



# Solving Poisson equation over planar NURBS domains with isogeometric analysis

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### (joint research with P. Anděl)

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Solving Poisson equation with isogeometric analysis

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## Outline

## 1 Isogeometric analysis

- Introduction
- NURBS surfaces
- Planar NURBS domains
- NURBS volumes

### 2 Implementation – example (Poisson equation)

- Homogeneous Dirichlet boundary value problem
- Non-homogeneous Dirichlet boundary value problem

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- many features common with the finite element method
- inspired by CAGD primary goal is to be geometrically exact independently of the discretization
- typically in engineering practice, design is done in CAD systems and meshes, needed for the finite element analysis, are generated from CAD data
- in some cases, mesh can be generated automatically, but in most cases, it is done semi-automatically – it usually needs human interaction
- ► it is estimated that about 80% of overall analysis time is spent in mesh generation in automotive, aerospace and ship industries
- each design change requires generation of new meshes which takes a lot of time
- further, inaccuracies in geometric representation can lead to problems with precision of obtained solutions, e.g. thin shell analysis is extremely sensitive to geometric imperfections or problems in fluid mechanics

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- then all objects are represented exactly (as in CAD system) and we do not need to create any other mesh – the mesh of the so-called "NURBS elements" is acquired directly from CAD representation
- further refinement of the mesh (knot insertion h-refinement) or increasing the order of basis functions (order elevation – p-refinement) are very simple, also the suitable combination of these methods called k-refinement seems to be very efficient and robust
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# NURBS surfaces

▶ NURBS surface of degree p, q is determined by a control net  $\mathbf{P}$  (of control points  $P_{i,j}, i = 0, ..., n, j = 0, ..., m$ ), weights  $w_{i,j}$  of these control points and two knot vectors  $U = (u_0, ..., u_{n+p+1}), V = (v_0, ..., v_{m+q+1})$  and is given by a parametrization

$$S(u,v) = \frac{\sum_{i=0}^{n} \sum_{j=0}^{m} w_{i,j} P_{i,j} N_{i,p}(u) M_{j,q}(v)}{\sum_{i=0}^{n} \sum_{j=0}^{m} w_{i,j} N_{i,p}(u) M_{j,q}(v)} = \sum_{i=0}^{n} \sum_{j=0}^{m} w_{i,j} P_{i,j} R_{i,j}(u,v)$$

▶ B-spline basis functions  $N_{i,p}(u)$  and  $M_{j,q}(v)$  are determined by knot vectors U and V and degrees p and q, respectively, by a formula

$$\begin{split} N_{i,0}(t) &= \begin{cases} 1 & t_i \leq t < t_{i+1} \\ 0 & \text{otherwise} \end{cases} \\ N_{i,p}(t) &= & \frac{t - t_i}{t_{i+p} - t_i} N_{i,p}(t) + \frac{t_{i+p+1} - t}{t_{i+p+1} - t_{i+1}} N_{i+1,p}(t) \end{split}$$

knot vector is a non-decreasing sequence of real numbers which determines the distribution of a parameter on the corresponding curve/surface and can be uniform or non-uniform and periodic or non-periodic

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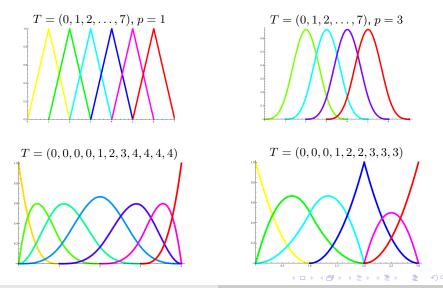
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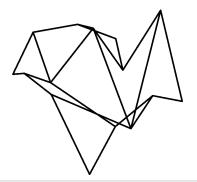
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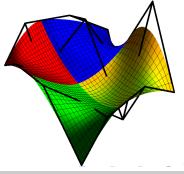
## NURBS surfaces – B-spline basis functions



# NURBS surfaces - properties

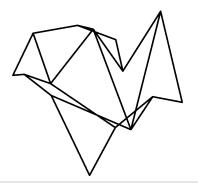
- ▶ B-spline basis functions of degree p are  $C^{p-1}$ -continuous in general
- ▶ knot repeated k times in the knot vector decreases the continuity of B-spline basis functions by k 1
- support of B-spline basis functions is local it is nonzero only on the interval [t<sub>i</sub>, t<sub>i+p+1</sub>] in the parameter space
- ▶ each B-spline basis function is non-negative, i.e.,  $N_{i,p}(t) \ge 0, \forall t$

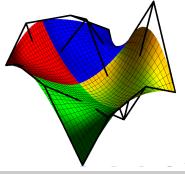




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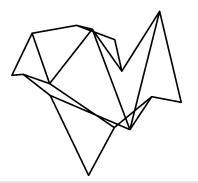
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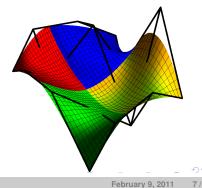




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- one of the key geometric problems in isogeometric analysis is a description of NURBS domains/volumes from their boundary data (contained in CAD model)
- recently, this problem was studied e.g. in Xu et al. (2010) for planar domains, where a sufficient condition for injectivity of planar B-spline parameterization is proposed and also an influence of different parameterizations on computation result is partially studied
- further, Manh et al. (201x) proposes two linear methods for extension of a B-spline parameterization from the boundary of a domain onto its interior during shape optimization of vibrating membranes:
  - the first method is inspired by ideas coming from linear elasticity and is based on a spring model of the mesh (works well for convex domains)
  - the other method is based on a "quasi-conformal deformation" parameterization of an initial reference shape is found by solving optimization problems, then inner control points are generated by quasi-conformal deforming the reference shape into the resulting configuration
- ▶ in general, the resulting domain parameterization should satisfy det(J) > 0everywhere in the parameter domain

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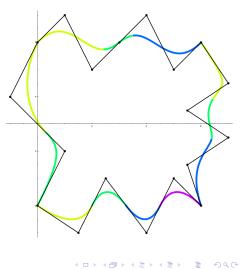
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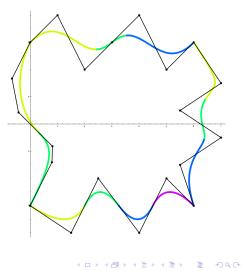
- let a simply connected domain be given by 4 boundary NURBS curves

   we want to find a control net and corresponding knot vectors for planar NURBS surface describing this domain:
- for each pair of "opposite" curves we need these curves to have the same degree (degree elevation)
- 2. ... and the same knots (knot insertion)
- 3. then we can compute interior control points we have several possibilities
- 4. finally, we obtain NURBS surface describing the domain which preserves given boundary curves



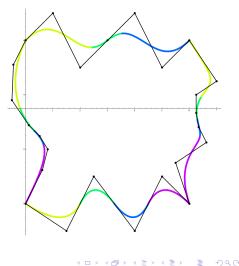
- let a simply connected domain be given by 4 boundary NURBS curves

   we want to find a control net and corresponding knot vectors for planar NURBS surface describing this domain:
- for each pair of "opposite" curves we need these curves to have the same degree (degree elevation)
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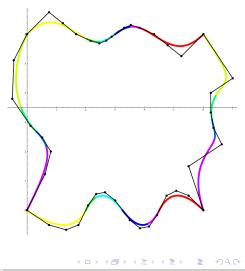
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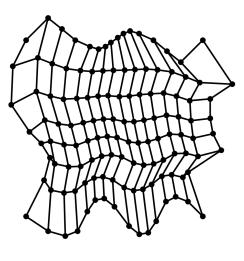
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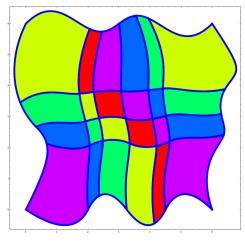
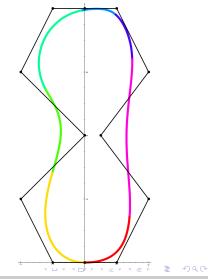


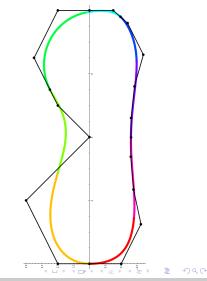
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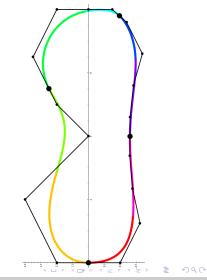
- let a domain be given by a closed boundary NURBS curve – similarly, we need to find control net and knot vectors for NURBS surface representing given domain
- using knot insertion, we subdivide curve into 4 parts with equal number of segments
- then we continue as in the case of 4 boundary NURBS curves – we match degrees and knots of opposite curves
- 3. we generate interior control points
- finally, we obtain NURBS surface describing the domain with prescribed boundary curve



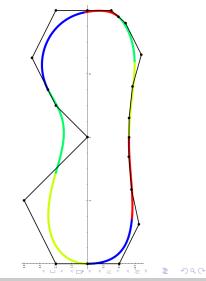
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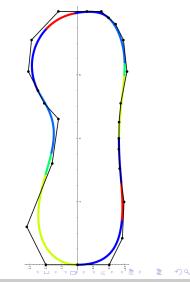


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# Domain bounded by a closed NURBS curve

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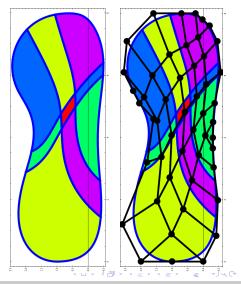
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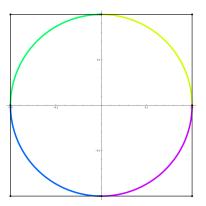


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let us find a parameterization of the unit disc, if the boundary unit circle is given in NURBS form



1. we can add circle center to the control net and connect all boundary control points with the center

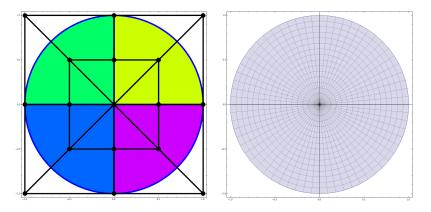
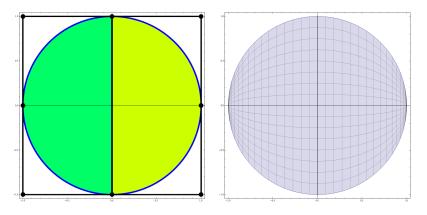


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2. we can divide circle into two parts and use similar algorithm as for 4 boundary NURBS curves



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3. or, we can divide circle into four parts and use algorithm for 4 boundary NURBS curves

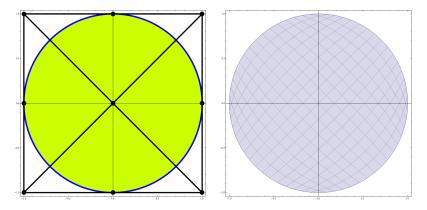


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- the boundary surfaces of the object are given as NURBS surfaces and we need to generate a volume parameterization which preserves the given boundary surfaces
- this is one of the main issues concerning the isogeometric analysis it is very difficult open problem for general CAD objects, but it is possible to obtain results for special classes of free-form objects
- Aigner et al. propose a variational framework for generating NURBS parameterizations of swept volumes, which are obtained by sweeping a closed curve through space
- Martin et al. (2009) presents a method for finding NURBS volume parameterzation based on discrete volumetric harmonic functions which uses closed triangle mesh representing the exterior geometric shape of the object and interior triangle meshes that can represent material attributes or other interior features

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we want to solve the Dirichlet boundary value problem given by

$$\begin{array}{ll} u_{xx} + u_{yy} = f & \text{in } \Omega, \\ u = g & \text{on } \partial\Omega, \end{array}$$
 (1)

where  $\Omega$  is a connected open region in xy-plane whose boundary  $\delta\Omega$  is "nice" (e.g. a smooth curve or a polygon)

• using Green's theorem, if u solves (1), then for any v (v = 0 on  $\delta\Omega$ ) it holds

$$\int_{\Omega} fv ds = \int_{\Omega} v \Delta u ds = -\int_{\Omega} \nabla u \cdot \nabla v ds = -\phi(u, v)$$

- ▶ the basic idea is similar to FEM we need to replace an infinite dimensional problem  $(u, v \in \mathbf{H}_0^1)$  by a finite dimensional one  $(u \in \mathbf{V}_g, v \in \mathbf{V})$
- V is usually chosen as a set of piecewise linear functions over Ω and one of the advantages of this choice of basis functions is that integrals

$$\int_{\Omega} v_j v_k ds$$
 a  $\int_{\Omega} 
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vanish if vertices  $x_j$  and  $x_k$  do not share a common edge in the triangulation

• further, we can write f and u as a linear combination of the new basis functions

$$u(x) = \sum_{k=1}^{n} u_k v_k(x), \ f(x) = \sum_{k=1}^{n} f_k v_k(x)$$

then we obtain

$$-\phi(u,v) = \int fv \longrightarrow -\sum_{k=1}^{n} u_k \phi(v_k, v_j) = \sum_{k=1}^{n} f_k \int v_k v_j, \ j = 1, \dots, n$$
 (2)

• if  $\mathbf{u} = (u_1, \dots, u_n)^T$ ,  $\mathbf{f} = (f_1, \dots, f_n)^T$  and  $L = (L_{ij}) = (\phi(v_i, v_j))$ ,  $M = (M_{ij}) = (\int v_i v_j)$ , then (2) can be rewritten into the form

#### $-L\mathbf{u} = M\mathbf{f}$

- since basis functions  $v_k$  have small support, L and M are sparse matrices
- moreover, L is symmetric and positive definite, so efficient solvers for system of linear equations can be used (e.g. conjugate gradient method)

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in isogeometric analysis, we use rational B-splines as basis function of V, i.e., we express the right hand side and the approximate solution as linear combinations of the basis functions representing the geometry

$$f(s,t) = \sum_{i=0}^{n} \sum_{j=0}^{m} w_{i,j} f_{i,j} R_{i,j}(s,t), \ u(s,t) = \sum_{i=0}^{n} \sum_{j=0}^{m} w_{i,j} u_{i,j} R_{i,j}(s,t)$$
nen
$$-\phi(u,v) = \int_{\Omega} fv ds$$

$$\downarrow$$

$$-\sum_{i=0}^{n} \sum_{j=0}^{m} w_{i,j} u_{i,j} \phi(R_{i,j}, R_{k,l}) = \sum_{i=0}^{n} \sum_{j=0}^{m} w_{i,j} f_{i,j} \varphi(R_{i,j}, R_{k,l}),$$

$$k = 0, \dots, n, l = 0, \dots, m$$

where

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$$\phi(R_{i,j}, R_{k,l}) = \int_{A} (\nabla R_{i,j} \cdot J^{-1}) \cdot (\nabla R_{k,l} \cdot J^{-1}) |\det(J)| dA$$
  
$$\varphi(R_{i,j}, R_{k,l}) = \int_{A} R_{i,j} R_{k,l} |\det(J)| dA$$

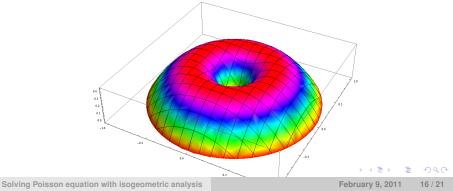
Solving Poisson equation with isogeometric analysis

we want to solve the homogeneous Dirichlet boundary value problem

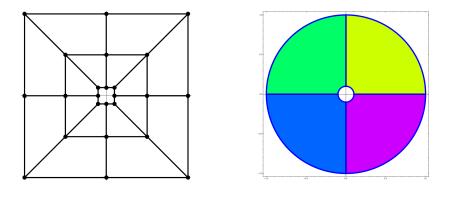
$$u_{xx} + u_{yy} = f \quad \text{in } \Omega, u = 0 \qquad \qquad \text{on } \partial\Omega,$$

where  $\Omega = \{(x,y) \in \mathbb{R}^2: \frac{1}{100} < x^2 + y^2 < 1\}$  with the help of isogeometric analysis

▶ for f = -4, the exact solution is  $u(x, y) = \frac{99 \log(x^2 + y^2)}{200 \log(10)} - x^2 - y^2 + 1$ 

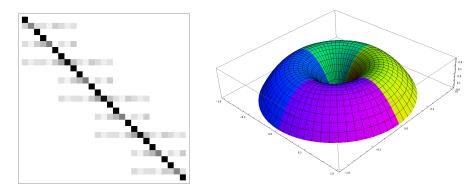


▶ 4 elements (knot vectors are V = (0, 0, 0, 1/4, 1/4, 1/2, 1/2, 3/4, 3/4, 1, 1, 1), U = (0, 0, 0, 1, 1, 1), control net shown below)



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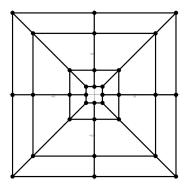
stiffness matrix is sparse and of size 27 × 27 and the obtained approximate solution is shown

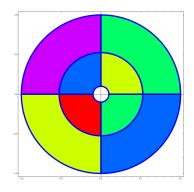


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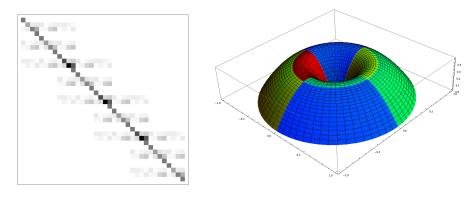
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▶ 8 elements (knot vectors are V = (0, 0, 0, 1/4, 1/4, 1/2, 1/2, 3/4, 3/4, 1, 1, 1), U = (0, 0, 0, 1/2, 1, 1, 1), control net shown below)



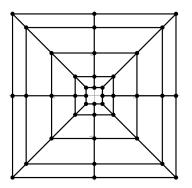


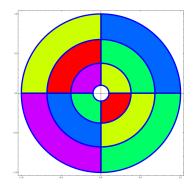
► stiffness matrix is sparse and of size 36 × 36 and the obtained approximate solution is shown



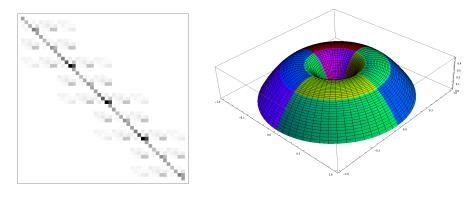
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▶ 12 elements (knot vectors are V = (0, 0, 0, 1/4, 1/4, 1/2, 1/2, 3/4, 3/4, 1, 1, 1), U = (0, 0, 0, 1/3, 2/3, 1, 1, 1), control net shown below)



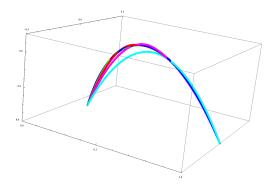


 $\blacktriangleright$  stiffness matrix is sparse and of size  $45\times45$  and the obtained approximate solution is shown



approximate solution tends quickly to exact solution

Parts	Error	Ratio
4	0.05801	
8	0.02248	2.58
12	0.00989	2.27
16	0.00526	1.88



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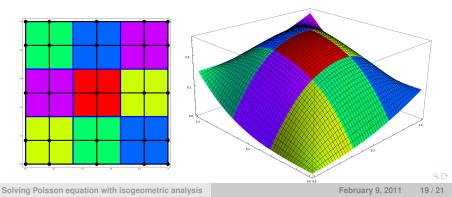
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we solve the non-homogeneous Dirichlet boundary value problem

$$\begin{aligned} & u_{xx} + u_{yy} = -4 & \text{in } \Omega, \\ & u = 0.2x^2 + 0.3y^3 & \text{on } \partial\Omega \end{aligned}$$

where  $\Omega = \{(x, y) \in \mathbb{R}^2 : 0 < x < 1 \land 0 < y < 1\}$ 

NURBS mesh and the corresponding approximate solution

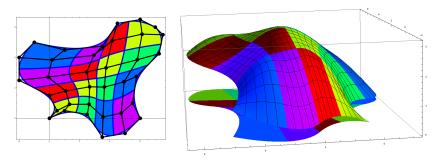


we solve the non-homogeneous Dirichlet boundary value problem

$$\begin{aligned} & u_{xx} + u_{yy} = -1 & \text{in } \Omega, \\ & u = 0.1x + 0.2y & \text{on } \partial\Omega \end{aligned}$$

where  $\Omega$  is planar NURBS domain given by 4 boundary NURBS curves

NURBS mesh and the corresponding approximate solution



# For Further Reading



Cottrell, J.A., Hughes, T.J.R., Bazilevs, Y.: *Isogeometric Analysis.* John Wiley & Sons, Ltd, 2009.



L. Piegl and W. Tiller *The NURBS Book.* Springer, 1996.



Hughes, T.J.R., Cottrell, J.A., Bazilevs, Y.:

*Isogeometric analysis: CAD, finite elements, NURBS, exact geometry, and mesh refinement.* 

Computer Methods in Applied Mechanics and Engineering, 194:4135–4195, 2005.



Y. Bazilevs, L. Beirão de Veiga, J.A. Cottrell, T.J.R. Hughes, and G. Sangalli *Isogeometric analysis: approximation, stability and error estimates for refined meshes.* Mathematical Models and Methods in Applied Sciences, 6:1031–1090, 2006.

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# For Further Reading

M. Aigner, C. Heinrich, B. Jüttler, E. Pilgerstorfer, B. Simeon and A.-V. Vuong *Swept volume parameterization for isogeometric analysis.* Technical report of EXCITING project, http://www.exciting-project.eu.

#### T. Martin, E. Cohen, R. M. Kirby:

*Volumetric parameterization and trivariate B-spline fitting using harmonic functions.* Computer Aided Geometric Design, Vol. 26, pp. 648-664. Elsevier, 2009.

N. D. Manh, A. Evgrafov, A. R. Gersborg, J. Gravesen:

Isogeometric shape optimization of vibrating membrane.

Computer Methods in Applied Mechanics and Engineering, to appear. DOI:10.1016/j.cma.2010.12.015



G. Xu, B. Mourrain, R. Duvigneau, A. Galligo:

Optimal Analysis-Aware Parameterization of Computational Domain in Isogeometric Analysis.

Advances in Geometric Modeling and Processing: LNCS 6130, pp. 236-254. Springer, 2010.

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