# THE POLE PLACEMENT EQUATION – A SURVEY

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We consider the linear equation AX + BY = C where A, B and C are given polynomials from K[s], the ring of polynomials in the indeterminate s over a field K, and X and Y are unknown polynomials in K[s].

#### 1. MOTIVATION

The equation

$$AX + BY = C (1)$$

has found application in several design problems for linear control systems, including the pole placement design. This problem consists in the following: given a plant with real-rational proper transfer function

$$P(s) = \frac{B(s)}{A(s)},$$

where A and B are coprime polynomials, one seeks to determine a dynamic output feedback controller with a real-rational proper transfer function, say

$$Q(s) = -\frac{Y(s)}{X(s)}$$

such that the closed-loop system has prespecified poles.

Provided A is the characteristic polynomial of the plant and X is that of the controller, then the characteristic polynomial of the closed-loop system, say C(s), which specifies the poles desired, is given by C = AX + BY.

Thus the pole placement design is based on equation (1). However not all solution pairs X, Y are of interest: one must take the one in which Y has least degree. This leads to a proper controller whenever one exists.

## 2. REVIEW OF THEORY

It is well known [1] that K[s] is a principal ideal domain. Thus (1) is solvable if and only if any greatest common divisor of A and B divides C. Writing D for a greatest

common divisor of A and B and denoting

$$\bar{A} = \frac{A}{D}, \quad \bar{B} = \frac{B}{D}, \quad \bar{C} = \frac{C}{D}$$

one concludes that (1) has a solution if and only if  $\bar{C}$  is a polynomial. Therefore if A and B are coprime then (1) is solvable for any C.

Suppose that  $\bar{X}, \bar{Y}$  is a particular solution pair of (1). Since the equation is linear, any and all solution pairs of (1) are given by

$$X = \bar{X} - \bar{B}T, \quad Y = \bar{Y} + \bar{A}T,$$

where T varies over K[s]. Thus the solution class of (1) is parametrized through T in a simple manner.

It is well known [1] that K[s] is a euclidean domain. Therefore if (1) is solvable and  $B \neq 0$  there is a unique solution pair  $X_{1 \min}, Y_1$  of (1) such that either  $X_{1 \min} = 0$  or  $\deg X_{1 \min} < \deg \bar{B}$ . Further if (1) is solvable and  $A \neq 0$  then there is a unique solution pair  $X_2, Y_{2 \min}$  of (1) such that either  $Y_{2 \min} = 0$  or  $\deg Y_{2 \min} < \deg \bar{A}$ . These two least-degree solution pairs coincide [4] whenever  $\deg \bar{A} + \deg \bar{B} > \deg \bar{C}$ .

As a result, equation (1) with  $A \neq 0$  and  $B \neq 0$  can possess solution pairs X, Y of arbitrarily high degree, limited only from below by deg  $X_{1 \min}$  and deg  $Y_{2 \min}$ .

#### 3. FIXED DEGREE SOLUTIONS

We shall study the class of solutions whose degrees are limited from above. We suppose that A, B and C in (1) are *non-zero* polynomials from K[s] with A and B coprime. Hence (1) is solvable. Let

$$p = \deg A, \quad q = \deg B, \quad r = \deg C.$$

If

$$A = a_0 + a_1 s + \ldots + a_p s^p$$

then, for any integer  $k \geq p$ , we denote

$$\operatorname{vec}_k A = [a_0 \ a_1 \dots a_p \underbrace{0 \dots 0}_{k-p}].$$

The existence result [5] is as follows. Let m, n be non-negative integers and  $d = \max(m + p, n + q, r)$ . Then a solution pair X, Y of (1) exists such that

$$X = 0$$
 or  $\deg X \le m$ ,  $Y = 0$  or  $\deg Y \le n$  (2)

if and only if  $\operatorname{vec}_d C$  is a K-linear combination of  $\operatorname{vec}_d A$ ,  $\operatorname{vec}_d s A$ , ...,  $\operatorname{vec}_d s^m A$ ,  $\operatorname{vec}_d B$ , ...,  $\operatorname{vec}_d s^n B$ .

A special case of particular interest concerns the *constant* solutions of (1). Putting m = n = 0 we deduce [6] that a solution pair X, Y of (1) exists in K if and only if  $\operatorname{vec}_d C$  is a K-linear combination of  $\operatorname{vec}_d A$  and  $\operatorname{vec}_d B$ .

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The set of solutions whose degrees are limited from above can be parametrized as follows [5]. Let  $m \ge q$  and  $n \ge p$ . If  $n \ge r - q$  then the set of solutions X, Y of (1) that satisfy (2) is given as

$$X = X_{1 \min} - BT_1, \quad Y = Y_1 + AT_1, \tag{3}$$

where  $T_1$  varies over K[s] and

$$\deg T_1 \le \min(m - q, n - p);$$

if  $m \ge r - p$  then the set of solutions X, Y of (1) that satisfy (2) is given as

$$X = X_2 - BT_2, \quad Y = Y_{2\min} + AT_2, \tag{4}$$

where  $T_2$  varies over K[s] and

$$\deg T_2 \leq \min(m-q, n-p).$$

Indeed suppose that  $n \geq r - q$ . Then (3) implies

$$\deg X = q + \deg T_1 \le m$$

$$\deg Y = \max(r - q, p + \deg T_1) \le n$$

so that deg  $T_1 \leq m - q$  and deg  $T_1 \leq n - p$ . In case  $m \geq r - p$  then (4) implies

$$\deg X = \max(r - p, q + \deg T_2) \le m$$
  
$$\deg Y = p + \deg T_2 \le n$$

and again  $\deg T_2 \leq m - q$  and  $\deg T_2 \leq n - p$ .

We note that at least one of the two conditions,  $m \ge r - p$  and  $n \ge r - q$ , is always satisfied. Of course (3) can be used to parametrize the solution set (2) even if n < r - q. Then, however,  $T_1$  has a higher degree than shown and is not completely free in K[s]. An analogous statement is true for (4) when m < r - p. To illustrate, we parametrize the solution class of

$$X + sY = s^2$$

such that  $\deg X \leq 1$  and  $\deg Y \leq 1$ . Using (3),

$$X = -sT_1$$
,  $Y = s + T_1$ ,  $T_1$  constant

while using (4),

$$X = s^2 - T_2$$
,  $Y = T_2$ ,  $T_2 = s + \tau$ ,  $\tau$  constant.

### 4. EXAMPLES

Can the double integrator

$$\dot{x}_1 = x_2, \quad \dot{x}_2 = u, \quad y = x_1$$

be converted into an harmonic oscillator using a *proportional* output feedback? The double integrator gives rise to the transfer function

$$P(s) = \frac{1}{s^2}$$

and any harmonic oscillator has the characteristic polynomial

$$C(s) = s^2 + \omega^2$$

for some real constant  $\omega > 0$ . Thus the answer depends on the polynomial equation

$$s^2X + Y = s^2 + \omega^2$$

having a constant solution pair X, Y.

Since

$$vec_2 A = [0 \ 0 \ 1]$$

$$\operatorname{vec}_2 B = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix}$$

$$\operatorname{vec}_2 C = [\omega^2 \ 0 \ 1]$$

the answer is an affirmative: the output feedback  $u = -\omega^2 y$  will do the job. The resulting system equations read

$$\dot{x}_1 = x_2, \quad \dot{x}_2 = u - \omega^2 x_1, \quad y = x_1.$$

On the other hand, the double integerator cannot be stabilized via proportional output feedback: the polynomial  $s^2X + Y$  is not Hurwitz for any real numbers X and Y.

As the second example, we consider the plant

$$\dot{x}_1 = u - x, \quad y = x$$

and find all output feedback controllers that will alter its characteristic polynomial s + 1 to  $s^2 + 3s + 2$ .

These controllers possess the transfer functions

$$Q(s) = -\frac{Y(s)}{X(s)},$$

where X, Y is the solution set of the equation

$$(s+1)X + Y = s^2 + 3s + 2$$

such that  $\deg X = 1$  and  $\deg Y \leq 1$ .

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The condition  $m \ge r - p = 1$  is verified. Therefore the solution set is given by

$$X = s + 2 - T_2, \quad Y = (s+1)T_2,$$

where  $T_2$  is any real polynomial of degree at most  $\min(m-q, n-p) = 0$ , hence any real constant.

A realization of the parametrized controller set is

$$\dot{w} = (T_2 - 2) w + (T_2 - 1) y$$
  
 $-u = T_2 w + T_2 y$ .

The case  $T_2=0$  leads to an unobservable realization while  $T_2=1$  leads to an uncontrollable realization. A PI controller is obtained when  $T_2=2$ .

If desired, the parameter  $T_2$  can be chosen so that a specific goal is achieved. For example, if the  $H_{\infty}$ -norm of the sensitivity function

$$S(s) = \frac{s+2}{s+2-T_2}$$

is not to exceed 1, we should avoid the values  $0 < T_2 < 4$ .

# 5. METHODS OF SOLUTION

Equation (1) can be solved in several ways [4]. One can distinguish *parametric* methods (where the polynomials are represented by their coefficients) and *non-parametric* ones (where the polynomials are represented by their functional values.) We shall describe three major parametric methods.

We suppose that A, B and C in (1) are non-zero *real* polynomials with A and B coprime. Hence (1) is solvable. For the sake of simplicity let

$$\deg A = \deg B = N, \quad \deg C = 2N - 1.$$

The Method of Indeterminate Coefficients [4] converts equation (1) into a system of 2N linear equations over the field of real numbers. Suppose we seek the least-degree solution pair X,Y:

$$\deg X \le N - 1, \quad \deg Y \le N - 1.$$

The 2N coefficients of X, Y satisfy the system of equations

$$\begin{bmatrix} \operatorname{vec}_{N-1} X & \operatorname{vec}_{N-1} Y \end{bmatrix} \begin{bmatrix} \operatorname{vec}_{2N-1} A \\ \dots \\ \operatorname{vec}_{2N-1} s^{N-1} A \\ \operatorname{vec}_{2N-1} B \\ \dots \\ \operatorname{vec}_{2N-1} s^{N-1} B \end{bmatrix} = \operatorname{vec}_{2N-1} C.$$

The system matrix is a Sylvester matrix and it has full rank since A and B are coprime.

The *Method of Polynomial Reductions* [3] reduces equation (1) to a polynomial equation that is much easier to solve. It consists of the substitutions

$$C' = C - A \frac{c_{\deg C}}{a_{\deg A}} s^{\deg C - \deg A}$$

$$C' = C - B \frac{c_{\deg C}}{b_{\deg B}} s^{\deg C - \deg B}$$

$$B' = B - A \frac{b_{\deg B}}{a_{\deg A}} s^{\deg B - \deg A}$$

$$A' = A - B \frac{a_{\deg A}}{b_{\deg B}} s^{\deg A - \deg B}$$

each reducing the degree of one of the polynomials A, B, C. The substitutions are repeated for the new polynomials A', B', C' and will ultimately reduce all A, B, C but one to zero. The resulting equation has a solution X' = 0, Y' = 0 and the solution pair X, Y of (1) is obtained through the backward substitutions

$$X = X' + \frac{c_{\deg C}}{a_{\deg A}} s^{\deg C - \deg A}$$

$$Y = Y' + \frac{c_{\deg C}}{b_{\deg B}} s^{\deg C - \deg B}$$

$$X = X' - Y \frac{b_{\deg B}}{a_{\deg A}} s^{\deg B - \deg A}$$

$$Y = Y' - X \frac{a_{\deg A}}{b_{\deg B}} s^{\deg A - \deg B}.$$

The process involves the euclidean algorithm for A, B and leads to the least-degree solution pair X, Y.

The Method of State-space Realization [2] combines matrix and polynomial operations. We write (1) as

$$X + \frac{B}{A}Y = \frac{C}{A}$$

and determine a reachable state-space realization (F, G, H, J) of the rational function B/A. The N coefficients of Y satisfy the system of equations

$$\operatorname{vec}_{N-1}Y \left[ \begin{array}{c} H \\ HF \\ \dots \\ HF^{N-1} \end{array} \right] = \operatorname{vec}_{N-1}(C \text{ mod } A)$$

and the corresponding X is recovered from (1); it is the least-degree solution pair. The system matrix is an observability matrix and it has full rank since A and B are coprime.

# 6. NUMERICAL EXPERIENCE

The method of indeterminate coefficients is straightforward and leads directly to a system of linear equations for the coefficients of the unknown polynomials. The

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method of polynomial reductions solves the polynomial equation by polynomial means and is not suitable for pencil-and-paper calculations, for it requires a large number of logical operations. The method of state-space realization combines the two above: one unknown polynomial is obtained by solving a system of linear equations while the other results from polynomial manipulations.

The comparison of the methods with respect to the arithmetic complexity is quite clear [7]. The fastest is the method of polynomial reductions, where the operations count is proportional to  $N^2$ . For the other two methods the arithmetic complexity is proportional to  $N^3$ . The slowest method, however, is that of indeterminate coefficients because it leads to a larger system of linear equations than the method of state-space realization.

The comparison of the methods from the precision point of view [7] is not that simple, however. Provided the polynomials A and B have no (especially multiple) roots close to each other, the precision of all three methods is alike. The ill-conditioned data, however, make the method of polynomial reductions fail more often than that of indeterminate coefficients. The method of state-space realization shows no clear-cut tendency, it stays between the two preceding methods.

To conclude, polynomial reductions are fast but sensitive to data, indeterminate coefficients are robust but slow, and the method of state-space realization is universal but second best in each single aspect.

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#### REFERENCES

- [1] N. Bourbaki: Algèbre Commutative. Hermann et Cie, Paris 1961.
- [2] E. Emre: The polynomial equation  $QQ_c + RP_c = \Phi$  with application to dynamic feedback. SIAM J. Contr. Optimiz. 18 (1980), 611–620.
- [3] J. Ježek: New algorithm for minimal solution of linear polynomial equations. Kybernetika 18 (1982), 505–516.
- [4] V. Kučera: Discrete Linear Control: The Polynomial Equation Approach. Wiley, Chichester 1979.
- [5] V. Kučera: Fixed degree solutions of polynomial equations. In: Proc. 2nd IFAC Workshop on System Structure and Control, Prague 1992, pp. 24–26.
- [6] V. Kučera and P. Zagalak: Constant solutions of polynomial equations. Int. J. Control 53 (1991), 495–502.
- [7] V. Kučera, J. Ježek and M. Krupička: Numerical analysis of diophantine equations. In: Advanced Methods in Adaptive Control for Industrial Applications (K. Warwick, M. Kárný and A. Halousková, eds.), Springer, Berlin 1991, pp. 128–136.

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