

COMPASS-U tokamak Toroidal field coils

v4.0
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Institute of Plasma Physics of the Czech Academy of Sciences

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Description of toroidal field (TF) coils for companies who shown interest in preliminary market consultations.

Document serves for discussion with companies with aim to:

- 1) Fulfill design requirements.
- 2) Meet engineering/manufacturing limitations and clarification of manufacturing process.
- 3) Lower the manufacturing cost.
- 4) Obtain preliminary price quotation.

Final design will be specified in technical specification for toroidal field coils after discussion with companies.

Presentations consists of:

- Design requirements.
- Purpose of components.
- **Questions for companies.**
- **Not fixed parameters (depending on answers from companies)**

Further information (drawings) which are regularly updated can be found in

http://www.ipp.cas.cz/o-ufp/Verejne_zakazky/doc.html under section “Coils of toroidal field”.

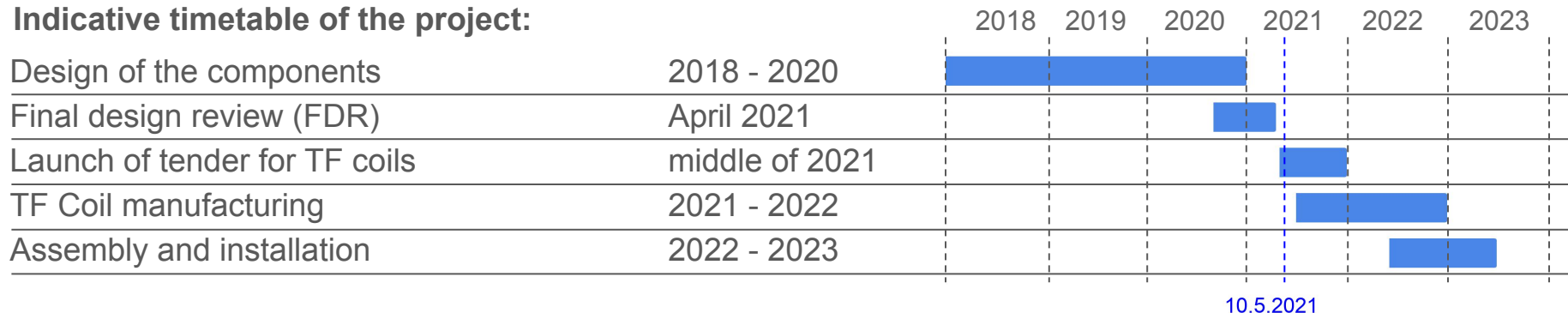
Toroidal field coil is one of the subsystems of COMPASS-U tokamak.

Key properties of COMPASS-U:

- High magnetic field to confine plasma (5 T) and high plasma current (2 mil. Amperes)
- Discharge durations up to several seconds, advanced plasma configurations, high heat fluxes
- Operation with high temperature first wall – up to 500°C
- Mid-size device with flexibility for scalings towards ITER and DEMO

⇒ unique capabilities to address DEMO challenges

Indicative timetable of the project:



Presumed scope of work:

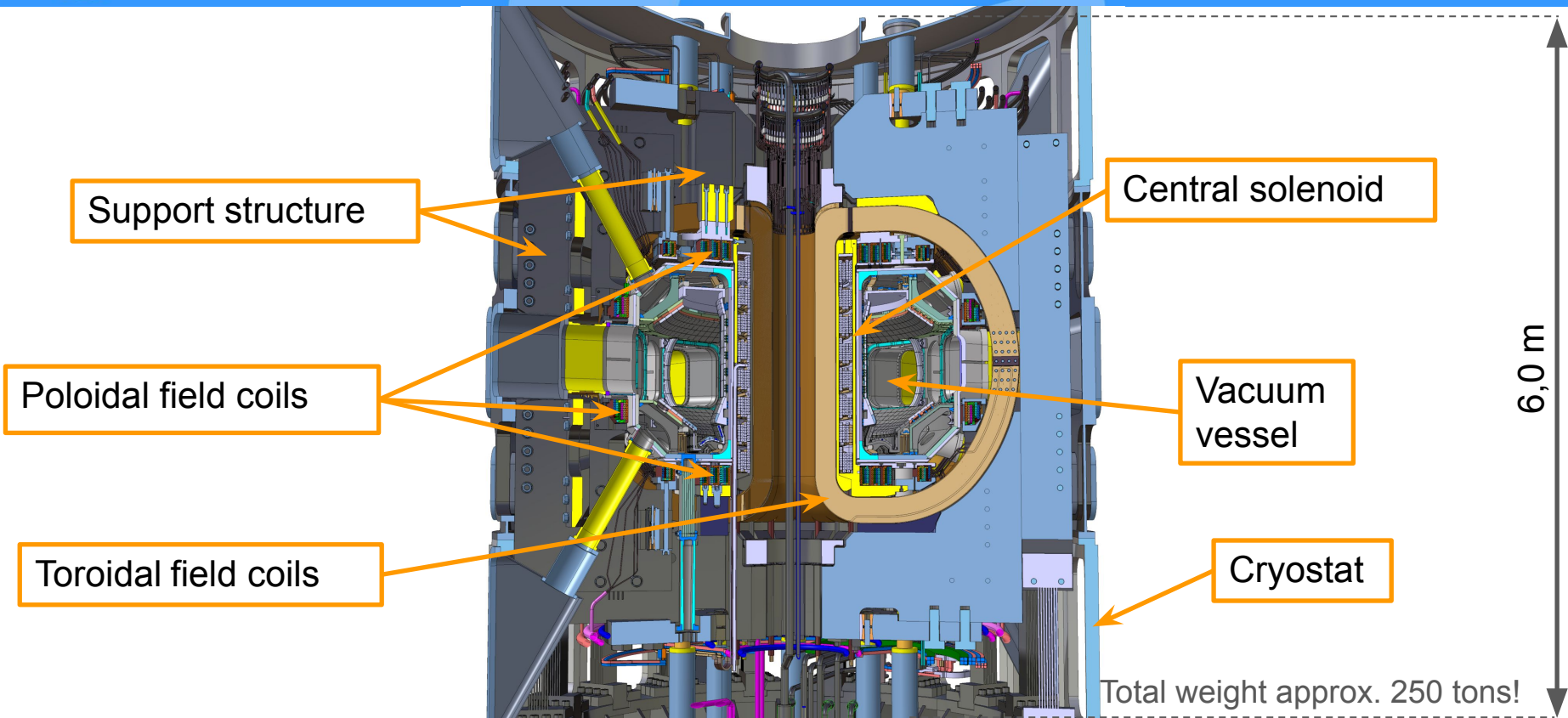
- Manufacture of 16 toroidal field coils

Presumed scope of work on the coil (what to expect):

- Machining of copper plates and connection (welding/brazing/soldering) of separately machined parts e.g. sliding/bolted joints if not possible to machine in one piece
- Insulation with fiberglass cloth and VPI and prepreg
- Electrical testing
- Test assembly
- Transport to IPP

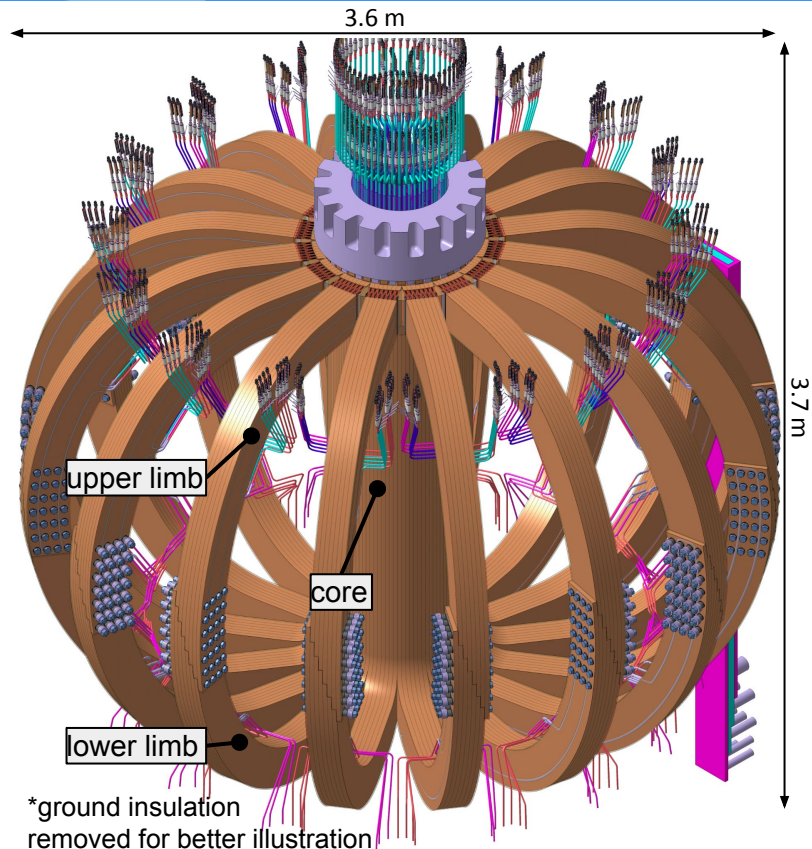
Notes:

- [Coil of central solenoid](#) (not part of the delivery) has to be wound on assembled TF core.
- Feltmetal (described later) is not part of delivery.
- Coil models and coil parameters in this presentation are preliminary and could change during preliminary market consultations.



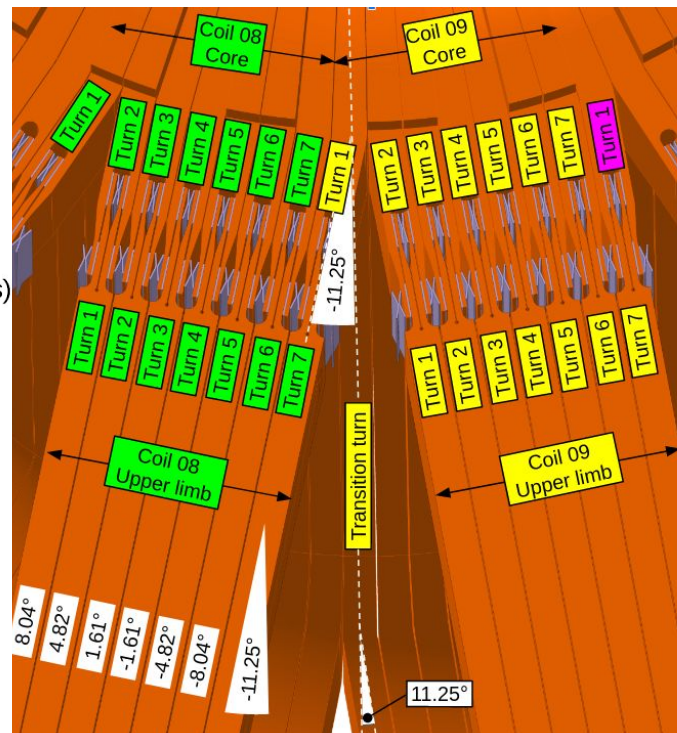
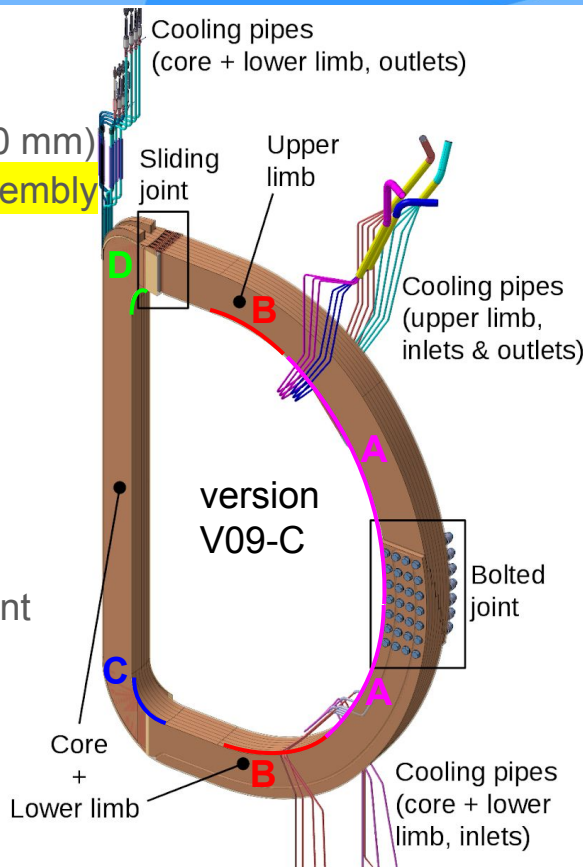
Preliminary parameters:

- 112 D-shaped turns grouped to 16 bundles with 7 turns
- Each turn composed of 2 parts with joints (upper and midplane joint - allow vertical assembly of parts inside of TF coils)
- Outer dimensions of one turn $\sim 2.6 \times 1.7$ m
- Total mass 22.7 tons (core+lower limbs: 14.8 tons, 16 upper limbs: 7.9 tons)
- Turns insulated by **fiberglass cloth + VPI + prepreg**
- Current 200 kA providing 5T @ $R = 0.896$ m for ~ 5 s
- Turn cross section 20×200 mm made from hardened OFHC copper or similar material (CuAg0.1(OF))
- Cryogenically cooled by gaseous Helium down to $T > 50$ K by cooling channels in each turn



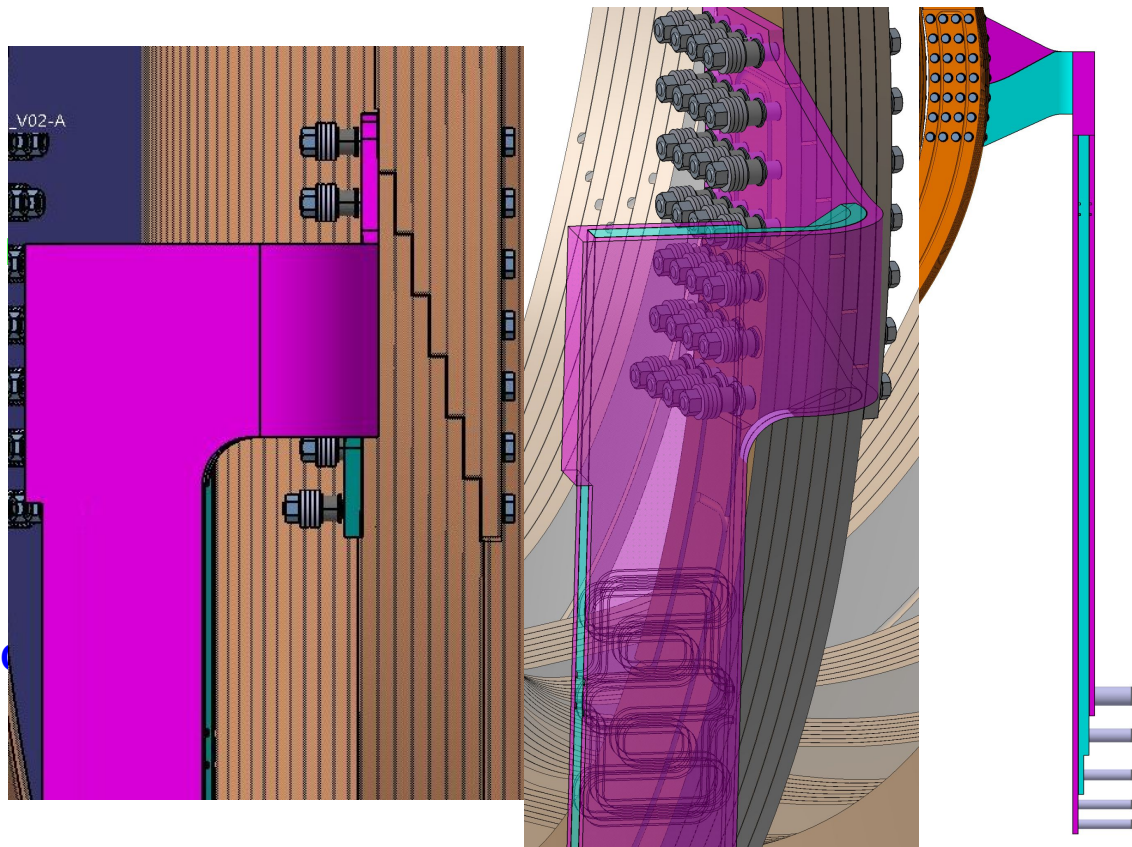
Preliminary design:

- D-shape vertically asymmetric:
4 radii ($r_{inner} = 1300, 700, 175, 100$ mm)
- VV & PF inside \Rightarrow vertical disassembly
 \Rightarrow two joints
- Upper joint in high stressed area
 \Rightarrow sliding joint
- Structural parts:
 - upper limb (planar geometry)
 - core (cylindrical)+
lower limb (planar) \Rightarrow bend)
- Feeder connection and turn-to-turn transition in bolted joint
- Coil-to-coil transition in core



Preliminary design:

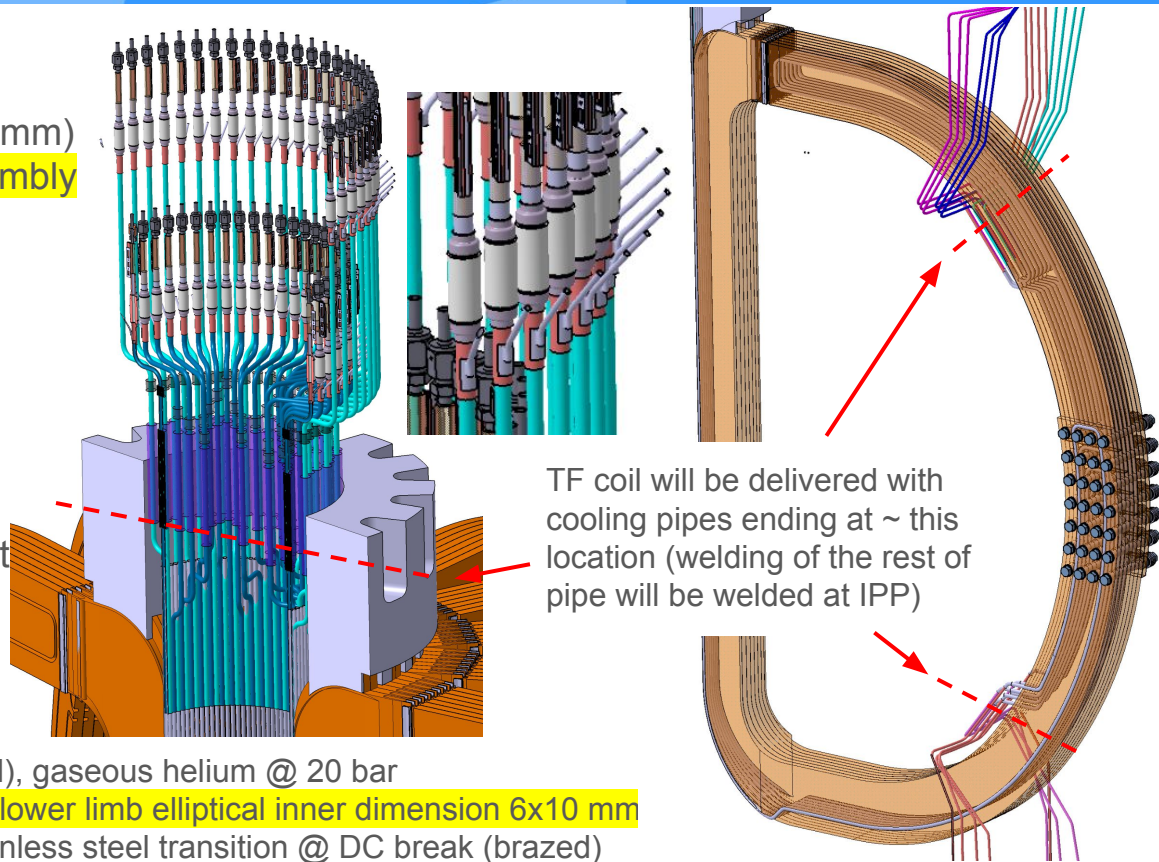
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turn-to-turn transition in bolted joint
- Coil-to-coil transition in core
- Feeder: $\Delta T \sim 200 \text{ K} \Rightarrow$
 \Rightarrow cross-section doubled
 \Rightarrow dipole \rightarrow quadrupole
 \Rightarrow thermal anchor



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- Cooling:
 - groove and pipe concept (soldered), gaseous helium @ 20 bar
 - upper limb inner $\varnothing 6 \text{ mm}$, core + lower limb elliptical inner dimension 6x10 mm
 - helium tightness \Rightarrow copper \rightarrow stainless steel transition @ DC break (brazed)

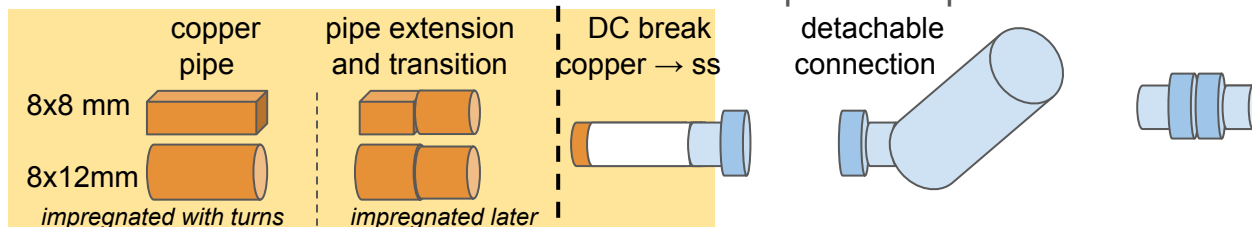


Operational parameters:

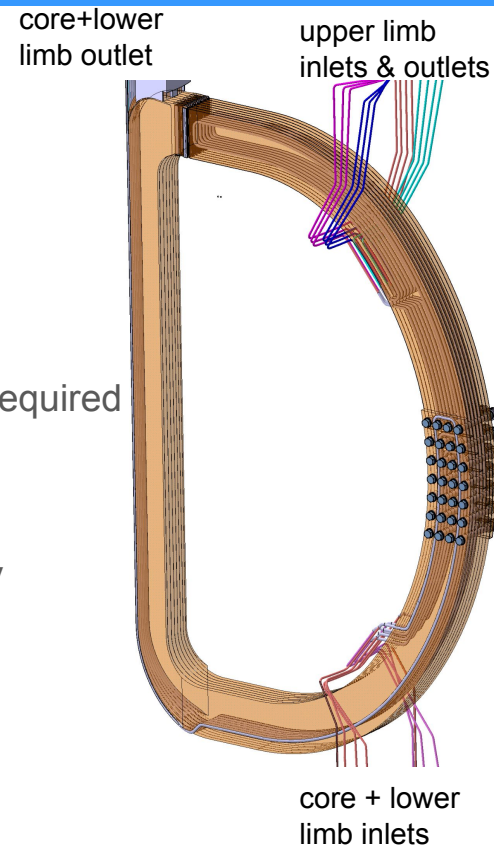
- Initial temperature 80 K, $\Delta T \sim 60$ K in ~ 10 s, cooldown time ~ 30 minutes

Cooling:

- Each part of the turn has its own cooling pipe
- Grove and pipe concept
- Material of pipes: copper (to match CTE + high conductivity)
- Connection of pipes: soldering (process should not anneal TF base material from full hard copper)
- Coolant: gaseous helium, pressure ~ 20 bar \Rightarrow helium tight connections required
- Distribution of helium outside TF coils by stainless steel pipes \Rightarrow copper to stainless steel transition required (covered under insulation)
- Pipes electrically connected to turns \Rightarrow insulation piece required
- Production and connection of transition piece not part of TF coils delivery

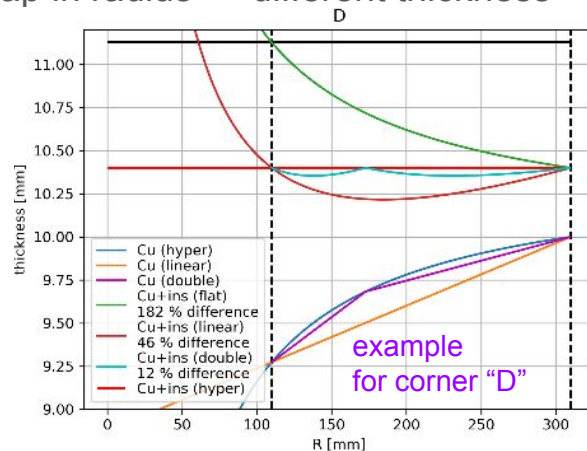
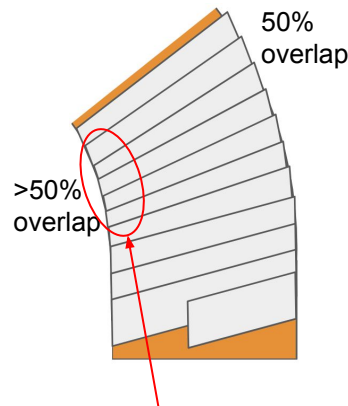
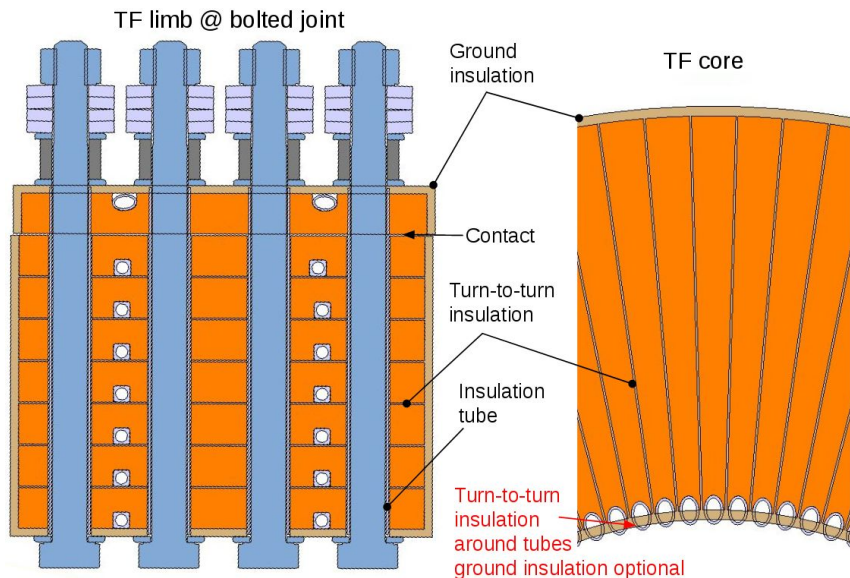


part of TF delivery | not part of TF delivery



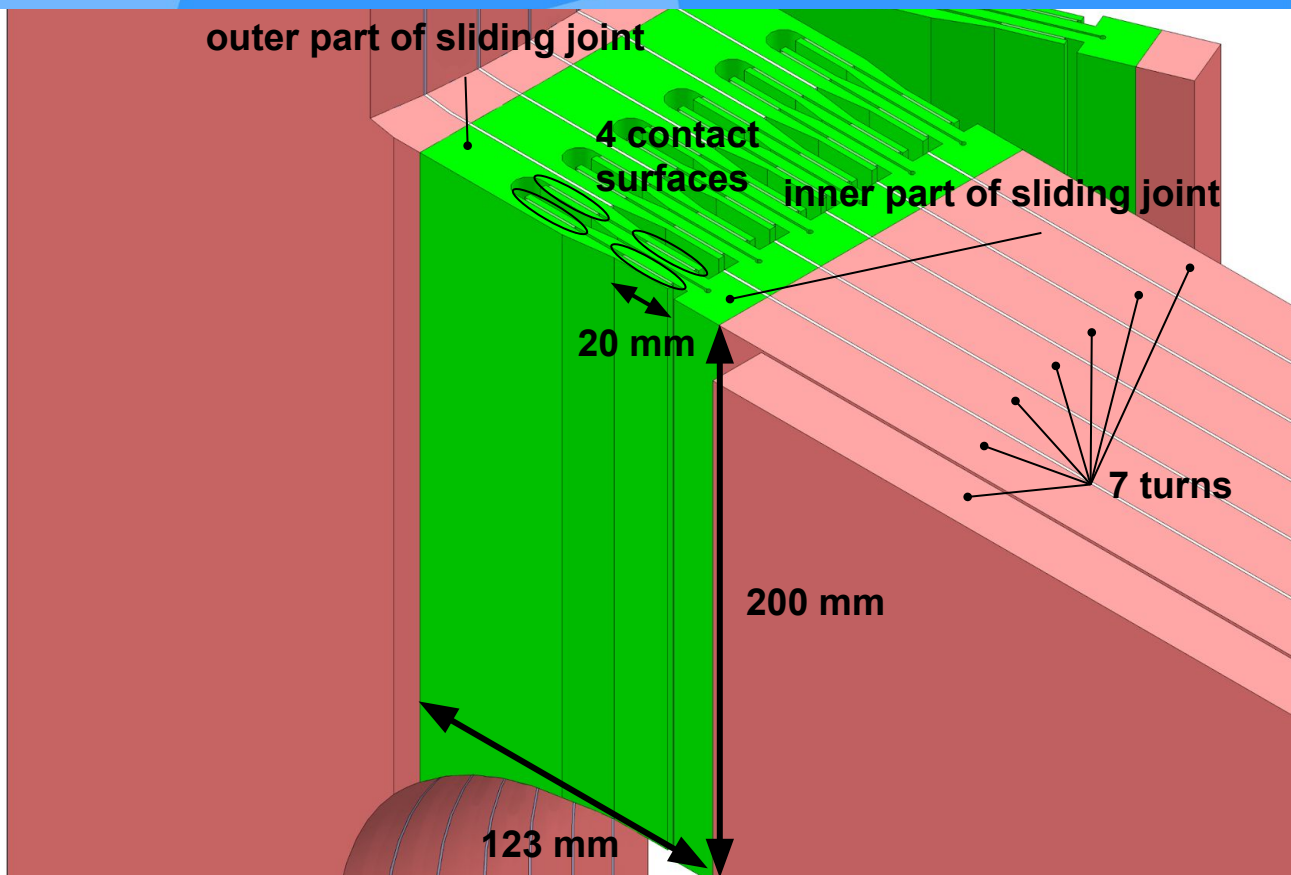
Design: (one of proposed solutions)

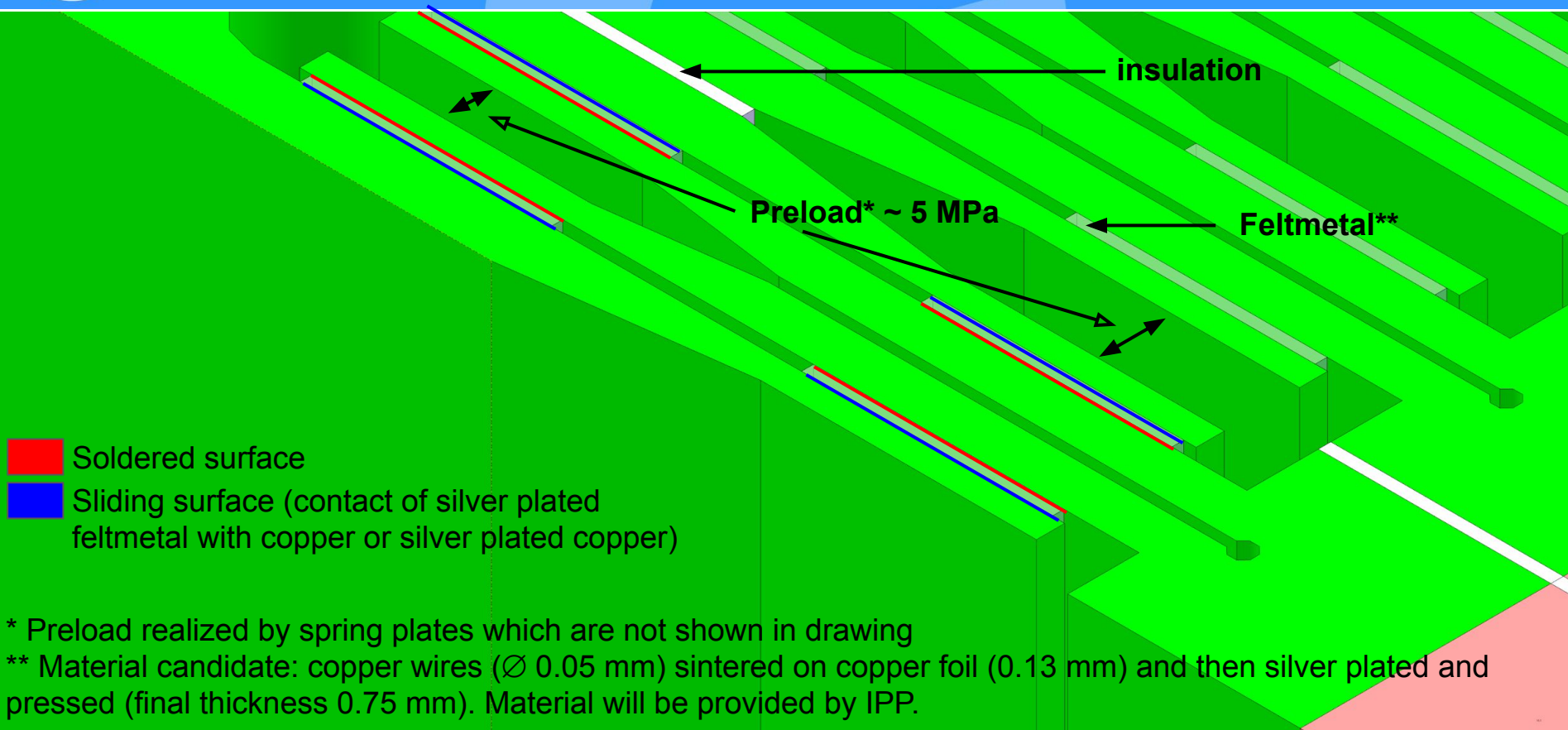
- Voltage: turn-to-turn 10 V, first-to-last turn 1 kV, turn-to-ground 2 kV. Stresses: tension 20 MPa, shear 50 MPa
- turn-to-turn 1 mm (fiberglass tape 50 % overlap + VPI) \Rightarrow different overlap in radius \Rightarrow different thickness
- ground (including turn-to-turn) 4 mm (prepreg sheet) \Rightarrow ground 3.5 mm
- insulation of cooling pipes and voltage taps up to DC break



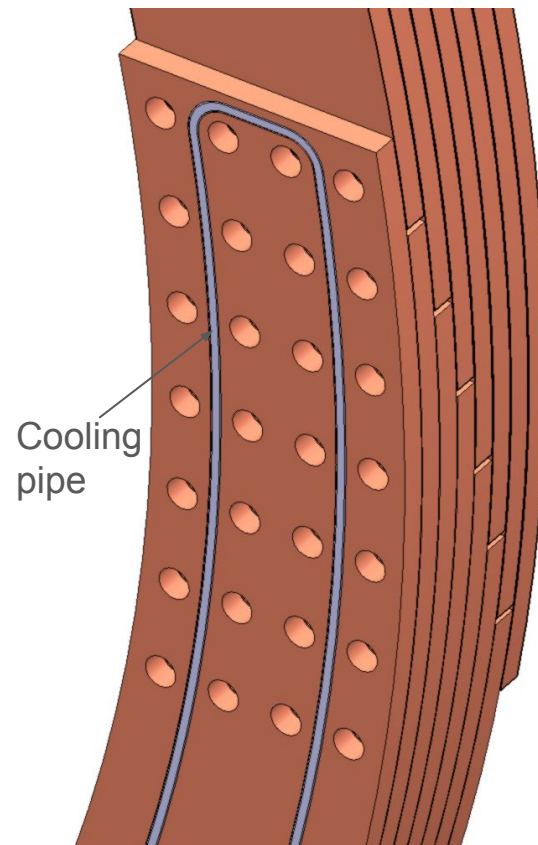
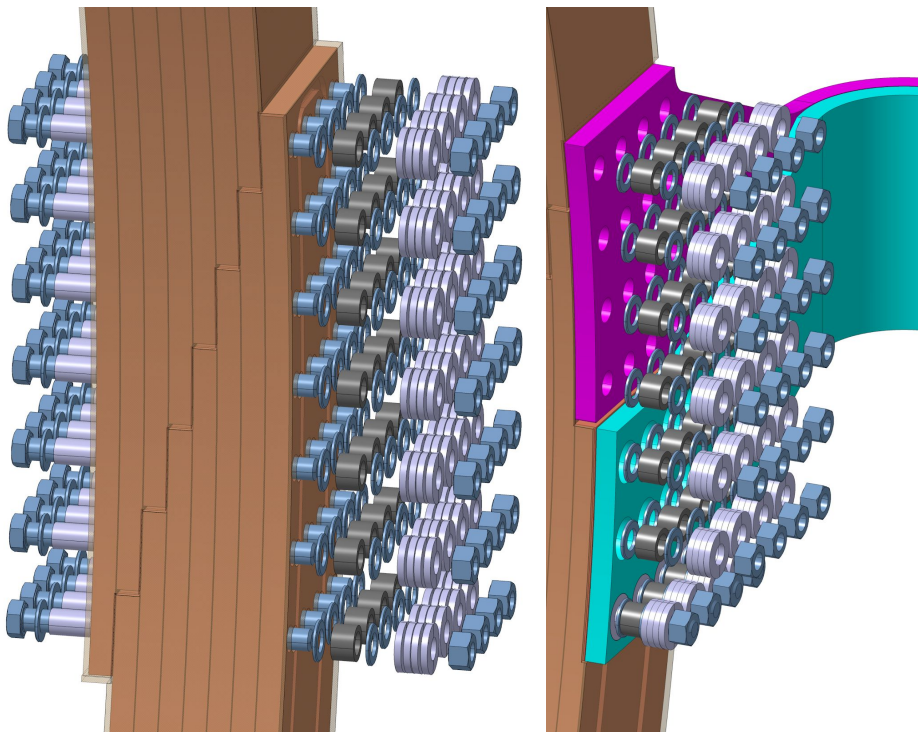
Different plate thickness at inner and outer radius \Rightarrow 3D machining required. Is it possible to? (fiberglass tape allows compression \Rightarrow double roof shape sufficient)

- coil current: 200 kA
- 7 turns per coil bundle
- 1 sliding joint per turn
- 4 contact surfaces per joint
- each surface has 20x200 mm
- average current density:
1.25 kA/cm²
- peak current density:
~ 5 kA/cm²





- 28x M20 bolt with insulation tube

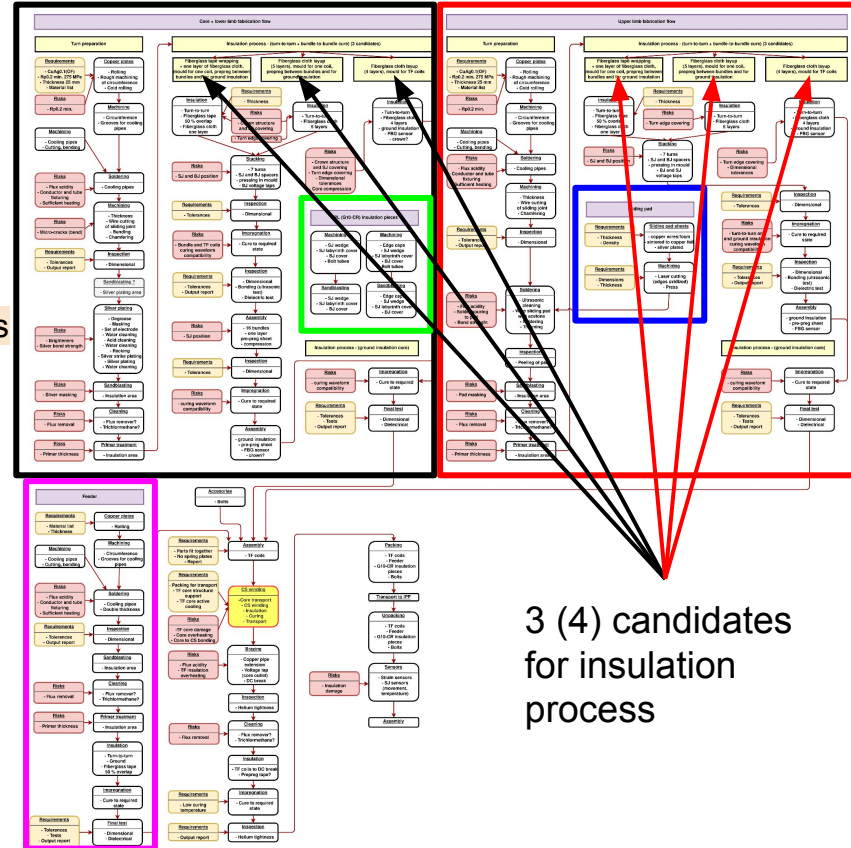


Materials:

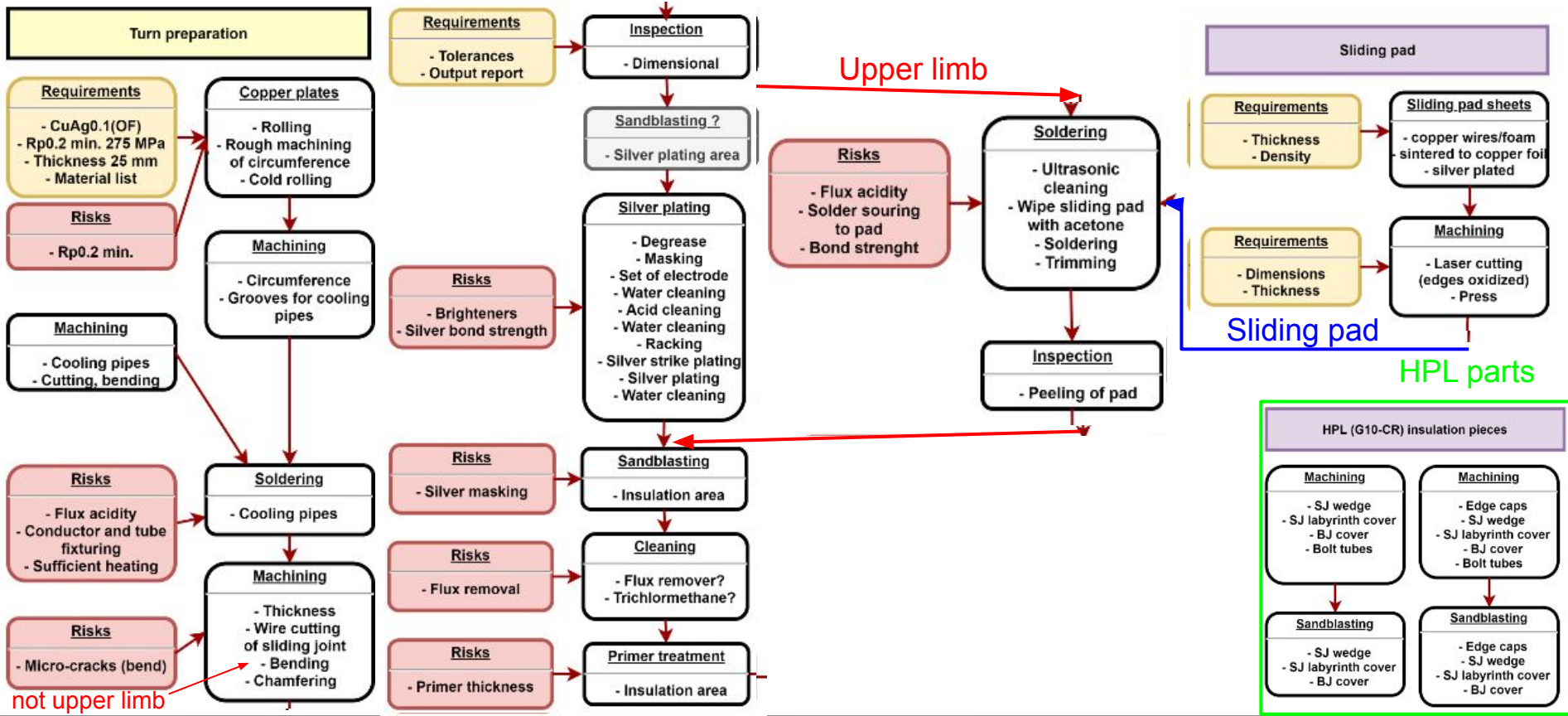
- Turns: CuAg0.1(OF) \Rightarrow higher strength w/o negative effect on conductivity, **RRR > 30**, **$R_{p0.2} > 275$ MPa**
- Composite:
 - VPI (reinforcement): E-glass tape or cloth 7781 style,
 - VPI (matrix): epoxy resin CTD-101K or GY282
 - Ground insulation and bundle-to-bundle connection: prepreg sheet \leftarrow compatible curing waveforms
 - G10-CR for insulation pieces machined from HPL
- Solder:
 - Sliding pad: Sn96Ag4
 - Cooling pipes: not yet decided
- Sliding pad material: Feltmetal™ or Copper foam
- Grease: Aremco 641-EV or CHO-LUBE 2440

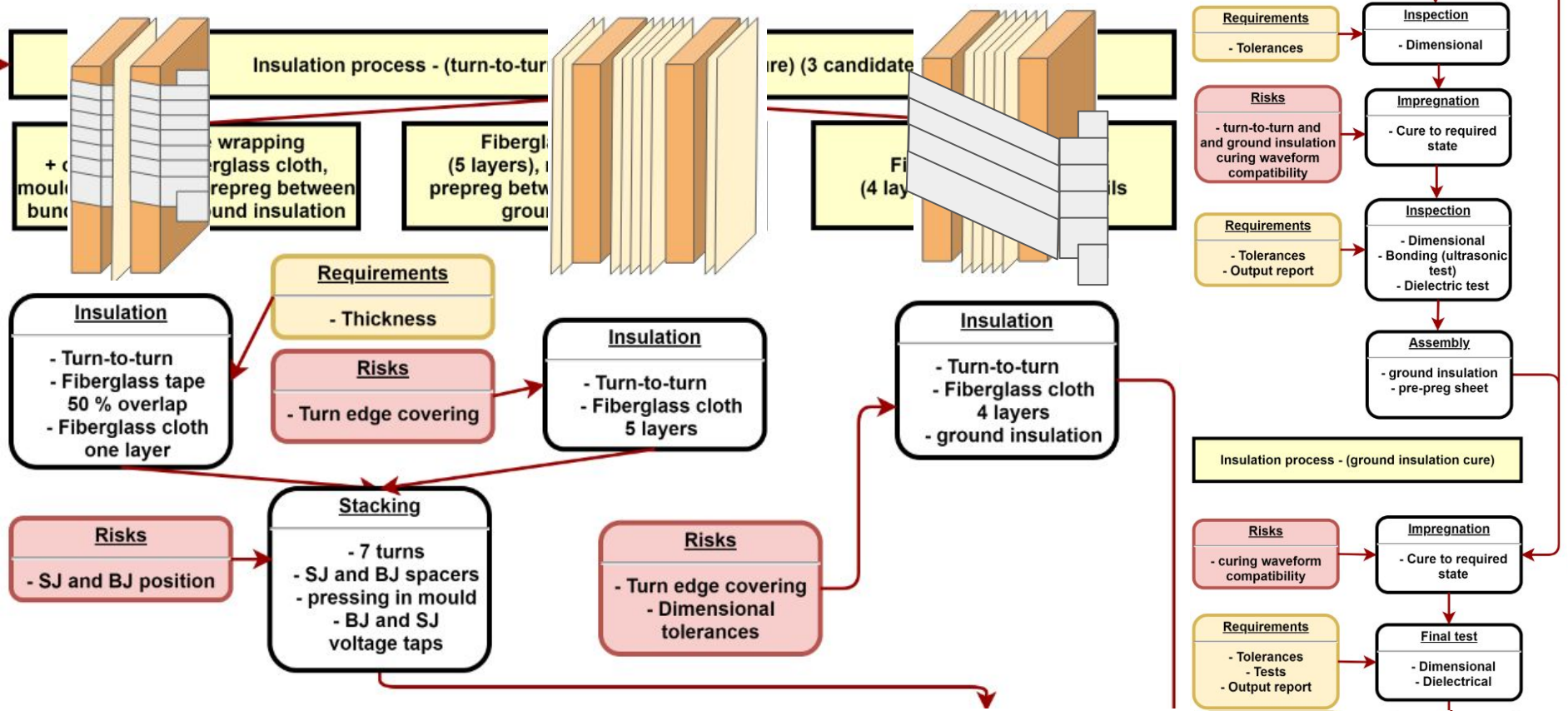
Main parts:

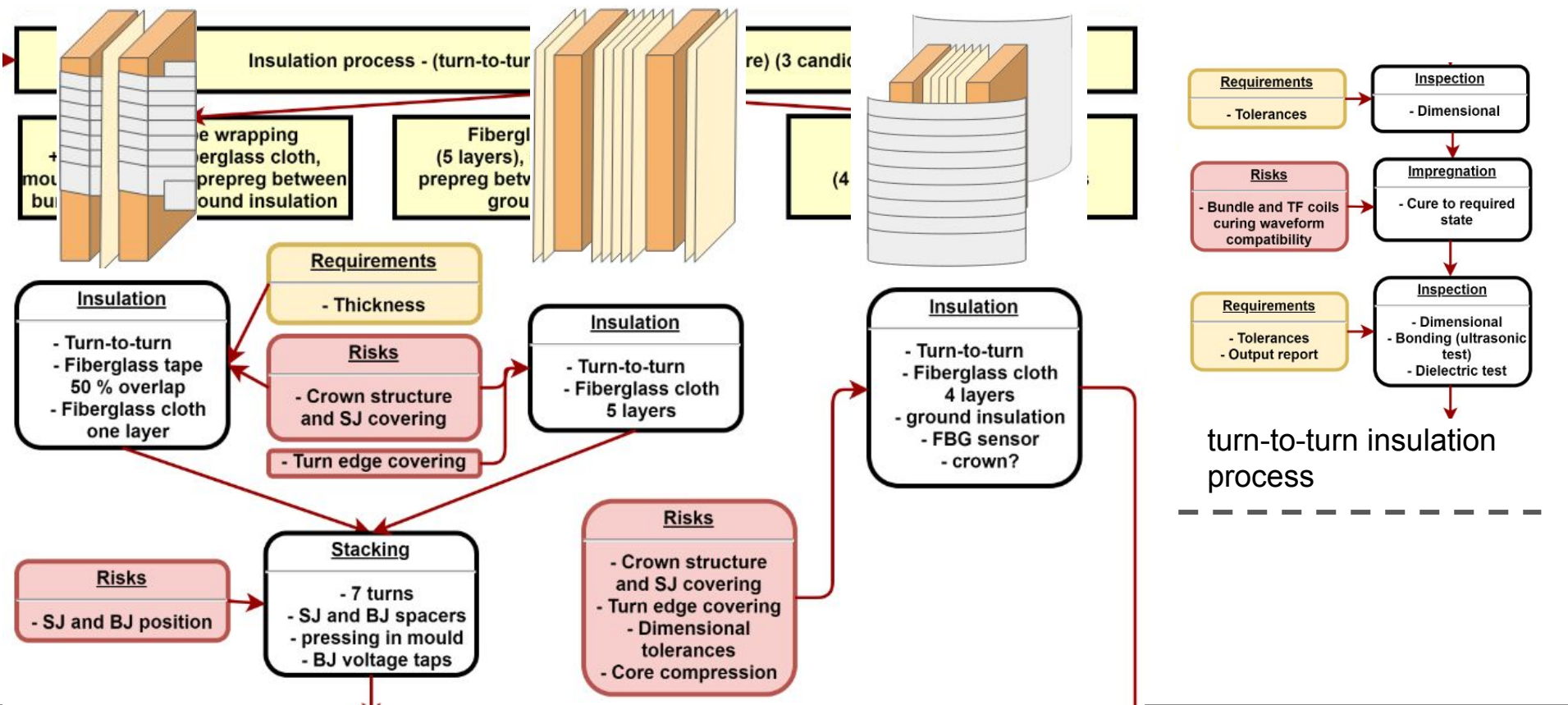
- Core + lower limb including **HPL parts**
- **Upper limb** including **Sliding pads**
- **Feeder** and **CS winding**



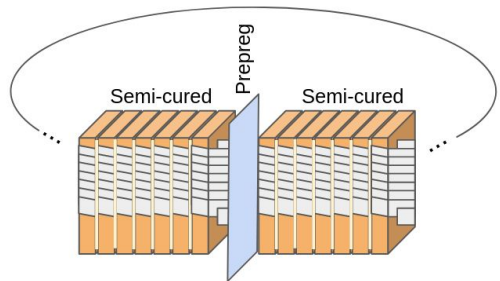
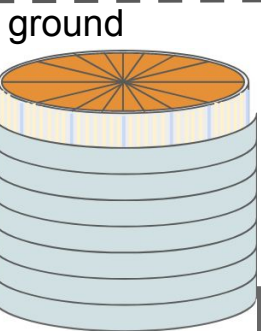
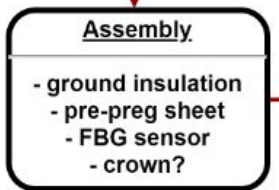
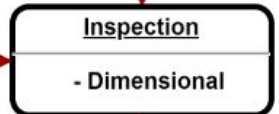
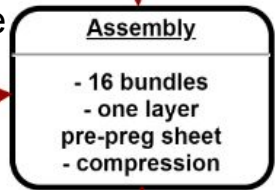
3 (4) candidates for insulation process





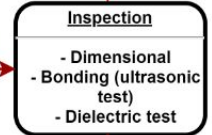
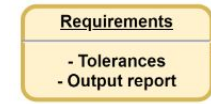
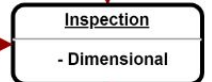
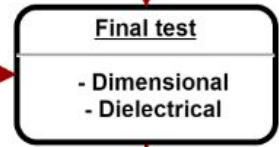
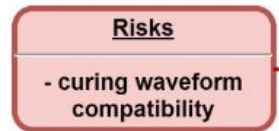


bundle-to-bundle

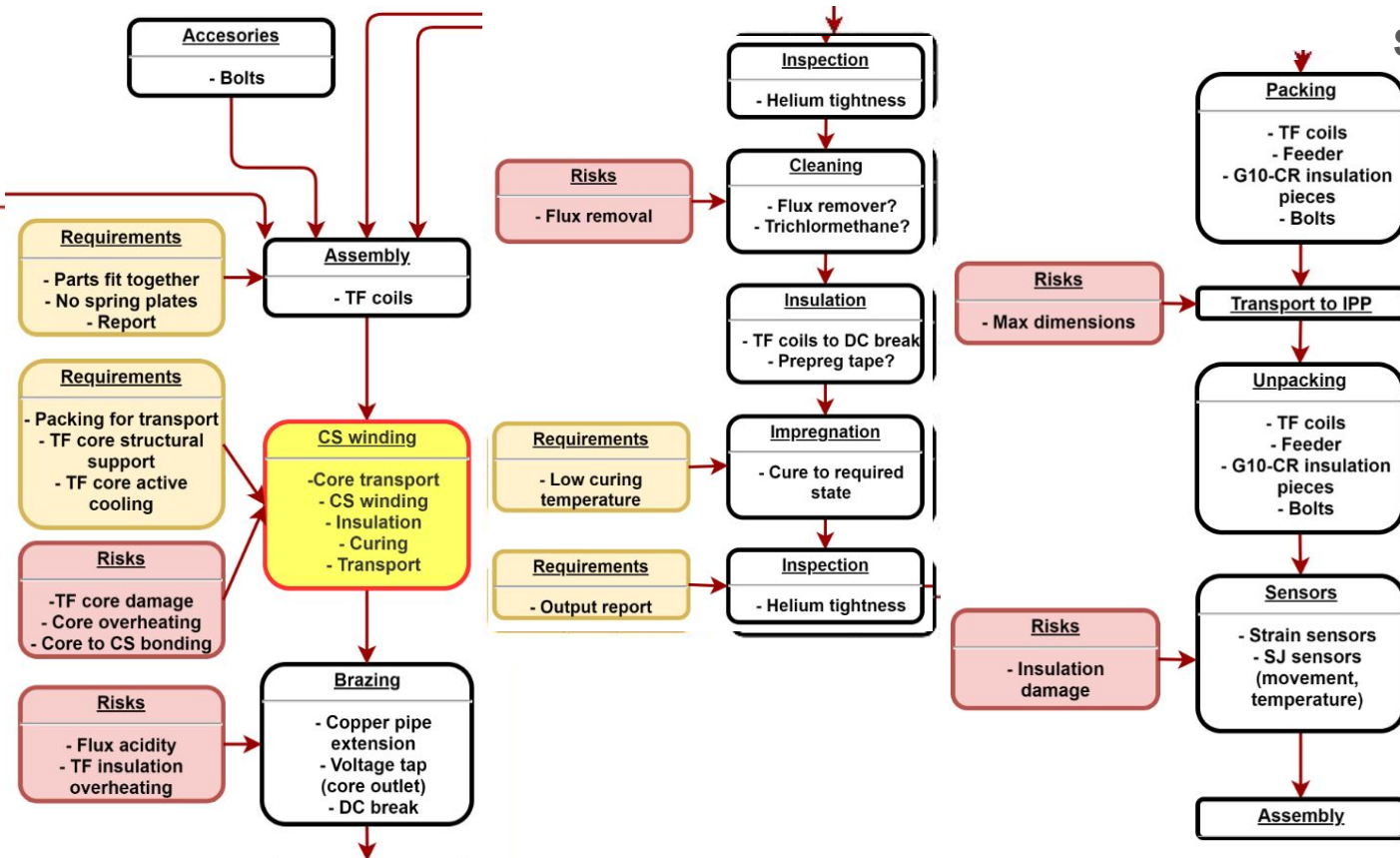


symmetrical cover
as cover

insulation cure)



turn-to-turn insulation process



Summary

- Reliable insulation by VPI
- Combination with prepreg sheet ⇒ ⇒ to meet manufacturing tolerances ⇒ lower the costs
- Variable overlap ⇒ ⇒ higher thickness in corners
- Critical operation: CS winding on the TF core

Machining tolerances:

- General tolerances will be set by DIN ISO 2768 mK.
- Tolerances for preliminary design of TF core are shown in attachment *HFCU-04-00-v7-3_B.pdf* (Sheets 1-4)
- TF core is a critical component in the sense that it is composed of 112 turns (parts) and the small variations on one turn can after assembly of 112 turns lead to significant variation. Second challenge is that the TF core part has to fit into upper limb in the location of sliding joint which is very detailed structure. Therefore, the tolerances on TF core parts are very tight.

There is a space for discussion how to meet requirements using different manufacturing process. Is there any preferable manufacturing process how to meet TF core tolerances (including VPI)?

Electrical Tests:

- Turn to turn voltage 1 kV
- First turn to last turn voltage 3 kV
- Coil to ground voltage 3 kV

1. Insulation process (fiberglass cloth + VPI or G10 composite or prepreg sheets) - depends on:
 - a. Which process can fulfill requirements on electrical and mechanical insulation properties and which can meet manufacturing tolerances
2. There are two bends in TF core with 11.25° angle. 6 of 7 turns are bended in same direction. One turn has top and bottom bend in opposite direction. It was assumed that bending will be done with thicker plates and then precise machining will be done. Is it possible to meet prescribed tolerances using this approach?
3. Different plate thickness at inner and outer radius \Rightarrow 3D machining required. Is it possible to? (fiberglass tape allows compression \Rightarrow double roof shape sufficient)
4. What is an approximate cost for manufacturing of the TF coils?

In case of any questions do not hesitate to contact us via email (next slide) or videoconference.

Further information (drawings) which are regularly updated can be found in http://www.ipp.cas.cz/o-ufp/Verejne_zakazky/doc.html under section “Coils of toroidal field”. (there is a language switch in upper right corner)

At website tenders electronic daily

Notification Number at Tender electronic daily: 2019/S 113-276584

(Číslo oznámení TED: 2019/S 113-276584)

Contact persons:

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Jaroslav Krbec email: krbec@ipp.cas.cz (also put nemec@ipp.cas.cz in the copy)

Attachment:

- *CU_CUPG-04-00-V08-B.zip*
 - Model of TF coils:
 - *CU_CUPG-04-00-V08-B.stp*
 - Drawings and machining tolerances of TF coils
 - *CU_CUPG-04-00-V01-A.pdf*