oxygenation, Electrical impedance tomography, Pulmonary edema, Swine

Introduction

Veno-arterial extracorporeal membrane oxygenation (VA ECMO) is a lifesaving method used in patients with severe circulatory failure refractory to conventional management (Abrams et al. 2014, Makdisi and Wang 2015). It can substitute lungs and support circulation since it enables blood gas exchange (oxygenation and carbon dioxide extraction), improves tissue perfusion (Hala et al. 2016, Lequier et al. 2017), and serves as a bridge of the critical period (Ostadal et al. 2018). Blood is bypassed from the native circulation through percutaneous venous cannula to the gas exchange unit and after being oxygenated, it is returned into the descending aorta. Blood from VA ECMO is thus mixed with the blood pumped by the left ventricle (LV). Recent papers have discussed the negative effects of increased afterload on the LV function (Fuhrman et al. 1999, Soleimani and Pae 2012, Ostadal et al. 2015, Brechot et al. 2017, Donker et al. 2019, Hála et al. 2020), which may lead to LV distension, a rise in the end-diastolic volume, end-systolic volume, end-diastolic pressure, and in left atrial pressure. Progression into pulmonary edema may consequently occur (Fuhrman et al. 1999, Burkhoff et al. 2015, Ostadal et al. 2015, Ostadal et al. 2018, Donker et al. 2019). Furthermore, clinical work by Kim et al. (2018) recently described how excessive cumulative fluid balance during early phases of ECMO increases the risk of mortality.

Pulmonary edema is a serious complication of VA ECMO, especially in patients with severely impaired left ventricular function. Therefore, it often requires urgent intervention (Fuhrman *et al.* 1999, Brechot *et al.* 2017, Donker *et al.* 2019). Currently, standard diagnostic procedures to detect pulmonary edema are based on clinical examination, lung ultrasound, echocardiography, chest radiography, and hemodynamics assessment. However, these methods are lacking the sensitivity to quantify fluid volumes (Cardinale *et al.* 2014) and may require repeated evaluations. Real-time diagnostic methods (e.g. transpulmonary thermodilution) are also available, however, requiring additional invasive procedure and lacking high sensitivity (Sobota *et al.* 2019).

Electrical impedance tomography (EIT) is a bedside, non-invasive, radiation-free, and realtime imaging technique based on the assessment of tissue resistivity. This is best represented by the physical quantity called impedance, obtained by probing the tissue with skin electrodes injecting a weak alternating current (excitation frequency ranges from tens to hundreds of kHz). Currently, it is being used for bedside monitoring of regional lung ventilation and the distribution of air within the lungs, especially in patients with acute lung injury and acute respiratory distress syndrome (Frerichs et al. 2017, Bachmann et al. 2018). Due to the air space in the alveoli, native resistivity of lung tissue is high and electrical impedance varies considerably with breathing cycles reaching peak values during inspiration. Conversely, impedance of plasma is low and therefore increased volume of fluid in lungs has a considerable effect on decreasing tissue electrical impedance. Sobota et al. (2019) and Becher et al. (2019) recently demonstrated in both animal experiments and clinical practice that intravenous administration of fluids has a significant effect on the lung impedance. Therefore, EIT can serve as a suitable method for bedside evaluation of small fluid changes in the lungs (Adler et al. 1997, Noble et al. 2000). Moreover, the diagnostic potential of EIT can be further increased using advanced signal analysis, which allows for the evaluation of the regional perfusion and heart work (Borges et al. 2012, Reinius et al. 2015).

The purpose of this pilot study was to evaluate the acute fluid changes in the lungs during VA ECMO support. Lung impedance changes were registered during incremental increases in VA

ECMO blood flow under both healthy and failing heart conditions. We present a new, computational analysis of the raw EIT data which detects minor changes in fluid content specifically within the lung tissue.

Methods

Experimental protocol was reviewed and approved by the Institutional Animal Expert Committee of the Fist Faculty of Medicine, Charles University and was performed at the University experimental laboratory, Department of Physiology, First Faculty of Medicine, Charles University, Prague, Czech Republic, in accordance with Act No 246/1992 Coll. on the protection of animals against cruelty. All animals were treated and cared in accordance with the European Guidelines on Laboratory Animal Care.

Animal model

Eight healthy female pigs (*Sus scrofa domestica*), weight 57 ± 2 kg, were included in this study. After 12 hours of fasting, animals were premedicated with midazolam (0.2-0.4 mg/kg IM) and ketamine (15-25 mg/kg IM), then margin ear vein access was secured, and induction of anesthesia was achieved by intravenous application of propofol (2 mg/kg IV). The animals were positioned into the dorsal recumbency before the endotracheal intubation was performed (tube 7-8 mm). Mechanical ventilation was operated by Hamilton G5 ventilator (Hamilton Medical AG, Switzerland), set to volume control ventilation described in more detail in the ECMO protocol section. The position of animals was stable during the whole experiment.

Total intravenous anesthesia was maintained during the experiment. Propofol (6-10 mg/kg/h) and midazolam (0.1-0.2 mg/kg/h) were combined with opiate analgesia (morphine 0.1-0.3 mg/kg/h), and the depth of anesthesia was confirmed by controlling reflexes, muscle tone, and cardiovascular reactions. Continual infusions of heparin (50-80 UI/kg/h) was set to prevent thrombosis. Infusion of Ringer's solution and 0.9% saline was kept within range 5-10 ml/kg/h to maintain central venous pressure (CVP) around 5 mmHg before the ECMO implantation. Foley catheter was inserted through the urethra to the urinary bladder to monitor urine production.

Experimental preparation and monitoring

A triple lumen central venous catheter was placed percutaneously through the external jugular vein for CVP monitoring, as well as for fluid and anesthetics administration. The femoral artery was cannulated to measure systemic blood pressure. A balloon Swan-Ganz catheter was inserted into the pulmonary artery via the femoral vein to simultaneously record pulmonary artery pressure, mixed venous oxygen saturation (SvO₂), and cardiac output (CCO Combo Catheter, Vigilance II, Edwards Lifesciences, USA), whereas pulmonary capillary wedge pressure (PCWP) was measured upon completion of each ECMO flow step. The right carotid artery was surgically exposed, and an ultrasound flow probe was placed around the vessel (4PSB or 6PSB, Science, Transonic Systems, USA) to continuously measure the blood flow. Regional tissue oxygenation (rSO₂) was monitored by near-infrared spectroscopy (INVOS Oximeter, Medtronic, USA) with sensors placed on forehead and right forelimb, to evaluate head and peripheral tissue oxygen saturation.

Electrical impedance tomography

Swisstom EIT-Pioneer set (Swisstom, AG, Switzerland) was used to measure the electrical impedance tomography of the thorax. The sensor belt, fitted with 32 evenly distributed electrodes, was placed around the circumference of the thorax and its position was verified by X-ray to ensure its proper position above diaphragm around both lungs and heart. Alternating electrical current of single frequency (3 mA, 200 kHz) was applied through pairs of electrodes and corresponding voltages were measured on the remaining electrodes. The pattern of the injecting and sensing electrodes was rearranged automatically, achieving apparent rotatory movement of probing electrodes around the chest, resembling the way the computed tomography image is obtained. This allows for the real-time (update rate 50 Hz) reconstruction of the tissue impedance, generating a 64x64 pixel matrix every 20 ms, and so creating a dynamic 2D image of the thoracic tomographic plane.

Veno-arterial extracorporeal membrane oxygenation

Extracorporeal membrane oxygenation in veno-arterial setting (VA ECMO) was used. The dosage of heparin was set to keep activated clotting time at 200-300 s. ECMO cannulas were introduced by Seldinger technic through punctures of the unilateral femoral vein and artery. The tip of the inflow venous cannula (21 Fr) was placed near the right atrium and the arterial outflow cannula (15 Fr) was placed in the descending aorta. The position of both cannulas was verified by fluoroscopy. Extracorporeal blood flow (EBF) was measured by the flow probe (ME 9PXL, Transonic, USA) attached to the outflow cannula. Blood gas parameters were monitored continuously in the blood leaving the oxygenator (CDI TM Blood Parameter Monitoring System 500, Terumo Cardiovascular System Corporation, USA). The oxygen and air flow were adjusted to maintain arterial pO₂ at 150-200 mmHg and pCO₂ at 35-45 mmHg.

ECMO protocol

After the introduction of VA ECMO, the defined protocol (Figure 1) with increasing EBF was applied to healthy cardiovascular system (before the induction of HF). Lung-protective ventilation was set to volume control: tidal volume (V_T) 6-7 ml/kg, positive end-expiratory pressure (PEEP) 5-6 cmH₂O, PIP < 25 cmH₂O, fraction of inspired oxygen (FiO₂) 30%. V_T and PEEP were kept constant during the protocol and the respiratory rate was adjusted to maintain end-tidal CO₂ (etCO₂) 35-45 mmHg. Administration of intravenous infusions was constant throughout the protocol (5-6 ml/kg/h). VA ECMO flow was increased stepwise with 20 ml/kg/min increments, starting at 20 ml/kg/min (referred to as EBF 1 l/min) and reaching up to 80 ml/kg/min (EBF 4 l/min). Each step lasted 8-12 minutes. At the end of each step lung impedance and hemodynamic parameters were obtained by averaging end-expiratory values during 30 s.

Heart failure

A model of acute HF was used in our experiment. Based on previous publications (Suzuki *et al.* 2008, Ishikawa *et al.* 2014, Li *et al.* 2014) and our own experience (Ostadal *et al.* 2016, Janak *et al.* 2017, Hala *et al.* 2018, Lacko *et al.* 2018), an ischemic HF model was induced by fluoroscopically controlled proximal occlusion of the left anterior descending coronary artery (LAD) with a balloon-tip catheter (balloon 4 x 20 mm or 5 x 20 mm). Amiodarone was administered (150-300 mg IV) prior to occlusion. LAD occlusion lasted for 40-50 min. In case the ventricular fibrillation (VF) occurred, the ECMO flow of 60 ml/kg/min was used to substitute the systemic circulation. Defibrillation was then performed after the balloon deflation. Moreover, if

MAP dropped below 50 mmHg, continual infusion of norepinephrine (0.01-0.1 mcg/kg/min) was started and titrated at the lowest rate to maintain MAP 50-60 mmHg.

Subsequently, identical VA ECMO protocol as described above was applied to conditions of acute ischemic heart failure, and hemodynamic and lung impedance values were compared to those acquired with the healthy circulation.

Electrical impedance data analysis

As mentioned above, the 64x64 pixel matrix of impedances was continuously generated throughout the whole experiment with an update rate of 50 Hz, creating a dynamic, real-time, cross-sectional, 2D thorax map, at the position of the EIT sensor belt. In time domain, each pixel of that matrix represents the time-course of reconstructed electrical impedance of corresponding thorax tissue region. To filter out frequencies higher than those related to breathing, we rejected all frequencies above 1 Hz by low-pass filter. Furthermore, to isolate the lung regions, we filtered out other chest areas, by discarding pixels (matrix elements) that were more than 0.8π cycle out of breathing phase, as viewed from the 0π phase pixel representing the center of the lungs (Figure 2). Pixels being less than 0.8π from the 0π reference point set up the breathing mask at the beginning of each experiment. Then, the impedance was averaged over this mask region only (summing all impedances of those pixels, divided by the number of pixels in the mask), giving us the course of impedance of whole lungs in time. These EIT values registered at the end of expiration cycles, averaged over the last 30 s of each EBF step, were further processed. To eliminate interindividual variability of absolute lung impedance, values of lung impedance were rescaled by normalization. Within the time frame of one ECMO protocol,

impedance values taken at various EBF steps were normalized with respect to the EBF of 1 l/min (assigned with reference impedance set to 1).

Statistical analysis

Except the electrical impedance, recordings were sampled at 400 Hz by PowerLab A/D converted and continuously recorded by LabChart Pro Software (ADInstruments, Australia). EIT data were analyzed in MATLAB (The MathWorks, USA) and normalized to baseline value measured at 1 l/min of EBF. Statistical analyses were performed in GraphPad Prism 7 (GraphPad Software, USA) and Excel (Microsoft, USA).

All results are expressed as mean ± standard error of mean (SEM). The differences among individual levels of EBF were analyzed using a repeated-measures one-way ANOVA with Tukey's multiple comparison test or using the Friedman test with Dunn's multiple comparison test (for data sets without normal distribution). Success in heart failure induction was verified using the Wilcoxon signed-rank test. A P value of < 0.05 was considered statistically significant.

Results

Hemodynamic characteristics of the model before (healthy) and after the acute heart failure (HF) induction are summarized in Table 1. Ventricular fibrillation occurred in all animals within the first ten minutes of LAD occlusion. It was successfully terminated by an external defibrillation. HF induction had a significant effect on all major hemodynamic parameters: cardiac output decreased from 5.5 \pm 0.7 to 2.9 \pm 0.3 l/min (P < 0.01), MAP from 76 \pm 5 to 51 \pm 4 mmHg (P < 0.01), carotid flow from 419 \pm 37 to 248 \pm 22 ml/min (P < 0.05), and mixed venous oxygen saturation and rSO₂ on forehead decreased by 23% and 25%, respectively (for both P < 0.05). All these parameters were obtained with 1 l/min of EBF support, before the start of each ECMO protocol. Moreover, five animals required norepinephrine administration (0.01-0.1 mcg/kg/min) during EBF 1 to prevent severe hypotension. In these animals, norepinephrine was discontinued after MAP reached 60 mmHg.

VA ECMO effects on hemodynamics and electrical impedance are detailed in Table 2 and Figure 3. With the same VA ECMO protocol applied to the healthy and the heart failure conditions, we have observed different effects on electrical impedance of the lung regions. With increasing EBF from 1 to 4 l/min the normalized lung impedance did not change in the healthy circulation but declined with each EBF step in HF group – from 1 ± 0.0 to 0.986 ± 0.009 , 0.979 ± 0.014 , and 0.974 ± 0.017 (for EBF 1 to 4 l/min, P < 0.001). Figure 1 shows an example of full trends of electrical impedance over the ECMO protocol in healthy and HF conditions.

In stepwise ECMO protocol applied to the healthy circulation, with increasing EBF (from EBF 1 to 4 l/min) MAP increased from 75 ± 5 to 92 ± 6 mmHg (P < 0.01) and mean carotid flow from 395 ± 26 to 435 ± 38 ml/min (P < 0.05). MPAP decreased from 29 ± 4 to 23 ± 3 mmHg (P < 0.001), PCWP decreased mildly from 5.4 ± 0.9 to 4.4 ± 0.6 mmHg (P < 0.05), and transpulmonary pressure gradient (TPG) from 24 ± 4 to 18 ± 3 mmHg (P < 0.01). SvO₂ increased from 76 ± 3% to $83 \pm 3\%$ (P < 0.01). Regional tissue oxygenation increased on forehead from 72 ± 2% to 76 ± 1% (P < 0.01) and did not change significantly on forelimb. With increasing EBF, the CVP gradually fell from 4.4 ± 0.5 to 2.6 ± 0.7 mmHg (P < 0.001).

Effects of the same ECMO protocol applied to HF model were considerably stronger. From EBF 1 to 4 l/min MAP increased from 52 ± 5 to 74 ± 6 mmHg (P < 0.01) and carotid flow increased from 258 ± 28 to 410 ± 34 ml/min (P < 0.01). MPAP did not change significantly, nevertheless PCWP increased from 8.3 ± 1.9 to 10.3 ± 1.8 mmHg (P < 0.001), and TPG decreased from 27 ± 4 mmHg to 15 ± 5 mmHg (P < 0.05). SvO₂ improved from $56 \pm 6\%$ to $84 \pm 4\%$ (P < 0.0001), rSO₂ on forehead increased from $52 \pm 4\%$ to $66 \pm 3\%$ (P < 0.01), and on forelimb from $58 \pm 3\%$ to $65 \pm 3\%$ (P < 0.01). CVP decreased from 7.5 ± 0.5 to 5.1 ± 0.4 mmHg (P <0.01).

V_T and PEEP was set constant during the whole protocol to minimize the influence of lung air content to the EIT measurement. Nevertheless, for EBF 1 to 4 l/min mean airway pressure decreased in both groups, from 10.0 ± 0.3 to 9.1 ± 0.4 cmH₂O (P < 0.001) in healthy circulation and from 9.9 ± 0.5 to 8.9 ± 0.3 cmH₂O (P < 0.05) in HF model. With increasing EBF, static lung compliance decreased in healthy circulation group from 31 ± 2 to 30 ± 2 ml/cmH₂O (P < 0.001) but did not change in HF model.

Discussion

Recent studies have reported the effect of increasing VA ECMO flow on the LV overload under severe heart failure condition. However, not enough attention has been paid to pulmonary edema which may consequently occur. The primary aim of this study was to evaluate the ability of EIT to distinguish even small changes in fluid content within the lung tissue related to VA ECMO operation. For this purpose, we have developed a custom-build algorithm for EIT signal analysis and together with other hemodynamic and oximetry parameters we used it to compare the effects of VA ECMO on healthy versus heart failure circulation.

Electrical impedance tomography for pulmonary fluid detection

Our key finding is that in a failing circulation supported by VA ECMO, the electrical impedance of pulmonary regions reduces with increasing EBF (1-4 l/min). This was significantly different from a healthy heart with identical ECMO support where there was no change in pulmonary region impedance (Figure 3). Impedance is affected by numerous parameters such as pulmonary aeration, fluid infusion rate, patient movement, and electrodes position, so care was taken that these were kept constant. This is discussed in more detail here.

The changes of thoracic electrical impedance associated with the breathing cycle are one order of magnitude larger than the changes induced by the heart-lung perfusion cycle or the fluid accumulation. Thus, several approaches have been proposed to separate lung regions and perfusion-related changes as well. This mainly includes auto-detection of the pulmonary region based on methods of identifying regions of interest such as frequency-based or statistic-based methods (Ferrario *et al.* 2012, Frerichs *et al.* 2017). However, some of these reconstructions do not correspond well to the expected lung anatomy. Isophase analysis, i.e. finding the regions of the same breathing phase (Riedel *et al.* 2009, Graf and Riedel 2017), realized by our own algorithm and area-averaging of the impedance signal identified more relevant breathing regions.

Volume control lung-protective ventilation with constant tidal volume (V_T) and constant PEEP was used to eliminate the effect of variable functional residual capacity and V_T on electrical

impedance, revealing thus much more delicate impedance effects caused by parameters like fluid accumulation in lungs. In heart failure conditions, the static lung compliance did not change significantly throughout the protocol, thus we assume that there was no influence of air volume on end-expiratory electrical impedance. In healthy condition there was a small decrease of static lung compliance (0.9 ml/cm H₂O) accompanied with no impedance decrease. This result was not expected but its magnitude had no significant effect on the outcome. We hypothesize that it could be the consequence of overall pulmonary deterioration often seen during general anesthesia.

The effect of fluid administration was minimized by keeping IV infusions constant throughout the protocol (5-6 ml/kg/h), eliminating possible effects on the lung impedance. We suppose that constant lung impedance measured during running infusions indicates balanced fluid intake and loss.

Under constant ventilation and constant fluid infusions, we assume that the decrease in pulmonary region impedance during VA ECMO can be interpreted as an indirect marker of fluid accumulation. Increasing EBF generates higher afterload (represented by the rise in MAP – see Figure 3) that impedes ventricular emptying of failing LV. This may be supported by the observation of LV filling pressure elevation (PCWP) despite significant reduction of preload (CVP) caused by ECMO drainage from the central veins.

Extracorporeal membrane oxygenation in healthy circulation

Interesting outputs of the study are findings regarding the effects of increasing VA ECMO flow on healthy circulation. Our data indicate that even for the highest EBF (80 ml/kg/min), which

is about 75% of the resting cardiac output, the overall hemodynamics and oxygenation changed only little. In healthy circulation, MAP increased by 23%, carotid blood flow increased by 10%, rSO₂ on the forehead by 7%, on the forelimb by 1%, and SvO₂ by 9%. Thus, increased blood flow caused by VA ECMO could have been balanced by regulatory mechanisms, such as shunting the blood through arterio-venous anastomoses and by reducing cardiac output. Since carotid flow (a correlate for the global blood flow) increased only by 10%, the latter option might be more involved. Indeed, during increasing of EBF from 1 to 4 l/min, we noticed a significant decrease in CVP (by 41%) and in MPAP (by 22%). The TPG decreased in healthy as well as in the HF groups. This is likely a consequence of increased venous drainage by VA ECMO inflow cannula.

Aside from decreasing preload, VA ECMO increases left ventricular afterload. However, in healthy animals MAP increased only by 23% (Table 2). Furthermore, the electrical impedance in the pulmonary region did not change during EBF stepwise increases. Thus, we assume that fluids were neither depleted nor accumulated in the lungs in healthy animals due to VA ECMO operation. This was contrary to the observations in the HF condition.

An unexpected observation was the decrease in pulmonary compliance (40 to 32 ml/cmH₂O) soon after the VA ECMO insertion during the preparatory phase. This could be related to high pulmonary vasoreactivity of swine lungs that was triggered by the contact of blood with the extracorporeal circuit.

Extracorporeal membrane oxygenation in heart failure

In all animals we have succeeded in inducing moderate to severe acute heart failure with severe hypotension, hypoperfusion, increased filling pressures of both left and right ventricle (i.e.

increased PCWP and CVP, respectively), and impaired oxygenation (Table 1). During the HF induction, the static lung compliance further decreased (32 to 25 ml/cmH₂O). This could have been caused by the onset of heart failure.

Recent studies have discussed EBF influence on a failing systemic circulation and our hemodynamic results are consistent with their findings (Burkhoff *et al.* 2015, Ostadal *et al.* 2015). In our study systemic hemodynamics and oximetry parameters increased considerably with increasing EBF from 1 to 4 l/min, MAP by 44%, carotid flow by 59%, SvO₂ by 49% (Table 2). The maximal EBF that was achieved in all animals was 80 ml/kg/min (4 l/min). Only such high flow allowed for almost complete restoration of hemodynamics and oxygen delivery, demonstrated by rSO₂ and SvO₂. Both these parameters are used also clinically to monitor patients supported with VA ECMO since they are not dependent on the pulsatility of blood flow. Interpretation of SvO₂ in terms of VA ECMO is rather complex as it would be influenced by actual ratio of pulmonary and extracorporeal flows. In the settings of VA ECMO, the SvO₂ reflects both delivery of oxygen and its extraction (Doufle and Ferguson 2016), but SvO₂ values may vary in the venous blood of tissues supplied by native and extracorporeal circulation (Ostadal *et al.* 2018).

Despite reduced CVP and hence decreased right ventricular output caused by increasing VA ECMO drainage of the central veins, there was significant increase in the already elevated PCWP (Figure 3). PCWP reflects both LV preload and LV cardiac output. If preload was reduced and PCWP increased, then this finding could again support the hypothesis that LV output (emptying) is compromised by increased LV afterload generated by increasing EBF. This is in accord with the findings from EIT discussed above.

Limitations

EIT is a highly sensitive method of fluid content monitoring as demonstrated above. The major EIT limitation is the dependence of impedance on several parameters that can change independently and might be difficult to separate in real-life scenarios. End-expiratory lung impedance can be influenced by other mechanisms than tidal volume and fluids, such as air trapping and/or air leaks. We consider air trapping was insignificant in our setup as no increase in intrinsic PEEP was noticed. Also, tidal volume and respiratory rate were low and there were no signs of airway obstruction. With adequate endotracheal cuff inflation, the air leak was only 2.1% of tidal volume in both groups and thus should not have affected the end-expiratory lung impedance. Moreover, it is known that EIT lacks the ability to reliably provide results in absolute units that would be unambiguously interpreted and compared among the patients, which is why we reported normalized EIT values solving that problem. In a recent study Da Silva Ramos et al. (2018) showed, that the differences in body dimension have a significant influence on the electrical impedance. To minimize this effect, we included animals of similar body weight. We expect that additional implementation of features like ventilation gating (based on airway pressure and flow) and cardiac cycle gating (based on ECG) would, in future, broaden the spectrum of observed parameters and make our analysis more robust. Moreover, this could enable the estimation of relative changes in systolic impedance variation (Vonk-Noordegraaf et al. 2000). We do not have a direct proof of lung fluid accumulation, e.g. transpulmonary thermodilution (TPTD). Nevertheless, Sobota et al. (2019) demonstrated that EIT is more sensitive compared to the TPTD in identifying the changes in lung fluids, as TPTD may not reflect small changes of lung fluids. Previous works have suggested that the pulmonary edema usually occurs after days of VA ECMO running (Lequier *et al.* 2017) and our protocol covered only short periods. Further work is needed to observe long-term VA ECMO influence on electrical impedance to evaluate lung fluid accumulation.

Conclusion

In heart failure conditions, the reduction of lung tissue electrical impedance was observed when VA ECMO flow was increased. In healthy circulation with VA ECMO, this impedance change was not detected. Under constant ventilation and fluid infusion this can be interpreted as transient fluid content changes in the lungs. We conclude that EIT could be considered helpful in monitoring the VA ECMO therapy and its effects on lung fluid content.

Conflict of interest

There is no conflict of interest.

Abbreviations

CVP – central venous pressure, EBF – extracorporeal blood flow, EIT – electrical impedance tomography, etCO₂ – end-tidal CO₂, FiO₂ – fraction of inspired oxygen, HF – heart failure, IM – intramuscular, IV – intravenous, LAD – left anterior descending coronary artery, LV – left ventricle, MAP – mean arterial pressure, MPAP – mean pulmonary artery pressure, PCWP – pulmonary capillary wedge pressure, $_{p}CO$ – cardiac output, pCO₂ – partial pressure of CO₂, pO₂ – partial pressure of oxygen, PEEP – positive end-expiratory pressure, PIP– peak inspiratory pressure, rSO_2 – regional oxygen saturation, SEM – standard error of mean, SvO_2 – mixed venous oxygen saturation, TPG – transpulmonary pressure gradient, TPTD – transpulmonary thermodilution, VA ECMO – veno-arterial extracorporeal membrane oxygenation, VF – ventricular fibrillation, V_T – tidal volume, ΔZ (tidal volume) – change of electrical impedance during breathing cycle, ΔZ (EBF) – change of electrical impedance during increasing EBF.

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Figures and tables



Figure 1. Representative example of EIT waveforms from one animal. Stepwise changes with increasing VA ECMO flows (purple) are aligned with electrical impedance for both healthy (green) and heart failure (red) conditions. Electrical impedance waveforms represent impedance of lung regions during breathing cycles. End-expiratory impedance was evaluated at the end of each EBF step and with increasing EBF it did not change in healthy condition but decreased significantly in heart failure. ΔZ (tidal volume) represents the change in electrical impedance during breathing cycle (tidal volume), whereas ΔZ (EBF) represents change in impedance with increased EBF (EBF 1 to EBF 4 l/min). Δ Z (EBF) is approximately 60% of the ΔZ (tidal volume) in this animal.



Figure 2. Analysis of EIT signal. To the left, 64x64 impedance matrix and corresponding colorbar map show the phase delay from the reference pixel of zero phase (red dot), representing the center of the left lung. In the middle, resulting breathing mask (orange) defines pixels which were analyzed at expiration (green dots), averaged over this mask region, and normalized to the EIT value obtained at EBF 1 l/min. EBF – extracorporeal blood flow, EIT – electrical impedance tomography.



Figure 3. The effect of veno-arterial membrane oxygenation blood flow (EBF) on selected hemodynamic parameters and EIT in a porcine model of healthy (green triangles) and heart failure (red dots) conditions. Means and SEMs shown here have descriptive meaning, for details of P values see the Methods. Values significantly different to 1 l/min (EBF 1) are marked with * for P < 0.05, ** for P < 0.01, *** for P < 0.001. The two P values in the legend reflect the whole EBF trend statistics. EBF – extracorporeal blood flow, EIT – electrical impedance of lung regions

normalized to EBF 1 (1 l/min), MAP – mean arterial pressure, PCWP – pulmonary capillary wedge pressure, ns – non-significant.

		Healthy	Heart failure	P value	Change	
pCO	l/min	5.5 ± 0.7	2.9 ± 0.3	< 0.01	-47%	
MAP	mmHg	76 ± 5	51 ± 4	< 0.01	-33%	
Carotid flow	ml/min	419 ± 37	248 ± 22	< 0.05	-41%	
SvO ₂	%	76 ± 3	59 ± 6	< 0.01	-23%	
rSO_2 head	%	72 ± 2	54 ± 3	< 0.05	-25%	

Table 1. Hemodynamic parameters of heart failure induced by myocardial ischemia. Values expressed as mean ± SEM. Last column presents the relative change between healthy and heart failure. Parameters were obtained with 1 l/min of EBF before start of the ECMO protocol. EBF – extracorporeal blood flow, ECMO – extracorporeal membrane oxygenation, MAP – mean arterial pressure, $_{p}$ CO – cardiac output measured using a pulmonary artery catheter, rSO₂ head – regional tissue oxygenation measured on forehead, SvO₂ – mixed venous oxygen saturation.

	I/min	EBF 1		EBF 2		EBF 3		EBF 4		P value	
		Healthy	Heart failure	Healthy	Heart failure	Healthy	Heart failure	Healthy	Heart failure	Healthy	Heart failure
MAP	mmHg	75 ± 5	52 ± 5	84 ± 5	53 ± 5	*87 ± 6	60 ± 4	**92 ± 6	**74 ± 6	< 0.01	< 0.01
Carotid flow	ml/min	395 ± 26	258 ± 28	425 ± 30	310 ± 43	*456 ± 31	319 ± 23	435 ± 38	**410 ± 34	< 0.05	< 0.01
MPAP	mmHg	29 ± 4	32 ± 4	27 ± 4	29 ± 5	*24 ± 3	25 ± 3	**23 ± 3	25 ± 3	< 0.001	ns
PCWP	mmHg	5.4 ± 0.9	8.3 ± 1.9	5.4 ± 0.9	8.8 ± 2.0	5.1 ± 0.5	10.5 ± 2.1	4.4 ± 0.6	*10.3 ± 1.8	< 0.05	< 0.001
CVP	mmHg	4.4 ± 0.5	7.5 ± 0.5	3.9 ± 0.5	6.5 ± 0.5	3.3 ± 0.6	6.0 ± 0.5	*2.6 ± 0.7	*5.1 ± 0.4	< 0.01	< 0.01
SvO ₂	%	76 ± 3	56 ± 6	80 ± 3	67 ± 4	*82 ± 2	*74 ± 3	*83 ± 3	****84 ± 4	< 0.01	< 0.0001
rSO ₂ head	%	72 ± 2	52 ± 4	73 ± 2	54 ± 5	*76 ± 2	61 ± 3	**76 ± 1	**66 ± 3	< 0.01	< 0.01
rSO ₂ limb	%	69 ± 2	58 ± 3	69 ± 2	61 ± 2	69 ± 2	62 ± 3	70 ± 2	**65 ± 3	ns	< 0.01
EIT		1.000	1.000	0.999 ± 0.006	0.986 ± 0.003	1.006 ± 0.007	**0.978 ± 0.005	1.006 ± 0.009	***0.974 ± 0.006	ns	< 0.001

Table 2. Comparison of the effects of extracorporeal blood flow on hemodynamic parameters and electrical impedance of lungs in healthy circulation and heart failure conditions. Values expressed as mean ± SEM. Values significantly different to 1 l/min (EBF 1) are marked with * for P < 0.05, ** for P < 0.01, *** for P < 0.001, **** for P < 0.0001. The two P values in last two columns reflect the whole EBF trend statistics. CVP – central venous pressure, EBF – extracorporeal blood flow, EIT –electrical impedance normalized to EBF 1, MAP – mean arterial pressure, MPAP – mean pulmonary artery pressure, PCWP – pulmonary capillary wedge pressure, ns – non-significant, rSO₂ – regional tissue oxygenation, SvO₂ – mixed venous oxygen saturation.

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